Chemical provenance of pre- to post-contact period copper and copper-rich alloy artifacts from archaeological sites in Nova Scotia, Canada: a laser ablation ICP-MS study

By J.L. Whattam

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Approved: Dr Jacob Hanley Associate Professor

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Copper had cultural significance to the Mi'kmaq peoples of the Maritimes, and was used in the fabrication of tools and personal, ceremonial, gift, and trade wares. In this study, LA-ICP-MS was used to characterize the trace elemental composition of artifacts from archaeological sites in Nova Scotia ranging from Early Woodland (2500-2400BP) to Protohistoric (450-350 BP) to European contact (1500+BP) periods in age, and samples of natural copper from potential sources with goals of: (i) differentiating artifacts derived from natural copper from those made from synthetic (refined) European (trade) copper and its alloys, and (ii) identifying the specific natural sources of copper that were exploited. The methodology used in this study improves on previous bulk analytical methods (e.g., INAA, XRF) that suffer from the presence of contaminating mineral phases within the copper volume analyzed and are more destructive. LA-ICP-MS analysis of 57 artifacts identified groupings compositional with specific elemental 10 enrichment/depletions/ratios, notably involving Ag, Pb, Hg, Bi, Zn and As. Most single artifacts are compositionally homogeneous with respect to the majority of elements with <20% relative variation in concentration over 8-10 ablation spots. Patinas show preferential enrichment (e.g., Fe, Sn, Zn, Au) and depletion (e.g., Ni, Co, Ge, Ag) relative to the fresh metal. However, differences in source composition are significant enough that the patina can be diagnostic of provenance. Three groups have definitive provenance determined: six artifacts from Cap d'Or, Nova Scotia (natural Cu), six from Margaretsville, Nova Scotia (natural Cu), and nine artifacts of European origin (refined Cu or Cu-Zn-Sn alloys). Seven remaining artifact groups have unknown provenance and, importantly, sources analyzed from Michigan, USA (Keweenaw Peninsula) are ruled out. Contrary to the Lake Superior model, copper deposits from the Bay of Fundy were important but many other sources of the metal are likely and require further investigation.

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1.0 Introduction

The chemical microanalysis of archaeological materials by non-destructive methods allows insight into the manufacturing and origins of objects that are of considerable cultural or archaeological value. For metallic artifacts in particular, which often present significant surface corrosion modifying primary composition, robust chemical characterization of fresh material has required invasive sampling methods and large sample volumes, primarily due to limitations in the analytical methodologies available to archaeological sciences historically. The preservation of sample integrity and appearance is a priority during collection, conservation, storage and study, and must be carefully reconciled with the desire to reduce uncertainties in provenance studies introduced when fresh metal cannot be accessed in an artifact.

In North America, there has been considerable work done to identify the origins of natural copper artifacts, ad to differentiate between natural and refined (European) copper and its alloys. In the sixteenth and seventeenth centuries, the first permanent settlers from Europe arrived in Nova Scotia to find it was inhabited by the Mi'kmaq, the indigenous group of people that had been living in Nova Scotia thousands of years before the arrival of the Europeans in the early 1600s (Morton, 1999). It has been heavily documented that the Mi'kmaq used materials such as animal hides and fur, bones, wood, and stones to make their clothing, jewelry and tools (Whitehead 1993, Leonard 1996, Whitehead et al 1998, Levine 1999, Rapp 2000, Bourque, 2001, Fenn 2001, Glascock & Neff 2003, Anselmi 2004, Lattanzi 2007, Dussubieux et al. 2008, Lattanzi 2008). Another material favoured by the Mi'kmaq, was copper. As indigenous peoples slowly spread across North America, their spiritual connections to, and practical utilization of, raw materials including metals

changed continuously. In fact, creating and trading of goods amongst themselves and with other indigenous peoples led to the first commercial use of metals (Quimby, 1966; Bourge, 2001; Lattanzi, 2007; Levine, 2007; Cooper et al., 2008; Cooper, 2011). The importance of copper to the Mi'kmag had also been increasing as migrations, settlements and discovery of new sources of the metal took place. Copper was used for a variety of purposes and in the archaeological record, objects of definitive purpose have been identified including trade "currency," personal adornments and burial necessities for the afterlife in the form of talismans, beads (Rapp, 2000; Mulholland & Pulford 2007) and tinkling cones (Levine 2007), and after European contact, the use of copper kettles for burial practices, practical use of vessels, and reworking into other objects listed here (Turgeon et al., 1990; Fitzgerald et al., 1993; Whitehead et al., 1998). The first use of copper in what is now Canada dates back to between 6800 BP (Ehrhardt, 2009) and 5560 BP (Beukens et al. 1992; Rapp & Hill, 2006) based on controlled archaeological stratigraphy (spatial relationships to other objects from these times) and radiocarbon dating methods. Later in the archaeological record for the Protohistoric period, it was known to be obtained from Europeans during trade involving the Spanish (Basque), and later the French, Dutch and English (Hancock et al. 1991; Whitehead, 1993; Rapp 2000; Lattanzi, 2006; Levine 2007; Klein et al 2010; Michelaki et al 2013).

To date there has been no scientific analytical studies done on pre-contact artifacts found in Nova Scotia in order to identify the sites of origin of their contained copper with respect to possible sources of this metal in the region, and elsewhere. In addition, there has been no work conducted to characterize contact-era artifacts through chemical analytical means. Several studies have been undertaken to discuss where indigenous peoples in some

areas of North America, (Ontario, Yukon, and the northeastern United States) procured their copper (Hancock et al., 1991; Fitzgerald et al., 1993; Levine 1996, 2007; Whitehead et al., 1998; Rapp et al., 2000; Fenn 2001; Junk, 2001; Lattanzi 2007, 2008; Mulholland & Pulford, 2007; Dussubieux et al., 2008; Hill, 2012), but no studies have been conducted in the Atlantic provinces with the exception of a single chemical analytical study of burial artifacts from three localities by INAA all found to be of European origin (Whitehead et al., 1998). The most commonly accepted theory with respect to the procurement of native copper for the creation of objects, is the Lake Superior model (Hancock et al., 1991; Levine, 1996, 2007; Rapp et al., 2000; Fenn, 2001; Lattanzi, 2007, 2008; Ehrhardt, 2009). Through this model, it has been widely accepted that any archaeological copper prior to European contact and trade, originated in the Lake Superior areas of Ontario (e.g., Mamainse Point) and Michigan (e.g., Keweenaw Peninsula). These locations were rich in large native copper deposits and were later mined commercially for over one hundred years (Rosemeyer, 2009, 2011). The deposit types in this area range from the volcanic red bed copper more typical of the Keweenaw Peninsula (Eckstrand et al., 1995), to less common stratiform sedimentary hosted copper deposits (ex. the White Pine Mine) (Brown, 1992; Eckstrand et al., 1995). Many researchers appear to simply accept or assume that copper artifacts originated from the Lake Superior region such as Holmes (1901) and Reeder (1903), both of whom "presented [this model] as if it were a proven fact" (Levine, 2007). However some archaeologists have questioned this hypothesis (see Levine, 1996, 2007; Rapp et al., 2000; Fenn, 2001; Lattanzi, 2007, 2008; Hill, 2012), and through careful chemical analysis by relative destructive means combined with statistical methods of data analysis, have shown that some artifacts found in the United States and central Canada (Ontario, Quebec) were likely sourced from other copper mineralization throughout the northeastern United States and Nova Scotia (the Bay of Fundy Region).

This study involved the microanalyses by laser ablation inductively-coupled plasma mass spectrometry (LA-ICP-MS) of 60 copper-based artifacts collected from 6 archaeological sites representing sites of aboriginal habitation in Nova Scotia, Canada (Figure 1.1, Table 1.1), and 38 geological samples (native, naturally-occurring copper) from 15 deposits in Canada (Nova Scotia; Figure 1.2), the United States (Michigan, Pennsylvania) and some international sources (Bolivia, the United Kingdom, Kazakhstan), Tables 1.1 and 1.2 summarize the characteristics of the artifacts and natural copper source samples analyzed. Some of the artifacts studied have been dated using archaeological methods and it is considered that the collection spans a time period through the Early to Late Woodland periods (2500-500 BP) and up to the contact period. However, little is known as to the original geological provenance of the copper found at the archaeological site localities. The application of LA-ICP-MS to in-situ trace element analysis is an appropriate method for archaeometry as it is a relatively non-destructive method (i.e., generating only microscopic pits invisible to the naked eye) compared to instrumental neutron activation analysis (INAA; requiring several hundred mg of sample) or X-Ray fluorescence (XRF; requiring a flat surface on the object greater than ~14 mm in diameter or a powder of minimum volume of several grams). The LA-ICP-MS method also achieves a much wider range of, and much lower detection limits for, trace elements compared to the other methods.

The main objectives of this study were (i) identify the source of native copper contained within artifacts recovered at various aboriginal archaeological sites across Nova Scotia, and (ii) to evaluate and discuss the benefits of LA-ICP-MS as an analytical method for metallic archaeological objects. The study establishes recommendation for the analysis of archaeological materials by LA-ICP-MS, highlighting the rapid analysis of materials for a range of trace elements that is not possible by other typically used analytical means without substantial sample preparation and destruction.

In this study, whole artifacts were mounted and inserted into the ablation chamber, analyzed and removed intact with no visible damage. It is important to note that the majority of the previous work on North American copper artifacts (Levine, 1996; Rapp, 2000; Kuleff and Pernicka, 1995; Rapp Jr., 1985; Mulholland and Pulford, 2007) used INAA to study trace element concentrations in native copper artifacts. Review of the data sets produced by these studies indicate that, in addition to their relative destructive nature, these applications of the methods above have revealed relatively large variations in copper chemistry from single artifacts and sources, likely due to contamination of the analytical volumes removed from the objects by inclusions of other mineral grains. More recently, LA-ICP-MS analyses of copper artifacts were done by Fenn (2001), Lattanzi (2007 and 2008), Cooper (2008) and Hill (2012). Some concerns about the standards utilized for calibration of analyte sensitivities in these LA-ICP-MS studies were identified and a full description of the relative advantages and disadvantages of the LA-ICP-MS method follows in a discussion.



Figure 1.1 Geological map of study area (modified from Marche, 2014) depicting changes in rock type. Excavation sites shown. Software: QGIS Version 2.2 Data Sources: Nova Scotia Department of Communities, Culture and Heritage, Nova Scotia Department of Natural Resources Disclaimer: Map not to be used outside of MNH/SMU research Datum & Projection: NAD 83 UTM Zone 20. Cartographer: Jennifer Marche.



Figure 1.2 Map of Nova Scotia showing geological units in the areas where native sources were collected. Modified from NS Department of Natural Resources online GIS Database.

| Table 1.1 | Object descriptions of an cop | per armacis in me | conection belonging to | me nova Scoua mus | eum anu (| .KM group. |
|-----------|-------------------------------|-------------------|--------------------------|-------------------------|------------------|---------------------|
| Sample | Site | Age ³ | Description ¹ | Patina ² | Size (cm) | Source |
| 8566 | Gaspereau Lake Reservoir | Woodland period | Nodule | Low | 2.4 x 0.9 | CRM Group |
| 8567 | Gaspereau Lake Reservoir | Woodland period | Nodule | Low | 3.0 x 1.6 | CRM Group |
| 8568 | Gaspereau Lake Reservoir | Woodland period | Nodule | High | 2.0 x 0.8 | CRM Group |
| 8569 | Gaspereau Lake Reservoir | Woodland period | Nugget | Low with Exposure | 1.3 x 1.1 | CRM Group |
| 8572 | Gaspereau Lake Reservoir | Woodland period | Nodule | High | 1.1 x 2.0 | CRM Group |
| 8573 | Gaspereau Lake Reservoir | Woodland period | Nugget | Low with Exposure | 1.8 x 1.7 | CRM Group |
| 8574 | Gaspereau Lake Reservoir | Woodland period | Altered Nodule | Medium | 1.2 x 1.0 | CRM Group |
| 8576 | Gaspereau Lake Reservoir | Woodland period | Worked Nugget | Low with Exposure | 1.6 x 1.1 | CRM Group |
| 8577 | Gaspereau Lake Reservoir | Woodland period | Nodule | High | 1.3 x 1.4 | CRM Group |
| 8579 | Gaspereau Lake Reservoir | Woodland period | Nodule | Low | 2.0 x 1.5 | CRM Group |
| 8580 | Gaspereau Lake Reservoir | Woodland period | Nodule | Low | 3.1 x 2.7 | CRM Group |
| 8581 | Gaspereau Lake Reservoir | Woodland period | Nugget | High | 1.0 x 0.6 | CRM Group |
| 8582 | Gaspereau Lake Reservoir | Woodland period | Nugget | Mid | 1.5 x 1.2 | CRM Group |
| 8584 | Gaspereau Lake Reservoir | Woodland period | Nugget | Mid with Exposure | 0.9 x 0.7 | CRM Group |
| 8587 | Gaspereau Lake Reservoir | Woodland period | Nugget | High | 0.9 x 0.4 | CRM Group |
| 8589 | Gaspereau Lake Reservoir | Woodland period | Nugget | Mid | 1.7×1.0 | CRM Group |
| 8590 | Gaspereau Lake Reservoir | Woodland period | Nugget | High | 18 14 | CRM Group |
| 8501 | Caspercau Lake Reservoir | Woodland period | Nugget | High | 22 - 04 | CPM Group |
| 9507 | Caspercau Lake Reservoir | Woodland period | Nugget | Lon | 2.2 . 0.4 | CRM Group |
| 9502 | Caspercau Lake Reservoir | Woodland period | Worked Nugget | Low | 21 - 16 | CRM Group |
| 9504 | Caspereau Lake Reservoir | Woodland period | Worken Nugget | Mid | 12-09 | CRM Group |
| 0074 | Gaspereau Lake Reservoir | Woodland period | Warhad Name | Milu Tamaith Ennorma | 1.5 1 0.0 | CRM Group |
| 0500 | Gaspereau Lake Reservoir | woodland period | worked Nugget | Low with Exposure | 1.9 X 1.5 | CRW Group |
| 8590 | Gaspereau Lake Reservoir | woodland period | Nugget | Low | 1.0 X 1.0 | CRM Group |
| 8597 | Gaspereau Lake Reservoir | Woodland period | Worked Nugget | Mid | 4.1 x 2.9 | CRM Group |
| 8598 | Gaspereau Lake Reservoir | Woodland period | Nugget | High | 1.8 x 0.4 | CRM Group |
| 8599 | Gaspereau Lake Reservoir | Woodland period | Nodule | Low | 2.6 x 1.9 | CRM Group |
| 8603 | Gaspereau Lake Reservoir | Woodland period | Worked Nugget | High | 1.7 x 1.4 | CRM Group |
| 8604 | Gaspereau Lake Reservoir | Woodland period | Nugget | Mid | 2.0 x 1.2 | CRM Group |
| 8605 | Gaspereau Lake Reservoir | Contact period | Rolled Sheet | Low | 3.3 x 2.6 | CRM Group |
| 8606 | Gaspereau Lake Reservoir | Contact period | Rolled Sheet | Low | 4.3 x 2.7 | CRM Group |
| 86097 | Gaspereau Lake Reservoir | Contact period | Rolled Sheet | Low | 5.1 X 3.7 | CRM Group |
| 0000 | Cosperent Lake Reservoir | Woodland period | Worked Nugget | Low | 1.4 1 1.4 | CRM Group |
| 8610 | Gaspereau Lake Reservoir | Woodland period | Nugget | Mid with Exposure | 1.6 x 1.7 | CRM Group |
| 818 | Muskrat Cove | Woodland period | Preserved* Rolled she | et Mid | 18 × 07 | CRM Group |
| 810 | Muskrat Cove | Woodland period | Preserved* Rolled she | et Low | 46 - 26 | CPM Group |
| 820 | Muskrat Cove | Woodland period | Preserved* Nugget | Low | 16 - 08 | CRM Group |
| 921 | Muskrat Cove | Woodland period | Drosowod* Ard | Low | 10-02 | CRM Group |
| 922 | Muskrat Cove | Woodland period | Pressrued* Nugget | Livw | 14-12 | CRM Group |
| 044 | Sollows Cove | Woodland period | Mugget | Ligi | 1.4 1 1.5 | CRIVI Group |
| 950 | Sellars Cove | Woodland period | Nugget | Low | 4.3 X 4.1 | Steve Davis |
| 009 | Sellars Cove | Woodland period | Nugget | Low | 1.9 1 0.0 | Steve Davis |
| 803a | Sellars Cove | woodland period | Necklace beads | High | U./ X U.3 | Steve Davis |
| 8030 | Sellars Cove | woodland period | Necklace beads | High | 0.8 X 0.3 | Steve Davis |
| 19 | Burnt Bone Beach | Woodland period | Rolled Sheet | Low | 6.3 x 3.2 | Michael Deal |
| 20 | Burnt Bone Beach | Woodland period | Rolled Tinkling Cone | e Low | 6.1 x 1.5 | Michael Deal |
| 99 | Isle Haute | Woodland period | Nugget | High | 1.6 x 0.7 | David Christianson |
| 211 | Isle Haute | Woodland period | Nugget | High | 1.9 x 1.7 | David Christianson |
| 1949 | Enfield | Contact period | Rolled Sheet | Mid with Exposure | 2.1 x 1.0 | Steve Davis |
| 2015 | Enfield | Contact period | Rolled Sheet | Mid | 2.0 x 0.8 | Steve Davis |
| 2158 | Enfield | Woodland period | Worked Nugget | High | 2.2 x 1.4 | Steve Davis |
| 2225 | Enfield | Woodland period | Nugget | Low | 2.6 x 0.9 | Steve Davis |
| 5337 | Enfield | Woodland period | Nugget | Low | 1.3 x 1.0 | Steve Davis |
| 2 | Margaretsville | Woodland period | Worked Nugget | Low | 2.6 x 1.7 | John Erskine |
| 64 | Clam Cove | Woodland period | Nugget | Mid | 1.3 x 1.4 | Michael Deal |
| 21 | Clam Cove | Woodland period | Nugget | Low | 1.8 x 3.1 | Michael Deal |
| 230 | Clam Cove | Woodland period | Nugget | Mid | 2.4 x 1.9 | Michael Deal |
| 173 | Jeddore Harbour | Woodland period | Nugget | High | 1.0 x 2.1 | Michael Deal |
| Rlake | Rafter Lake | Woodland period | Worked Awl | Mid | 4.0 x 0.6 | Steve Davis |
| | | | | | | |

Table 1.1 Object descriptions of all copper artifacts in the collection belonging to the Nova Scotia Museum and CRM group.

*Preserved samples were treated with a solution of 5% B-72 in acetone prior to the commencement of this study ¹Note: not all artifacts listed were used in analyses

²Morphological artifact descriptions follow those detailed in Leonard (1996)

³Patina descriptions range from low coverage (0-30% of the artifact covered in thick green patina) mid coverage (31-60%) and high coverage (61-100%) any artifacts with exposure of fresh copper have been noted

⁴Age refers to suspected age of artifact using archaeological methods as per Cottreau-Robins, pers. comm. (2013)

| Mine | Host Rock | Deposit Type | County | State/Province | Country | Copper Produced (lbs) |
|------------------------------------------|------------------------------------------------------------------------------------------|-----------------------------------------------------------|------------------------------------------|--------------------|---------------|------------------------------|
| Phoenix | basaltic extrusive rocks and sediments ² | fissure vein ¹ | Keweenaw | Michigan | USA | 17 205 566* |
| Calumet | basaltic extrusive rocks and sediments ² | fissure vein ¹ | Keweenaw | Michigan | USA | 17 205 566* |
| Central Mine | conglomerate ² | fissure vein ¹ | Keweenaw | Michigan | USA | 17 205 566* |
| Copper Falls | conglomerate ² | fissure vein ¹ | Keweenaw | Wisconsin | NSA | 17 205 566* |
| Isle Royale | basaltic extrusive rocks and sediments ² | amygdaloid ore bodies ¹ | Houghton | Michigan | NSA | 254 632 779 ¹ |
| Osceola Mine | cambrian sediments ² | amygdaloid ore bodies ¹ | Houghton | Michigan | USA | 4 782 774 32 ¹ |
| White Pine | carbonaceous shale, siltstone, sandstone ³ | stratiform sedimentary ³ | Ontonagon | Michigan | NSA | 4 088 269 603 ⁹ |
| Greenstone Quarry | quartz | fissure vein ¹ | Adams County | Pennsylvania | USA | unknown |
| Corocoro | shale, sandstone, conglomerates ⁴ | vein ⁴ | N/A | Le Paz | Boliva | $200\ 000\ 000\ ^{4}$ |
| Itauz Mine | clastic redbed sequences ⁵ | stratiform sedimentary ⁵ | N/A | Dzhezkazgan | Kazakhstan | 207 452 860 000 ⁵ |
| Cap d'Or | basalt, carbonate quartz veins ⁶ | vein ⁶ | Cumberland | Nova Scotia | Canada | 12 320 10 |
| Margaretsville | basalt ⁷ | amygdaloid ore bodies ⁷ | Annapolis | Nova Scotia | Canada | 0** |
| Victoria Beach | basalt ⁷ | amygdaloid ore bodies ⁷ | Digby | Nova Scotia | Canada | 0** |
| Cornwall | metasediments ⁸ | veins ⁸ | N/A | Cornwall | England | 352 736 ¹¹ |
| 1. Broderick, 193 Bevins et al. 2010; | 1; 2. Butler & Burbank, 1929; 3. Brown, 19 9. Rosemeyer, 2010; 10. Messervey, 1929; 1 | 92; 4. Singewald & Berry, 1 1. Geological Survey of Gr | 992; 5. Box et al. eat Britain, 1846. | 2012; O'Reilly, 20 | 07; 7. Campb | ell, D.A., 1966; 8. |
| *Common tonnag | ie listed is representative of all of the copper | collected from all active mi | nes in the Keweel | naw Peninsula (K | osemeyer, 200 | (6 |
| | ысее печег рин шио ргоцисион (иллик, р | sts. comm. 2014) | | | | |

Table 1.2 : Descriptions of native copper sources



Figure 1.3 All artifacts used in this study from the Nova Scotia Museum. Inset: Artifact 8609.

2.0 Methodology

2.1 Sample selection and preparation

The samples used for this study comprised two different types: native copper samples, and archaeological copper-based samples. Native copper samples were purchased from private collections and sampled from larger specimens in the collections of the Nova Scotia Museum. Artifacts for this study were borrowed from the Nova Scotia Museum and come from collections that were discovered, assembled and characterized by provincial and private archaeologists Steve Davis, Michael Deal, Helen Sheldon, John Erskine and archaeology employees at Cultural Resources Management Inc. (Halifax) over a twenty year period (Cottreau-Robins, pers. comm., 2014). The collection includes artifacts from 6 different sites with various types of artifact morphology (e.g., shape and/or type of object, size, preservation) represented (Table 1.1, Figure 1.3). Morphological descriptions follow those detailed by Leonard (1993). Archaeological samples suspected or known to have been used for burial purposes or in burial ritual were excluded from this study.

2.1.1 Artifact copper

The archaeological samples were measured, catalogued and described prior to analysis using LA-ICP-MS. Owing to the size constraints of the laser ablation chamber, artifacts smaller than 2cm x 2cm x 2cm were selected to be analyzed with priority and larger artifacts were analyzed last with the maximum size possible being 6.1 cm x 3 cm x 0.1 cm. Samples ranged from worked nuggets to small decorative items such as tinkling cones and beads for necklaces, to fragments of rolled copper and copper-based alloy sheets of suspected European origin (Figure 1.3, Table 1.1). Artifacts larger than ~2.5 cm were carefully mounted in bricks of paraffin wax hollowed out to allow the artifacts to rest on

the brick and still be stable (Figure 2.1A). Samples smaller than ~2.5 cm were mounted in paraffin wax packing on top of, or within, the cores of drilled out cylindrical epoxy pucks (Figure 2.1B). This allowed for stabilization and levelling of the artifacts to be flush with the top of the surface of the sample holder to ensure that they were as close to the sampling cone (and within laser and optical focus) as possible, while still allowing for movement of the sample stage, but without risking damage to their brittle, patina-covered surfaces. In total, 60 artifacts were analyzed and only 57 artifacts being used in provenance determination as one was modern Zn metal, and two artifacts were too corroded for accurate analyses to be obtained (i.e., no fresh metal remaining at depth in the objects).

2.1.2 Natural copper source samples

A total of 38 samples of native (natural) copper samples were analyzed including multiple samples from single localities to allow assessment of site compositional homogeneity. Some of the samples came from private collections and others were accessed from the Nova Scotia Museum at the Museum of Natural History location. From each of the native copper samples, small fragments (<0.5 cm) were taken from each sample and mounted into epoxy pucks using Buehler Transoptic Powder, and a Buehler Simplimet 1000 Automatic Mount Press at Saint Mary's University. These pucks were then polished and ground down to expose fresh native copper without patina (Figure 2.1C).

2.1.3 Analytical standards

Five certified standards were used for data reduction (external calibration of analyte sensitivities) and quality control (e.g., inter-standard determination of analytical accuracy). Three copper standards from MBH Labs (United Kingdom; "residuals in refined copper" standard numbers 38X 27866, 39X 27869 and 39X 17872), as well as a silicate glass



Figure 2.1 Images of sample stages, mounts and ablation pits in copper artifacts. Photos courtesy of Dr. Catherine Cottreau – Robins, Nova Scotia Museum, and Dr. Jacob Haney, Saint Mary's University. A) Larger irregular artifacts in laser ablation chamber tray, mounted in paraffin wax. B) Smaller artifacts mounted in hollow epoxy pucks with paraffin wax holding each artifact in place. C) Three natural source samples of native copper mounted into an epoxy puck. D) SEM–BSE image of laser ablation pits in an artifact after ablation, showing fresh copper at depth (bright white) and corrosion products (patina) comprised of Cu-Fe-O-OH-Cl. E) SEM - SE image of ablation pits F) Enhanced SEM image of an ablation pit with melted copper flaring around the pit and surrounding ablation ejecta.

(SRM610) and a pressed sulfide powder pellet (MASS1) standard from NIST (National Institute of Standards and Technology) were utilized. Preliminary study of the ablation quality and composition of other certified reference materials, (e.g., NIST400; unalloyed copper VII) showed that while the samples were relatively homogeneous, the ablation characteristics of the samples were unusual, showing a lack of coupling of the laser with the sample and an inverse correlation between Cu isotope count rate and fluence. The reasons for this poor ablation behavior is unclear. Table 2.1 summarizes standards used for quantification of specific elements and Table 3.1 summarizes reported vs determined element concentrations for the respective standards.

2.2 Laser ablation ICP-MS method and data reduction protocol

2.2.1 Instrumentation and operating conditions

All artifacts used in this study were analyzed by LA-ICP-MS for trace elements at the University of New Brunswick, Department of Earth Sciences. The system used comprised a Resonetics RESOlution M-50 (193 nm Ar-F Excimer) with S-155 Laurin Technic Cell coupled to an Agilent 7700x quadrupole ICP-MS. Ablation was carried out at a fluence of \sim 4 J/cm². And at a repetition rate of 2.5 Hz with 10 measurements taken in each artifact or sample as a series of 90 µm-diameter pits (Figure 2.1 D-F). Ablation aerosols were transported to the ICP-MS using a He-Ar mixture (300 mL/min He, and 930 mL/min Ar). Complete analytical and data acquisition/reduction parameters are summarized in Table 2.1.

2.2.2 Quantification and data reduction schemes

Raw laser ablation data was reduced using the Iolite data reduction software package that runs in the Igor Pro compiler (version 6). Reference standard files were prepared from

Table 2.1: Table of LA-ICPMS operating conditions

| LA | |
|-----------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Model | Resonetics RESOlution M-50 with S-155 Laurin Technic cell |
| Wavelength | 193 nm |
| Pulse duration (FWHM) | 20ns |
| Repetition rate | 2.5 Hz |
| Spot diameter | 90 µm |
| Energy density | $\sim 4 \text{ J/cm}^2$ |
| Primary (calibration) standards | MBH39X27866, MBH39X27869, MBH39x17872, MASS1 |
| Secondary (QC) standard | MBH39X27866, MBH39X27869, MBH39x17872, MASS1 |
| ICP-MS | |
| Model | Agilent 7700x with dual external rotary pumps |
| Forward power | 1500W |
| Shield torch | |
| Sampling depth | 4.0 to 5.0 mm |
| Gas flows | |
| Carrier (He) | 300 mL/min |
| Make up (Ar) | 930 mL/min |
| ThƠ/Th ⁺ | <0.1% |
| Data acquisition and reduction paramete | rs |
| Dwell time per isotope | 15 ms |
| Detector mode | Dual mode |
| Data reduction software | Iolite platform on Igor Pro 6 |
| Internal Standard used | Cu wt% (assumed 99 wt% for all objects or determined |
| | for alloys) |
| Isotopes determined with standard 66 | ⁵⁶ Fe, ⁷² Ge, ¹⁹⁷ Au, ²⁰⁸ Pb, ²⁰⁹ Bi |
| Isotopes determined with standard 69 | ³¹ P, ³⁴ S, ⁵³ Cr, ⁵⁹ Co, ⁶⁰ Ni, ⁶⁵ Cu, ⁶⁶ Zn, ⁷¹ Ga, ⁷⁵ As, ¹⁰⁷ Ag, ¹¹¹ Cd, |
| | ¹¹⁵ In, ¹²¹ Sb, ¹²⁵ Te |
| Isotopes determined with standard 72 | ¹¹⁸ Sn |
| Isotopes determined with standard Mass | 1 ⁵⁵ Mn, ⁷¹ Ga, ⁹⁵ Mo, ²⁰² Hg |
| Quadrupole settling time | 5 ms |
| Analysis time | background (20s) abaltion (20s) washout (5s) |

certified element concentration data provided for each standard by MBH laboratories. Regularly during LA-ICP-MS measurements, standards (MBH copper standards SRM610 and MASS1) were analyzed to allow evaluation of analytical accuracy and precision, and the homogeneity of the standards. To do this, each standard was treated as an unknown sample and quantified using the other standards (e.g., MBH66 treated as unknown with its trace element concentrations quantified using MBH69 to calibrate analyte sensitivities). A full compilation of the inter-standard quality control exercise is summarized in Table 3.1. Raw data for blocks of 8-20 artifacts were quantified using each of the five standards. Then, a comparison of the resulting data was done in order to evaluate internal consistency. With the exception of a few elements that could only be quantified using MASS1 because they were not present in the MBH standards (e.g., Mn, Ga, Mo, Hg), all data reported were quantified using the MBH standards. No data are reported using the SRM610 standard for quantification due to matrix mismatch. Copper was used as an internal standard for quantification, and was set to 99 wt% Cu for all natural copper samples and artifacts (with the exception of some European-sourced artifacts.) For some artifacts suspected as not being ~pure Cu (European refined Cu-Sn-Zn alloys) based on their appearances on fresh surfaces, SEM-EDS spectra were obtained and quantified in order to determine the appropriate Cu concentration to use for quantification (e.g., artifacts 8606 [95.5 wt% Cu] 8607 [92.2 wt% Cu], 002 [97.03 wt% Cu] 8609 and 8605 [95 wt% Cu], 20 [95.24 wt% Cu] 19 [69.25 wt% Cu] 819 [83.60 wt% Cu] and 8604 [67.04 wt% Cu].) Since objects were variably coated in patina (Figure 2.1F) and the thickness of this patina could not be determined before analysis, signals were examined closely to identify maximum depth (in time of ablation) at which a patina of different composition occurred. This could be

identified readily in transient signals (Figure 2.2, 2.3) as the time during ablation at which point specific elements preferentially depleted (e.g., Ag) and enriched (e.g., Au, Mn) in the patina showed an increase or decrease, respectively, in measured isotope count rate to a relatively constant level (see portions of signal interval labelled "patina" and "fresh metal" in Figure 2.2C). Additionally, count rates for ⁶⁵Cu appeared to initially be low at the start of the signal and then rise but remain variable in the patina, followed by an interval of constant ⁶⁵Cu count rate (e.g., Figure 2.2C). The maximum duration of ablation that the transition from apparent patina to fresh metal was observed was approximately half of duration of the total ablation (~10s). On the basis of these criteria, ablation signals were reduced into two separate groups to generate a separate quantified data set for: (i) the shallow part of the ablation profile (patina) ablation time starting one second into ablation and ending ten seconds into ablation, and (ii) the deep part of the ablation profile (fresh metal), starting eleven seconds into ablation and ending one second from the end of ablation.

2.3 Data manipulation

Once the data was quantified for each of the two signal portions (shallow and deep), it was filtered for analyses below detection limits. Additionally, examination of the transient signals showed the presence of anomalous peaks ("spikes" in signal intensity) that likely represent contaminating mineral particles, present even in the fresh metal (Figures 2.2 and 2.3). During data reduction, many of these particles contributed to anomalously high reported concentrations for the ablation intervals quantified resulting in outliers within blocks of 8-10 analyses of each sample for some elements. Outliers were excluded, the remaining analyses were averaged and a standard deviation was calculated for each

element in each sample, and the results were then plotted into spider diagrams allowing a preliminary graphical determination of compositional similarities between artifacts. Artifacts with similar trace element chemistry were sorted into categories for comparison with natural source copper analyses.



Figure 2.2 Transient LA-ICP-MS signal (cps) vs time (s) for measured isotopes from three ablations of artifact 99 (suspected natural copper). Red arrows highlighting peaks in signal intensities. A) Cu, Cr, Mn, Fe, Ga, Hg, and Bi with Bi, Mn and Fe "spikes" highlighted. B) Cu, Zn, Sn, Sb, Te with Sb and Sn "spikes" highlighted. C) Cu, As, Ag, Au, and Pb, with Pb and Ag "spikes" highlighted. Also labelled in this frame are the interpreted intervals of patina (e.g., elevated ¹⁹⁷Au and ⁵⁶Mn, lower ¹⁰⁷Ag and low to variable ⁶⁵Cu) and fresh metal (e.g., where these isotope count rates drop rise and level out respectively.



Figure 2.3 Transient LA-ICP-MS signal (cps) vs time (s) for measured isotopes from three ablations of artifact 99 (suspected natural copper). Red arrows highlighting peaks in signal intensities. A) Cu, Cr, Mn, Fe, Ga, Hg, and Bi. B) Cu, Zn, Sn, Sb, Te with Sn and Te "spikes" highlighted. C) Cu, As, Ag, Au, and Pb, with Pb and Ag "spikes" highlighted. Relative to ⁶⁵Cu, many elements appear elevated in the first ~10s of the signal in the refined European copper, representing the patina coating.

3.0 Results

3.1 Analyses and comparisons of standards

The composition of the four key standards (three MBH copper standards; MASS1 sulfide) used in this study were compared to each other by setting one standard as analyte sensitivity calibrant against another standard as an unknown. The LA-ICP-MS data for each standard quantified by each of the other standards were compared to the reference certificates provided by MBH Laboratories and NIST to estimate analytical accuracy and standard homogeneity (Table 3.1), and to deduce which standard was the most appropriate to quantify each element in the artifacts. To further evaluate the feasibility of each standard for specific elements through a check for internal consistency, analyses of artifacts quantified by each standard were compared against each other (Figure 3.1). After careful scrutiny of the results attained for each standard, compared to the certified references, it was determined that each standard would only be appropriate to quantify specific elements as outlined below and in Table 2.1. Selection of the most appropriate standard for each individual element was based on selection of the standard yielding the greatest accuracy and precision for elements reported. Figure 3.1 shows comparison of analyses of two artifacts with very different trace element concentrations, one of suspected European origin (8604) and one of suspected North American (natural copper) origin (99), based on archaeological evidence (not this study). In this figure, comparison of quantified (mean of 10 analyses ± 2 s.d.) trace element concentrations by external calibrant 72 vs. 66, 69 vs. 66, and 72 vs. 69 are shown.

| Table 3.1 | Evaluat | tion of analyt | fical accuracy | v (values i | in ppm) utilizi | ing standards | MBH 38 | X 27866, 39X | 27869, and | 39X 17872 (1 | esiduals in coj | pper) and MAS | S1 (sulfide) |
|---------------|-------------------|----------------------|----------------------|-------------------|----------------------|----------------------|-------------------|----------------------|----------------------|----------------------|-------------------------|-------------------------|-------------------------|
| Element | 66 _{exp} | 66 _{ms(69)} | 66 _{ms(72)} | 72 _{exp} | 72 _{ms(66)} | 72 _{ms(69)} | 69 _{exp} | 69 _{ms(66)} | 69 _{ms(72)} | MASS1 _{exp} | MASS1 _{ms(66)} | MASS1 _{ms(69)} | MASS1 _{ms(72)} |
| P | 147 | 345 (1398, 76) | 229 (396, 66) | 45 | 29.9 (17.7, 42) | 228 (765, 75) | 119 | 133 (138, 66) | 185 (268, 70) | NC | ŊŊ | ŊŊ | ŊŊ |
| S | 469 | 150 (38.4, 61) | 302 (163, 63) | 242 | 373 (155, 46) | 119 (63.9, 61) | 112 | 351 (133, 56) | 223 (148, 68) | 276000 | 11861 (3671, 60) | 4089 (4681, 82) | 12137 (2810, 78) |
| C | 12 | 14.4 (105, 62) | ŊŊ | NC | ŊŊ | ŊŊ | 20 | 3.69 (9.81,49) | ŊŊ | 37 | 30.3 (49.9, 68) | 29.2 (49.1, 64) | δN |
| Mn | NC | δN | ŊŊ | 55 | ŊŊ | ŊŊ | NC | ŊŊ | ŊŊ | 260 | ŊŊ | ŊŊ | 727 (1337, 78) |
| Fe | 30 | 28.3 (64.1, 66) | 75.2 (210, 63) | 450 | 247 (187, 43) | 202 (196, 59) | 30 | 31.9 (77.5, 71) | 70.2 (231, 69) | 156000 | 92300 (91548, 64) | 99853 (71070, 58) | 404123 (317886, 78) |
| Co | 308 | 266 (98, 62) | 371 (107, 62) | 102 | 84.6 (8.93, 46) | 70.6 (25.5, 65) | 36 | 40 (14.5, 63) | 49.9 (23.5, 58) | 67 | 68.9 (5.91, 60) | 60.4 (12.6, 57) | 124 (19.6, 78) |
| N | 487 | 512 (372, 72) | 503 (42.2.57) | 537 | 530 (44.6. 45) | 559 (1458, 72) | 190 | 184 (12.9.54) | 190 (21.7, 68) | 61 | 102 (6.17, 64) | 106 (9.03, 58) | 163 (11.7.78) |
| Zn | 287 | 352 (119, 59) | 313 (235, 68) | 1070 | 1015 (150, 42) | 1289 (383, 60) | 65 | 49.7 (15.5, 64) | 55 (44.8, 69) | 207383 | 163028 (27675, 63) | 204503 (32115, 55) | 305401 (119551, 78) |
| Ge | 29 | 25.4 (6.03, 67) | ŊŊ | NC | ŊŊ | ŊŊ | 123 | 137 (13.8, 55) | ŊŊ | 50 | 85.5 (8.11, 58) | 76.7 (5.57, 58) | ŊŊ |
| As | 383 | 386 (57.1, 61) | 353 (105, 52) | 203 | 223 (63.5, 15) | 239 (118, 62) | 98 | 97.5 (8.27, 60) | 84.9 (24.8, 49) | 65 | 58.8 (3.60, 59) | 59.8 (3.99, 60) | 89.9 (15.1, 78) |
| Ag | 57 | 56.5 (11.4, 65) | 48.9 (43.4, 69) | 214 | 213 (28.5, 45) | 239 (93.1, 62) | 349 | 345 (24.7, 77) | 291 (309, 70) | 67 | 53.8 (2.49, 65) | 54.4 (2.96, 58) | 88.9 (45.3, 78) |
| Cd | 139 | 153 (40.4, 56) | 116 (64.6, 57) | 13 | 14.4 (10.2, 59) | 18.1 (23.4, 71) | 28 | 24.7 (3.76, 63) | 20.5 (11.4, 62) | 70 | 57.9 (9.84, 53) | 66.8 (11.6, 62) | 80.2 (23.5, 78) |
| In | 437 | 424 (144, 67) | 354 (129, 59) | 241 | 273 (101, 49) | 259 (143, 59) | 90 | 90.7 (14.9, 64) | 76.5 (29.2, 51) | 50 | 62.4 (3.31, 60) | 61.4 (7.31, 58) | 85.8 (16.3, 78) |
| Sn | 448 | 246 (691, 75) | 451 (786, 68) | 1800 | 1844 (1323, 58) | 1208 (1022, 44) | 106 | 925 (5516, 65) | 1672 (7943, 69) | 55 | 65.6 (10.4, 80) | 47.7 (29.8, 40) | 127 (59.8, 78) |
| Sb | 52 | 55.5 (112, 68) | 49.2 (51.7, 68) | 217 | 227 (90.7, 50) | 250 (98.1, 75) | 362 | 340 (34.1, 53) | 310 (366, 70) | 55 | 64.6 (3.78, 59) | 68.9 (5.78, 60) | 119 (63, 78) |
| Te | 32 | 49.4 (156, 67) | 52.1 (103, 63) | 208 | 273 (1612, 60) | 352 (1515, 72) | 153 | 92 (279, 71) | 129 (340, 68) | 21.1 | 7.22 (13.5, 74) | 14.6 (12.7, 63) | 20.1 (17.1, 78) |
| Ν | 16 | 17.2 (14.9, 68) | 26.2 (4.98, 54) | 15 | 8.79 (1.17, 39) | 9.63 (16.2, 70) | 80 | 74.8 (5.86, 56) | 122 (23.2, 56) | 47 | 62.9 (5.07, 65) | 67.7 (6.79, 62) | 169 (20.2, 78) |
| Pb | 54 | 47.2 (27, 55) | 35.9 (840, 69) | 2930 | 5365 (6765, 55) | 4775 (7457, 71) | 225 | 242 (122, 63) | 200 (5014, 70) | 80 | 63.2 (16.1, 59) | 60.1 (13.7, 61) | 302 (824, 78) |
| Bi | 47 | 52.1 (18, 55) | 37.7 (64.5, 68) | 240 | 350 (392, 51) | 389 (692, 71) | 376 | 321 (90.3, 58) | 233 (495, 69) | 99 | 40.9 (2.93, 56) | 49.5 (10.2, 59) | 65.3 (54.6, 78) |
| $^{1}NC = n0$ | value re | eported for th | hat standard; | NQ = n0 | of quantified (1 | not available | in standar | d as certified | I value) | | | | |

³Subscript exp = expected values for certified reference standard \mathbb{C}^{4} Subscript ms(XX) = measured values for certified reference standard treating as an unknown and quantifying it with another certified reference standard

²Values outside of brackets is average value based on 'n' analyses; values in brackets represent ±1 s.d. on the average value, and 'n' analyses



Figure 3.1 Comparisons of quantified concentrations of trace elements in copper artifacts using different standards for external calibration of analyte sensitivities. Each panel shows the concentration in ppm of trace elements quantified by the listed external standard, compared to that of the same artifact quantified by another external standard. The red line in each tile represents a linear relationship with a slope of 1. Data points show mean element concentration (10 analyses) \pm 2 s.d. on the mean value. A) Artifact 99, concentration of trace elements quantified by standard 72, vs those quantified by standard 66. B) Artifact 8604, concentration of trace elements quantified by standard 66. C) Artifact 99, concentration of trace elements quantified by standard 69, vs those quantified by standard 66. D) Artifact 8604, concentration of trace elements quantified by standard 69, vs those quantified by standard 66. F) Artifact 99, concentration of trace elements quantified by standard 69, vs those quantified by standard 66. F) Artifact 99, concentration of trace elements quantified by standard 69, vs those quantified by standard 66. F) Artifact 99, concentration of trace elements quantified by standard 69, vs those quantified by standard 66. F) Artifact 99, concentration of trace elements quantified by standard 69, vs those quantified by standard 66. F) Artifact 99, concentration of trace elements quantified by standard 72, vs those quantified by standard 69. F) Artifact 8604, concentration of trace elements quantified by standard 72, vs those quantified by standard 69. F)

By the methods discussed above, evaluation of the standard MBH 38X27866 (henceforth referred to as 66) proved that it was the most appropriate standard to use for Fe, Ge, Au, Pb, and Bi. Evaluation of the standard MBH 39X 27869 (henceforth referred to as 69) provide that it was the most adequate standard to use for P, S, Cr, Co, Ni, Zn, As, Ag, Cd, In, Sb, and Te. Evaluation of the standard MBH 39X 17872 (henceforth referred to as 72) proved that it was the most adequate standard to use for Sn. Overall, standard 69 proved to be the best with good ablation behavior and the majority of elements reporting the closest to the certified values, and was used for the majority of elements quantified in this study. Elements not quantified using standard 69, 66, or 72 were those that were not certified or even quantified from MBH Laboratories (Mn, Ga, Mo, and Hg) thus MASS01 was used. Other elements quantified by 66 and 72, were not inaccurately quantified by standard 69. Rather, they were just more accurately quantified by the other two standards. Notably, many elements were not being reported in standard 72 accurately (Table 3.1).

3.2 Comparison of patina and fresh metal composition, and sample homogeneity

Comparison of the first and last ~10 seconds of ICP-MS transient signals (Figure 3.2) allowed for the differences in composition of the altered surface patina and the fresh metal of the artifacts to be evaluated. Repeated analyses of four artifacts – two of "European" origin (8604 and 8606), and two of "North American" origin (99 and RLAKE) – were used for comparison of the composition of patina (corrosion products) and fresh (unaltered) copper or alloy.

Figure 3.2 shows that the majority of elements are reported in higher concentrations in the patina relative to the fresh metal. What is relevant from this comparison is analyses of patina, containing a lower concentration of Cu than fresh metal (due to the presence of Fe,



Figure 3.2 Comparison of trace element concentrations (ppm) in patina (y-axis; first 9 seconds of ablation profile) and core copper (x-axis; last 9 seconds of ablation profile). The red line represents a linear relationship with slope 1. Data points show mean element concentration (10 analyses) ± 2 s.d. on the mean value. A) Artifact 8604; B) Artifact 8606; C) Artifact 99; D) Artifact RLAKE.

P, H₂O and other elements forming the patina compounds), will overestimate trace element concentrations during data reduction. The exact wt% Cu content of weathering and corrosion products is unknown. Elements that are actually enriched in the patina relative to the fresh metal would be expected to show concentrations much higher (i.e., farther away from the 1:1 line) than those elements apparently enriched in the patina solely due to the overestimation of the Cu content of the patina during internal standardization in the data reduction. For example, in artifact 99 (Figure 3.2C) enrichments in Zn, Sn, Fe, As, and Au are seen in the patina, whereas elements such as S, Sb, Co, Ni, and Ge show increased concentration in the fresh metal. By evaluating ablation intervals for patina and fresh metal, one is able to evaluate if the patina is representative of the composition of the fresh metal underneath. If the same relative concentrations of trace elements are observed in the patina and fresh metal (i.e., elements are all over-reported by the same magnitude owing to uncertainty in patina composition) then patina analysis may still be appropriate for chemical provenance studies. However, if patina and fresh metal compositions show no systematic shift from one another, the patina is not representative. For this study, the former case held true and few objects showed variable enrichment or depletion in metals in the patina, with the exception of several of the artifacts comprised of refined copper and copper-based alloys from Europe. Ideally, analysis of the actual patina to determine its Cu content is preferred but this was not done in the present study. For this study it was not a requirement to use the patina data, as fresh metal was accessed during each ablation.

Understanding that many of the concentration relationships are similar in the patina of the artifact negates the requirement to drill into the artifact to expose fresh copper to determine provenance, reinforcing the value of this methodology over previously used bulk 27

analytical methods. European objects composed of alloys are clear exceptions to this, notably where they contain Zn. Dussubieux et al. (2008) showed a preferential depletion in Zn concentration in artifacts that were highly oxidized, weathered, and corroded, even in the fresh metal.

All of the artifacts and potential source samples were analyzed 8-10 times for statistical purposes as well to test sample homogeneity. These four artifacts had each ablation shot compared to the other nine shots of each respective artifact. Spider diagrams showing the individual (not mean) analyses of fresh metal in the same four artifacts used for the patina vs. fresh metal comparison can be found in Figures 3.3 and 3.4. Artifact 8604 shows minor variation in Sb, Mn, Cr and Te (< 20% relative variability). Artifact 8606 shows much larger variation from one shot to another (up to an order of magnitude variation) with the largest variations noted in Zn and Mn. However, the variations are systematic and the pattern of relative trace element concentrations is very similar from one shot to another across the entire variation in concentration. This may be expected for refined copper or copper-based alloy specimens that should not contain mineral inclusions but may show spatial variations in the purity of the metal or alloy. For naturally occurring copper, variations in trace element composition are expected to be less systematic from one analysis to another and can be attributed to inclusions of minerals that bear the variable trace elements in question (Figures 2.2, 2.3). Artifact RLAKE, for example, shows a much greater variability than artifact 99 and the variation in trace element concentration from shot to shot are very non-systematic in artifact RLAKE. Overall, while the analytical precision that partly reflects sample homogeneity is specific to each object, it was observed that for the majority of objects analyzed, trace element concentrations showed <30%28

variation from shot to shot (and typically no more than 20%), and where variation was observed it was systematic in natural copper artifacts, allowing for confidence in the degree of certainty for provenance assignment.

Standards, and all of the shots were averaged, approximately 40 shots per standard. Using the appropriate standard for quantification, as outlined in Table 2.1, it can be seen that the concentrations of elements for each standard reported in Table 3.1, are very close to the certified references, and that standards themselves, show good homogeneity using statistical means.

3.3 Source chemistry

Samples used for provenance evaluation came from six general locations: Nova Scotia, Canada; Michigan, USA; Pennsylvania, USA; Cornwall, UK; Bolivia and Kazakhstan. (Table 3.2, Figure 3.5). Elements that prove to be diagnostic of source locations are Fe, Ni, Zn, As, Mo, Ag, Pb, Cd, In, Sn, Sb, Te, Au, Hg, and Bi, with emphasis on the relationships between the concentrations of Ag and Pb; Hg and Bi; Zn and As; and in some cases the relationship between Sn, Sb and Te. Table 3.2 lists average concentration of all elements for each source location used in this study.



Figure 3.3 Comparison of the concentration of trace elements (ppm) determined for each individual laser ablation shot. A) Artifact 8604, good homogeneity. B) Artifact 8606 low homogeneity, variation between each shot.


Figure 3.4 Comparison of the concentration of trace elements (ppm) determined for each individual laser ablation shot. A) Artifact RLAKE, low homogeneity B) Artifact 99, moderate - high homogeneity.

3.3.1 Nova Scotia, Canada

Samples of Nova Scotian copper (figure 3.5A) were sampled from private collections and the Nova Scotia Museum collection. The private collection yielded sixteen samples of copper from Cap d'Or, and the samples from the Nova Scotia Museum yielded four samples from Margaretsville. Margaretsville copper samples contain on average higher Ag concentration (81.9 ppm) than Pb concentrations (0.059 ppm), moderately higher Hg (2.05 ppm) concentrations than Bi concentrations (0.516 ppm), and low Zn concentrations (0.534 ppm) compared to As concentrations (0.581 ppm). Cap d'Or samples contain moderate Zn vs As relationships (136 and 0.998 ppm respectively) (Table 3.1) lower Ag vs Pb (16.3 ppm vs 15.8 ppm respectively) and Hg (2.16 ppm) vs Bi (0.114) relationships. 3.3.2 Cornwall, UK

Source samples from Cornwall, UK (Figure 3.5 B) have high As vs Mo relationships (46.9 ppm vs 0.035 ppm) as well as a significantly higher Ag: Pb relationships (209 vs 0.067 ppm). It has the highest Ag concentration of the non- North American copper sources (Figure 3.5B). Copper from Cornwall also has been slightly enriched with Hg (4.74 ppm) in comparison to Hg found in coper from Bolivia (1.79 ppm) and Kazakhstan (2.36 ppm). 3.3.3 Michigan, USA

Samples from Michigan were collected from six different copper producing areas within the Great Lakes Region of North America (Figure 3.5C). Three from the Keweenaw

| England 151 (77.2, 16) 0.375 (0.195, 4) 0.547 (0.561, 6) 1.39 0.709 (0.372 0.709 (0.372 0.709 (0.004 (0.016, 6) 0.709 (0.266, 10) 4.6.9 (0.016, 6) 0.379 (0.266, 10) 4.6.9 | Kazakhstan 129 (22.6, 8) 1.75 (0.58, 4) 0.735 | United States | United States | Bolivia | Canada | Inited States |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|---------------|
| 151 (27.2, 16) (2.3.75 (0.195, 4) 0.547 (0.561, 6) 1.2.9 0.55 (0.195, 12) 0.709 (0.195, 12) 0.709 (0.195, 12) 0.709 (0.195, 12) 0.709 (0.265, 10) (0.265, 10) (15.2, (16) | 129 (22.6, 8) 1.75 (0.58, 4) 0.735 | | | | | Omen Diates |
| (2.7.2, 16) (0.1355 (0.1955, 4) 0.547 (0.561, 6) 1.39 (0.879, 9) 0.016 (0.009, 5) 0.016 (0.1955, 12) 0.729 (0.195, 12) 0.726 (0.016, 6) 0.379 (0.266, 10) 4.6.9 (15.2, (16) | (22.6, 8) 1.75 (0.58, 4) 0.735 | 149 | 117 | 153 | 142 | 151 |
| (0.375 (0.575 0.547 0.547 (0.561, 6) 1.39 1.39 (0.879, 9) 0.016 (0.009, 5) 0.016 (0.195, 12) 0.024 (0.016, 6) (0.024 0.022 0.0224 (0.016, 6) (0.026, 10) (0.266, 10) (15.2, (16) | 1.75 (0.58, 4) 0.735 | (25.0, 16) | (17.9, 16) | (14.2, 8) | (17, 32) | (23.4, 8) |
| (0.195, 4) 0.547 (0.561, 6) 1.39 0.016 (0.009, 5) 0.016 (0.195, 12) 0.212 0.222 0.222 0.224 (0.016, 6) 0.379 0.379 0.379 (0.016, 6) (0.026, 10) 4.69 | (0.58, 4) 0.735 | 0.213 | 0.234 | 0.325 | 0.845 | 0.12 |
| 0.547 0.561, 6) 1.39 0.51, 6) 0.879, 9) 0.099, 5) 0.212 0.709 0.709 0.709 0.709 0.709 0.709 0.709 0.709 0.709 0.709 0.709 0.709 0.709 0.709 0.709 0.709 0.716 (0.165 0.716) 0.716 (0.165 0.716) 0.716 (0.165 0.716) 0.716 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717 (0.165 0.717) (0.179 0.717 (0.165 0.717) (0.179 0.717 (0.165 0.717) (0.165 0.717) (0.165 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175 0.717) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) (0.175) | 0.735 | (0.134, 8) | (0.12, 7) | (0.287, 4) | (0.323, 11) | (0.066, 3) |
| (0.561, 6) 1.39 (0.879, 9) 0.016 (0.195, 12) 0.705 0.712 0.725 0.725 0.726 0.726 0.379 0.379 (0.016, 6) 0.379 (15.2, (16) (15.2, (16) | | 0.654 | 0.588 | 0.984 | 0.417 | 0.65 |
| 1.39 (0.879, 9) 0.016 (0.009, 5) 0.212 0.212 (0.195, 12) 0.212 (0.195, 12) 0.224 (0.016, 6) 0.379 (0.266, 10) (15.2, (16) | (0.388, 6) | (0.323, 5) | (0.469, 10) | (0.609, 7) | (0.374, 19) | (0.495, 2) |
| (0.879, 9) 0.016 0.016 0.009, 5) 0.212 0.212 0.212 0.224 0.024 0.024 0.024 0.024 0.379 0.379 0.379 (15.2, 10) | 0.2 | 2.43 | 0.504 | 8.32 | 0.746 | 3.53 |
| 0.016 (0.009, 5) 0.212 0.195, 12) 0.709 0.709 0.724 (0.016, 6) 0.379 0.379 0.379 0.379 (15.2, (16) | (0.141, 2) | (1.74, 7) | (0.421, 8) | (11.6, 8) | (0.607, 19) | (3.45, 3) |
| (0.009, 5) (0.195, 12) 0.709 (0.532, 8) (0.266, 10) 0.379 0.379 (152, (16) (152, (16) | 0.028 | 0.08375 | 0.084 | 0.011 | 0.014 | 0.05 |
| 0.212 0.709 0.709 0.723, 8) 0.024 0.024 0.016, 6) 0.266, 10) 46.9 (15.2, (16) | (0.024, 6) | (0.075, 8) | (0.069, 10) | (0.006, 6) | (0.015, 21) | (0.036, 3) |
| (0.195, 12) 0.709 0.709 0.023, 8) 0.024 0.016, 6) 0.379 0.379 (0.266, 10) (15.2, (16) | 0.168 | 0.535 | 0.645 | 0.345 | 0.58 | 0.445 |
| 0.709 0.532,8) 0.024 0.016, 6) 0.379 (0.266, 10) 46,9 (15,2, (16) | (0.089, 4) | (0.625, 4) | (0.275, 6) | (0.172, 4) | (0.712.25) | (0.078, 2) |
| (0.532, 8) 0.024 (0.016, 6) 0.379 (0.266, 10) 4.6.9 (15.2, (16) | 0.445 | 0.257 | 0.197 | 0.456 | 0.534 | 0.288 |
| 0.024 (0.016, 6) 0.379 (0.266, 10) 46.9 (15.2, (16) | (0.601, 2) | (0.183, 13) | (0.149, 10) | (0.601, 5) | (0.407, 24) | (0.309, 5) |
| (0.016, 6) 0.379 (0.266, 10) 46.9 (15.2, (16) | 0.043 | 0.099 | 0.122 | 0.018 | 0.009 | 0.05 |
| 0.379 (0.266, 10) 46.9 (15.2, (16) | (0.034, 5) | (0.063, 7) | (0.087, 10) | (0.015, 5) | (0.013, 20) | (0.036, 3) |
| (0.266, 10) 46.9 (15.2. (16) | 0.61 | 0.501 | 0.511 | 0.495 | 0.443 | 0.52 |
| 46.9 (15.2, (16) | (0.274, 4) | (0.431, 10) | (0.198, 9) | (0.373, 4) | (0.379, 15) | (0.337, 3) |
| (15.2, (16) | 0.55 | 26.1 | 10.5 | 0.528 | 0.581 | 8.51 |
| | (0.212, 7) | (14.9, 16) | (1.75, 16) | (0.219, 6) | (0.566, 28) | (1.88, 8) |
| 0.035 | 0.094 | 0.126 | 0.117 | 0.015 | 0.004 | 0.22 |
| (0.021, 6) | (0.009, 2) | (0.113, 11) | (0.066, 10) | (0.011, 4) | (0.011, 23) | (0.142, 4) |
| 310 | 79.6 | 205 | 56.9 | 1.85 | 81.9 | 104 |
| (74.7, 16) | (40.4, 8) | (39.8, 16) | (39.9, 16) | (0.968, 8) | (31.1, 32) | (20.6, 8) |
| 0.035 | 0.033 | 0.068 | 0.051 | 0.048 | 0.014 | 0.051 |
| (0.038, 6) | (0.029, 4) | (0.062, 10) | (0.033, 11) | (0.033, 5) | (0.027, 21) | (0.054, 4) |
| 0.005 | 0.015 | 0.005 | 0.006 | 0.011 | 0.008 | 0.003 |
| (0.005, 7) | (0.006, 4) | (0.003, 8) | (0.005, 9) | (0.007, 4) | (0.009, 31) | (0.001, 3) |
| 0.038 | 0.065 | 0.04 | 0.036 | 0.059 | 0.063 | 0.018 |
| (0.027, 12) | (0.038, 6) | (0.031, 9) | (0.033, 9) | (0.045, 7) | (0.052, 30) | (0.013, 5) |
| 0.067 | 0.069 | 0.052 | 0.068 | 0.155 | 0.05 | 0.298 |
| (0.037, 9) | (0.073, 2) | (0.034, 11) | (0.034, 10) | (0.083, 4) | (0.039, 19) | (0.108, 8) |
| 0.014 | 0.033 | 0.23 | 0.087 | 0.07 | 0.11 | 0.04 |
| (0.012, 5) | (0.026, 4) | (0.38, 8) | (0.075, 12) | (0.014, 2) | (.094, 22) | (0.00, 2) |
| 0.00 | 0.00 | 0.012 | 0.005 | 0.00 | 0.001 | 0.004 |
| (0.00, 16) | (0.00, 3) | (0.012, 6) | (0.004, 6) | (0.00, 5) | (0.001, 32) | (0.002, 4) |
| 4.59 | 2.36 | 3.62 | 2.26 | 1.79 | 2.05 | 1.35 |
| (0.578, 16) | (0.543, 8) | (6.68, 16) | (1.27, 16) | (0.352, 8) | (0.413, 32) | (0.243, 8) |
| 0.021 | 0.036 | 0.007 | 0.008 | 0.156 | 0.059 | 0.016 |
| (0.012, 8) | (0.023, 5) | (0.005, 8) | (0.006, 13) | (0.227, 7) | (0.039, 26) | (0.008, 7) |
| 0.006 | 0.017 | 0.005 | 0.005 | 0.041 | 0.516 | 0.028 |
| (0.005, 9) | (0.01, 8) | (0.003, 9) | (0.005, 7) | (0.038, 5) | (0.978, 29) | (0.028, 8) |
| | (0.023) (0.027, 12) (0.027, 12) (0.037, 9) (0.012, 5) (0.012, 5) (0.012, 5) (0.012, 6) (0.00, 16) (0.0012, 8) (0.005, 9) | (0.037, 12) (0.038, 6) 0.038 0.065 0.057 0.069 0.067 0.069 0.014 0.053 0.014 0.035, 4) 0.014 0.035, 3) 0.014 0.035, 4) 0.014 0.036 0.00 (0.012, 5) 0.00 (0.00, 3) 4.59 2.36 0.031 0.00 0.031 0.00 0.032 10.00, 3) 4.59 2.36 0.032 0.036 0.031 0.036 0.032 0.036 0.041, 8) 0.011, 8) | 0.003 0.005 0.004 0.067 0.065 0.043 0.067 0.068 0.031, 9) 0.067 0.069 0.052 0.067 0.038, 6) 0.031, 9) 0.067 0.038, 6) 0.032 0.014 0.033 0.033, 11) 0.014 0.035 0.033, 11) 0.016 0.036 0.032 0.00 0.003 0.23 0.012, 6) 2.36 3.62 0.021, 6) 0.035, 8) 0.007 0.021 0.035, 9) 0.007 0.021 0.035, 6) 0.007 0.021, 8) 0.035, 5) 0.005, 8) 0.005 0.012, 5) 0.005, 8) 0.005 0.011, 8) 0.005, 8) | (0.027, 12) (0.033, 6) (0.031, 9) (0.033, 6) (0.033, 6) (0.033, 9) 0.067 0.068 0.062 0.044 0.036 0.036 0.067 0.069 0.052 0.032 0.0368 0.0368 0.0368 0.067 0.0369 0.052 0.034, 10 0.0343, 10 0.0368 0.012 0.037, 9) 0.0173, 2) (0.034, 10) 0.0341 0.0368 0.012 0.033 0.032 0.238, 8) 0.0375, 12) 0.0341 0.010 0.012 0.033 0.012 0.0365 0.0065 0.00 0.012 0.012, 6) (0.045, 6) 2.266 2.266 0.012 0.005, 8) (0.05, 8) (0.005, 8) 0.006 13) 0.005 0.005, 8) (0.005, 8) (0.005, 8) 0.006 13) 0.005 0.005, 9) (0.012, 6) (0.005, 3) 0.006 13) | | |



Figure 3.5 Trace element discrimination diagrams showing elemental concentrations (ppm) for all source samples of native copper. These samples were not reduced by their respective concentrations of copper as we knew they were natural native copper that had not been smelted. A) Nova Scotian copper from Cap d'Or and Margaretsville locations. B) Copper from Cornwall, UK. C) Michigan copper showing six samples taken from six different copper producing mines located in three different copper counties. D) Bolivian Copper. E) Pennsylvanian copper from Adam's County F) Copper from Kazakhstan.

County (Phoenix Mine, Central Mine and Copper Falls), two from Houghton County (Isle Royale, and Osceola Mine), and one from the Ontonagon County (White Pine Mine). Many of the trace element signatures for all of the Michigan samples were consistent amongst the other samples, with notably high Ag (56.9 - 205 ppm) low Pb (0.007 - 0.016 ppm), moderate (1.35 - 3.62 ppm) and low Bi (0.005 - 0.028 ppm). Significantly different from the Nova Scotian samples, the Michigan copper shows an enrichment in As (8.51 - 26.1 ppm) with respect to Zn (0.197 - 0.288 ppm) whereas Cap d'Or samples have slightly higher concentration of Zn compared to As, and Margaretsville samples have a moderately lower concentrations of Zn than As. Michigan samples show homogeneity and consistency between each of the samples (Figure 3.5C) however some variation exists in the concentration of Zn, Sn, Sb, and Te, between all of the different mines, which given enough analyses of artifacts from that location, could give us knowledge on exactly which mine or deposit the aboriginal peoples were procuring their copper.

3.3.4 Bolivia

Bolivian copper from Le Paz, has a very limited concentration of trace elements. Relative to the other sources used in this study, Bolivian copper is nearly pure (Figure 3.5 D). The greatest enrichments are found in Ag and Hg, however they are not enriched to the same scale as compared with the North American samples. Hg and Ag on average are only present in concentrations of 2.36 and 79.6 ppm respectively in Bolivian copper, whereas in the North American samples, Ag, Hg and Pb can get into the hundreds of ppm level, showing more impurities in the sources from North America.

3.3.5 Pennsylvania, USA

Copper from Adam's County, Pennsylvania (Figure 3.5E), had trace element chemistry similar to those of Michigan in terms of overall trace element signatures, with the exception of select elements, for example As and Mo. Pennsylvanian copper has As concentrations in the range of hundreds of ppm with the average concentration being 392 ppm, and Mo concentrations so low that the average concentration is 0.007 ppm. In the copper samples from Michigan, As concentrations only range between 8.51 and 26.1 ppm and Mo concentrations in Michigan range between 0.117 and 0.220 ppm. Another exception is the Pb to Cd relationships. In Michigan samples, the concentration of Pb is lower than that of Cd (0.007 - 0.016 ppm Pb vs 0.051 - 0.068 ppm Cd). Pennsylvanian samples show a higher Pb concentration than that of Cd, 0.067 and 0.006 ppm respectively.

3.3.6 Kazakhstan

Copper from Kazakhstan (Figure 3.5F) is similar to that of Bolivia, as both samples do not contain high concentrations of impurities via trace elements. The copper samples from Kazakhstan also contain enrichments of Ag and Hg, however they are more concentrated than the impurities in Bolivia with the average concentration of Ag being 79.6 ppm and Hg being 2.36 ppm.

3.4 Artifact chemistry

A total of fifty seven artifacts, (Figures 3.6, 3.7, 3.8; Table 3.3) of the collection of sixty, were analyzed for this study. Artifacts 218, 818 and 82, were excluded from further comparisons with copper sources, as it was determined that these sources were modern metal alloys containing abundant Zn, Fe and Sn and originating with gun metals and Cu-Zn-Sn alloys from the 1900s. Each of the artifacts were sorted into a specific provenance

group based on their trace element signatures. For this study, provenance determination was based on the concentration of Fe, Ni, Zn, As, Mo, Ag, Pb, Cd, In, Sn, Sb, Te, Au, Hg and Bi, relative to each other in a given artifact. Emphasis was placed on the relationships between Ag and Pb, Hg and Bi, and Zn and As. To further sub-divide, some artifacts were separated based on the concentration of Sn vs the concentration of Sb, however that separation is not required. Using these element concentration relationships, ten artifact groupings are created.

3.4.1 Group I

Group one is the collection of artifacts that are not pure native copper and in fact are either alloys or smelted copper with high Fe impurities. When reduced by Fe, these artifacts show enrichments in Zn, Ag, Pb, In, Sb, Au, and Bi. Significant differences that set the group one artifacts (2, 19, 20, 819, 8604, 8605, 8606, 8607, and 8609) apart from the others is the presence of an enrichment (relative to other elements) of Au in these artifacts. Au is present in these artifacts between 0.91 ppm to 470.9 ppm which is a much wider range and higher concentrations than the other provenance groups. Notable differences in elements exist in As (range between 177 and 10140 ppm), Te (0.05 and 64.12 ppm), and Hg (0.032 and 1366 ppm) (Figure 3.6A & B) which means that while we can safely assume that these artifacts are very similar in origin, there is some variation among the exact provenance of each copper artifact, or the smelting techniques that went into making them. For further details see Hodge et al. (in prep.)



Figure 3.6 Discrimination diagrams for the first four provenance groupings. A) Group I – not reduced by iron B) Group I – reduced by iron C) Group II – not reduced by iron D) Group II – reduced by iron E) Group III – not reduced by iron F) Group III – reduced by iron G) Group IV – not reduced by iron H) Group IV – reduced by iron.



Figure 3.7 Discrimination diagrams of groups V, VI and VII A) Group V – not reduced by iron B) Group V – reduced by iron C) Group VI – not reduced by iron D) Group VI – reduced by iron E) Group VII – not reduced by iron F) Group VII – reduced by iron.



Figure 3.8 Discrimination diagrams of the last three provenance groupings. A) Group VIII – not reduced by iron B) Group VIII – Reduced by iron C) Group IX – not reduced by iron D) Group IX – reduced by iron E) Group X – not reduced by iron F) Group X – reduced by iron.

| Table 3.3 Ave | rgage concentra | tion (ppm) of all : | artifacts used i | n this study | ٨ | | | | | | | | | | | | | | | | | | | | |
|----------------------------|---------------------|---------------------|--------------------|--------------|------------|------------|----------------------|---------------|--------------|------------------|-------------|-------------|---------------------------------------|-------------|-------------|----------------------|-------------|---------------------|---------------|-----------------------------------------|----------------------|-----------------|-----------------------------|----------------------|----------|
| Planate | 19 | 20 | 21 | 2 | 230 | 1949 | 2015 | 2158 | 2225 | 5377 | 8566 | 8567 | 8568 | 8569 | 8572 | 8573 | 8574 | 8576 | 8577 | 8579 | 8580 | 8581 | 1582 8 | 584 8 | 1587 |
| Frement B. | urnt Bone Beach | Burnt Bone Beach | I Clam Cove | Clam Cove | Clam Cov | e Enfiels | I Enfield | Enfield | Enfield | Enfield | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR 6 | ILR O | TLR |
| v | 238 | 382 | 31101 | 483 | 206 | 227 | 199 | 176 | 211 | 163 | 849.70 | 295 | 169 | 214.00 | 485 | 201 | 1203 | 131 | 261 9 | 440.00 | 260 | 6.68 | 261 58 | 8.00 | 245 |
| 5 | (65.7, 8) | (131, 10) | (97643, 10) | (340, 9) | (31.9, 10) | (24.5, 1 | 0) (46.6, 10 | (11.6, 10) | (31.8, 10) | (15.1, 10) | (346, 10) | (53.8, 10) | (30.5, 10) (| 33.3, 10) | (127, 10) | (73.4, 10) | (1217, 10) | (15.5, 10) (6 | 2.1, 10) (3 | 647, 10) (3 | 53, 10) (2 | 4.8, 10) (7 | (9, 10) (23 | 3, 10) (49 | .8, 10) |
| გ | (103.8) | (507, 10) | (3222.8) | (906.9) | (98.8.10) | 24.8.1 | 0) (285.10) | 9.50 | (164, 10) | (118, 10) | (1325, 10) | (1122.10) | 1997 | 2.59.10) | (194, 10) | (242, 10) | 0430 | 164,100 (1. | 8.2.10) (11 | 588.10) (| 29.10) (2 | 4.96 | 01.10 01.79 M4.10) (29 | 6,10) (31 | 4.10) |
| M | 1.32 | 0.81 | 56 | 3.51 | 66.8 | 37.3 | 0.74 | 0.205 | 0.73 | 0.732 | 20.10 | 1.47 | 1.21 | 1.63 | 2.36 | 9.56 | 20.3 | 0.73 | 16.0 | 1016 | BDL | 1.12 | 6 6 | .88 | 5.64 |
| | (1.03, 8) | (0.461, 10) | (155, 8) | (7.49, 9) | (61.9, 10) | (21.2, 3 | (1.62, 10 | (0.104, 9) | (0.535, 10) | (0.987, 10) | (11.2, 10) | (0.649, 10) | (0.772, 10) | (1.79, 7) | (0.786, 10) | (7.11, 10) | (15.7, 10) | 0.599, 10) (0. | 774, 10) (3 | 19, 10) | BDL (0. | 476, 10) (3 | (8, 10) (2.2 | 5, 10) (4. | 1, 10) |
| Fe | (13579, 8) | (27717, 10) | 3/408 (115462, 10) | (4622, 9) | 076766, 10 | 080 | 0) (2951,10 | (18.4, 10) | (534, 10) | (715, 10) | (11018, 10) | (439, 10) | (567, 10) (| 147, 10) | (130, 10) | 1028 (1289, 10) | (60375, 10) | (46.2, 10) (1) | 667, 10) (11' | 7643, 10) (0 | 925, 10) (3 | 132, 10) (1: | 93, 10) (38 | 2.10) (44 | 13, 10) |
| č | 15.9 | 17.9 | 168 | 3.52 | 1.63 | 0.23 | 0.649 | 0.059 | 0.37 | 0.261 | 3.80 | 0.82 | 0.154 | 0.06 | 0.325 | 0.286 | 6.24 | 0.06 | 1.09 | 623 | 0.311 | 0.305 | 1.67 2 | 30 0 | 345 |
| 3 | (7.75, 8) | (10.8, 10) | (473, 8) | (6.62, 9) | (0.836, 10 | (0.369, | 7) (1.40,5) | (0.076, 8) | (0.223, 10) | (0.289, 9) | (3.26, 10) | (0.444, 10) | (0.149, 9) () | 0.062, 7) | (0.347, 10) | (0.365, 10) | (6.09, 10) | (0.037, 9) (0. | 979, 10) (2 | 8.6, 10) (0 | .082, 10) ((| 0.32, 9) (0. | 49, 10) (6. | 26, 9) (0.5 | 02, 10) |
| IN | 195 | 570 | 1332 | 10.6 | 1.92 | 1.07 | 1.16 | 0.652 | 1.67 | 1.96 | 13.31 | 8.60 | 0.816 | 0.52 | 1.62 | 4.7 | 37.7 | 131 | 1.68 | 246 | 1.73 | 0.639 | 10.4 | 42 0 | 946 |
| | (99.1, 8) 355562 | (203, 10) | (3514, 7) 807 | (20.9, 9) | (1.67, 10 | 1001 | () (2.73, 8) 60.5 | 33.1 | (0.758, 10) | (01,235,10) | 717.80 | 205 | 33.7 | 1.62 | (11.29, 10) | (01,5.15, 10) 296 | (30.5, 10) | (1.15, 8) (19.2 | 7.9 (8,91.1 | 921.00 (0 | .041, 10) (0 60.9 | 28.9 (4 | 19, 10) (12 558 2 | 5, 10) (0.5 | 78.8 |
| Zn | (174809, 8) | (121070, 10) | (2492, 10) | (159, 9) | (44.4, 10) | (62.4,1 | 0) (41.4, 10 | (11.9, 10) | (92.3, 10) | (113, 10) | (307, 10) | (54.6, 10) | (19.7, 10) (| (01, 2, 10) | (77.3, 10) | (151, 10) | (1003, 10) | (18.9, 10) (5 | 43, 10) (1) | 852, 10) (0 | 0.4, 10) (2 | 14,10) (2 | 6,10) (13 | 6, 10) (32 | .1, 10) |
| 2 | 3.03 | 1.95 | 52 | 2.91 | 1.95 | 0.423 | 0.32 | 0.157 | 1 | 0.88 | 9.65 | 3.56 | 1.14 | 0.204 | 1.24 | 1.01 | 27.9 | 0.149 | 169.0 | 175 | 141 | 0.856 | 3.25 5 | 44 | 181 |
| 5 | (2.02, 8) | (0.581, 10) | (145, 8) | (4.93, 9) | (0.609, 10 | 0.333,1 | 0) (0.542, 10 | (0.024, 10) | (0.653, 10) | (0.751, 10) | (6.61, 10) | (1.95, 10) | 0.693, 10) (0 | 0.127, 9) | (0.609, 10) | 0.716, 10) | (26.7, 10) | (0.104, 8) (0. | 589, 10) (8 | 2.4, 10) ((| 0.46, 10) (0. | 446, 10) (1 | 42, 10) (2.8 | (5, 10) (0.9 | 63, 10) |
| Ge | UL 175 W | 1011 | 10 201 | 0 880 0J | 01.10 | 101.02 | 3 341 00 10 | 00110 0 | 01 345 0 | C/770 | 012 10 | (0.465 10) | 0 10 201 0 | -100 | 0 303 10) | 0 206 101 | 101 96 91 | 0 13 151.0 | 201 101 102 | 31 100 0 | 115 01 0 | 11 18 80 1 | 101 03 101 03 3 | 200 UL 30 | 0 161 |
| 1 | 512 | 917 | 358 | 8108 | 50.4 | 5.6 | 1.82 | 0.972 | III | 96.9 | 23.75 | 13 | 8.52 | 124 | 6.35 | 60.6 | 112 | 0.75 | 23 | 128 | 154 | 9.26 | 10.9 2 | 5.7 | 8.6 |
| VS | (226, 8) | (210, 10) | (1145, 9) | (62.9, 9) | (17.9, 10) | (3.88, 1) | 0) (1.40, 10 | (0.342, 10) | (3.47, 10) | (4.33, 10) | (14.4, 10) | (5.03, 10) | (5.48, 10) (| 1.16, 10) | (3.42, 10) | (5.78, 10) | (232, 10) | 0.161, 10) (3 | .46, 10) (2 | 23,10) ((| .48, 10) (5 | (11, 10) (4 | 75, 10) (5.9 | 3, 10) (3.0 | 61, 10) |
| Ma | 0.513 | 0.58 | 27.5 | 0.881 | 3.17 | 0.183 | 0.121 | 0.201 | 0.52 | 0.245 | 1.37 | 0.26 | 117 | 0.24 | 0.23 | 0.242 | 1.24 | 0.14 | 3.31 | 6.40 | 0.185 | 0.268 | 0.45 0 | 54 0 | 122 |
| | (0.234, 7) | (0.26, 10) | (71.6, 7) | (0.432, 9) | (1.13, 10) | 0.188,1 | 0) (0.063, 10 | (0.129, 10) | (0.484, 10) | (0.304, 10) | (1.86, 10) | (0.197, 10) | (0.079, 10) (0 | (192, 10) | (0.222, 7) | (0.12, 9) | (0.972, 10) | 0.062, 10) (5 | .12, 10) (3 | .45, 9) (0 | .096, 10) (0 | .106, 9) (0. | 28, 10) (0.6 | 74, 10) 0.1 | 23, 10) |
| Ag | 629.00 | 485 | 450 | 26.1 | 8.02 | 282 | 248 | 232 | 80.6 | 220 | 134.70 | 246 | 86.9 | 254.00 | 179 | 201 | 273 | 256 | 54.7 | 226 | 2.7 4 | 494.00 | 11 01 0 | 457 | 488 |
| , | (113, 8) | (11) | (884, 10) | (21.0, 9) | (1.69, 10 | 0 (351, 1 | 0) (88.7, 10 | 0 (121, 10) | (33, 10) | (15.5, 10) | (33.2, 10) | (224, 10) | (37.7, 10) (| 0136 | (13.7, 10) | 0 407 | (139, 10) | (178, 10) (2 | 7.6, 10) (6 | 0) (01,11) (0 | 0.746 | 0 167 (1) (1 | | 47, 10) (24 | 10, 10) |
| Cd | (0.663, 8) | (0.452, 10) | (53.7, 10) | (6.966.0) | (0.483, 10 | 1.111.0) (| 0) (0.184, 10 | (0.282.10) | (0.547, 10) | (0.217.10) | (1.34, 10) | (0.481.10) | 0.068, 10) () | 0.121.9) | 0.225, 10) | 0.293, 10) | (07.10) | 0.061.7) (0. | 042.10) (3 | 86, 10) (0 | 086, 10) (0 | (185.9) (7 | 39, 10) (0.4 | 36, 10) (0.4 | 42, 10) |
| ę | 17.5 | 109 | 0.722 | 160.0 | 0.228 | 0.004 | 0.005 | 0.003 | 0.196 | 0.059 | 2.86 | 0.041 | 0.07 | 0.466 | 0.112 | 0.009 | 0.126 | 0.004 | 0.005 | 1.15 | 0.018 | 0.541 | 372 0. | 273 0 | 055 |
| • | (4.09, 8) | (39.5, 10) | (1.88, 7) | (0.095, 8) | (0.173, 10 | (0.002, | 7) (0.004,7 | (0.002, 8) | (0.268, 10) | (0.131, 10) | (6.49, 10) | (0.047, 10) | (0.117, 9) (| (1.03, 5) | (0.164, 9) | (0.006, 10) | (0.114, 10) | (0.002, 7) (6 | .001, 8) (0. | 559, 10) (0 | .011, 10) () | 1.12, 8) (0. | 94, 10) (0.6 | 00' (8'66) | 078, 9) |
| Sn | 801 | 21155.00 | 12 | 13.1 | 0.83 | 0.134 | 0.264 | 0.397 | 1.79 | 0.277 | 8.58 | 2 101 | 0.45 | 0.311 | 0.875 | 1.09 | 16.6 | 0.281 | 0.317 | 170 | 1.45 | 3.05 | 10 101 01 | .12 0 | 152 |
| t | 201 | (01 ,2007) 433 | 30.1 | 0.426 | 0.495 | 0.488 | 90'0 (n | (at 'acca) | 0.602 | (01,149 0.149 | 3.50 | 0.169 | 0.381 | 0.078 | 0.277 | 0.124 | (mr (crcr)) | 0.043 (ut , Puc.u. | 0.039 | 8.16 | c) (at 'cr') | 0.093 (UL , PO. | | 169 (01.747) | 1351 |
| ŝ | (50.2, 8) | (232, 10) | (84.8, 8) | (0.578, 9) | (0.462, 10 | (1.06,1) | 0) (0.067, 9 | (0.075, 10) | (1.07, 10) | (0.144, 10) | (4.73, 10) | (0.067, 10) | (0.409, 10) () | 0.086, 5) | (0.37, 10) | (0.048, 10) | (0.729, 10) | 0.024, 10) (0. | 023, 10) (1 | 4.1, 10) ((| 0.022, 8) (0. | 088, 10) (1 | 13, 10) (0.1; | 28, 10) (0.5 | (19, 10) |
| Te | 0.959 | 0.055 | 64.1 | 0.121 | 0.496 | 0.009 | 0.032 | 0.025 | 0.117 | 0.023 | 0.25 | 0.011 | 9200 | 0.064 | 0.132 | 0.09 | 0.301 | 0.03 | 0.078 | 2.37 | 60.09 | 0.187 | 0.59 0 | 90 | 91.6 |
| | (0.505, 8) | (0.024, 9) 18.8 | (180, 8) | 0.011 | 0.043 | 0.205 | 0.005 | 0.003 | 0.041 | 0.024 | 0.34 | 0.036 | 0.019 | 0.046 | 0.032 | 0.019 | 0.023 | 0.003 | 0.003 | 0.91 | 0.005 | 0.04 (01 (0 | 0.0 (6, 68/ | 93, 9) (U.) 039 0 | (8,151 |
| ч | (4.09, 8) | (10.1, 10) | (16.6, 7) | (0.007, 9) | (0.038, 10 | (0.524, | 8) (0.003, 6 | (0.002, 6) | (0.059, 10) | (0.046, 10) | (0.469, 10) | (0.024, 10) | (0.022, 9) () | 0.069, 4) | (0.043, 9) | (0.016, 9) | (0.022, 9) | (0.003, 6) (0 | .003, 4) () | ((()))))))))))))))))))))))))))))))))))) | 0) (6,900) | .042, 9) (0. | 48, 10) (0.0 | .0) (6,67 | 067, 9) |
| He | 4.833 | 4.57 | 554 | 22.9 | 6.42 | 231 | 146 | 85.1 | 315 | 387 | 3.83 | 0.72 | 606.0 | 0.596 | 3.2 | 0.393 | 3.76 | 0.46 | 0.544 | 27.6 | 0.47 | 4.21 | 376 1 | 3.2 1 | 1.22 |
| 8 | (4.12, 8) | (3.13, 10) | (1738, 10) | (13.6, 9) | (0.917, 10 | (116, 1(| () (72.5, 10 | (53.7, 10) | (210, 10) | (230, 10) | (3.19, 10) | (0.504, 10) | (0.402, 10) (0 | (241, 10) | (2.61, 10) | 0.132, 10) | (3.34, 10) | 0.114, 10) (0. | 454, 10) (9 | .51, 10) (0 | .125, 10) () | 1.5, 10) (0. | 84, 10) (6.6 | 7,10) (0.6 | 24, 10) |
| Pb | 15261 | 8106.00 | 232 | 7.59 | 6.83 | 2.05 | 0.589 | 0.40 | 3.29 | 3.47 | 65.98 | 3 | 222 | 0.312 | 5.16 | 1.44 | 26.3 | 0.213 | 0.289 | 212 | 423 | 5.22 | 13.1 4 | 32 | 1.48 |
| | (5292, 8) | (3942, 10) | (730, 10) | (4.99, 9) | (3.95, 10 | 1 (2.23, 1 | 0) (0.396, 10 | (0.425, 10) | (1.81, 10) | (4.21, 10) | (118, 10) | (1.78, 10) | (4.53, 10) (0 | (01,171,10) | (11.7, 1) | 0.755, 10) | (21.2, 10) | 0.178, 10) (0 | 335, 10) (J | 9.2,10) () | () () () | 17, 10) (2 | (0, 10) (7.2 0, 10) (7.2 | 2, 10) (0.8 | 42, 10) |
| Bi | 17.9.8) | (14.3.10) | (6.6.9) | (0.283.9) | 01.886.10 | 1.110.01 0 | CT0.0 (0.021.10 | 01.019.10) | (0.123.10) | (01.390.0) | (1.06.10) | (0.04.10) | 0.066.10) 0 | 0.015. 9) | (1.55.10) | 0.081.10) | (0.89.10) | 17.52.91 (0. | 006.10) (2 | 38, 10) (0 | 044.10) (0 | 08.10) (0. | 14.10 (0.7 | 19.101 (0.3 | 85. 10) |
| ¹ Values outsi | te of brackets at | re average values | based on 'n' an | talyses | in family | forman 1 | | Tax bernary 1 | (and famous) | (as (acar) | las hand | (articul) | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 1. | (a. (a) | (au (10000) | far from | | a) far fan | at far far | al far far a | in far fan | in the first | and far for | 100 600 |
| ² Values insid- | of brackets rep | present ±1 s.d and | 'n' analyses | | | | | | | | | | | | | | | | | | | | | | |
| ³ Respective a | rcheological site | 's are listed helow | each artifact n | number | | | | | | | | | | | | | | | | | | | | | |
| 'GLR = Gas | erean Lake Res | ervoir | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | |

| Table 3.3 ct | ntinued | | | | | | | | | | | | | | | | | | | | | |
|--------------------------|---------------|-------------------|---------------------|--------------------|-----------------------|-------------|----------------|-------------|--------------|------------------------|---------------------|-------------|----------------------|-----------------------|--------------------|--------------------|----------------------|----------------------|---------------|------------------|-------------------|----------------|
| Element | 8289 | 8590 | 1658 | 8592 | 8594 | 8595 | 8596 | 8597 | 8658 | 8599 | 8604 | 8605 | 8606 | 8607 | 8098 | 8609 | 8610 | 8630 | 66 | 211 | 173 | 7 |
| | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | GLR | Isle Haute | Isle Haute | Jeddore Harbou | Margaretsville |
| | 150 | 122 | 141 | 1128 | 183 | 132 | 362 | 242 | 165 | 1112 | 268 | 117 | 156 | 85947 | 615 | 73 | 152 | 107 | 395 | 256 | 1418 | 236.92 |
| 2 | (18.4, 10) | (25.9, 10) | (9.59, 10) | (2343, 10) | (38.5, 10) | (20.9, 10) | (54.5, 10) | (172, 9) | (47, 10) | (1891, 10) | (34.7, 10) | (10.6, 10) | (20, 10) | (226676, 7) | (352, 10) | (12.3, 10) | (13.5, 10) | (25.1, 10) | (51.3, 10) | (25.3, 10) | (1404, 9) | (20.5, 10) |
| 5 | 50.6 | 33.9 | 9.74 | 7290 | 391 | 80.2 | 364 | 155 | 165 | 3326 | 38.3 | 9.8 | 15.5 | 5487 | 165 | 18.4 | 643 | 52.8 | 11.3 | 52.2 | 2372 | 35.62 |
| | (01,9.95) | (21.8, 10) | (5.04, 10) | (18226, 10) | (368, 10) | (01.4, 10) | (339, 10) | (241, 10) | (108, 10) | (0862, 10) | (32.1, 10) | (4.64, 10) | (21.7, 10) | (15665, 10) | (135, 10) | (01,7,10) | (04.1, 10) | (54.8, 10) | (1.34, 10) | (36.9, 10) | (1773, 9) | (33.3, 10) |
| Mn | BUL | BDL | 0.475 | 505 | BUL | 1.59 | 64-1 | 25.8 | 20.4 | 1353 | 65.6 | 5.0 | 141 | 6262 | 14.8 | 91.1 | 0.45 | 1.94 | 4.55 | 52.8 | BUL | 1.751 |
| | BUL | BUL | (01,295,10) | (103, 10) | 101 1010 | (01 (878-0) | (01, 67.9, 10) | (6 (7 9) | (9.88, 10) | (6,556) | (01, 10) | (1, 1) | (4.78, 10) | (113818, 10) | (01,54,10) | (01.79, 10) | (0.339, 9) | (01,10) | (01, 609, 10) | (49.7, 10) | 1091 | (1.14, 10) |
| Fe | 101 101 | COOT OF | 1.84 | 85457 | 2785 | 077 | 00.606 | 12000 101 | 100 100 | 680/C | 10401 | 101 002 | 434 | 342130 | C/TC | 6/17 | 100 | 1473 101 | 116 | 1003 | 17261 | 101 CUCH |
| | 0 105 | (NT (007) | (01 (2.4.6) | (01, (01+0) | (01 , 494.C) | (01,114) | (01 '06T) | (UI (800CI) | (NT '04C) | (01 (1/0/11) | (01 (CC07) | 01456 | 01 (007) | (AT '6+C+70) | (01.4.11C) | 01.44,10) | 0 104 | (1445, 10) 1 13 | (01,122) | (NT 410, TU) | (4/13, 9) | (NT 'COCT) |
| ථ | 012510 | 0 015 91 | (0 017 T) | (141 10) | 0.15 10 | (1) 744 8) | 101 38 00 | (9 85 8) | (0 032 10) | 1154 0) | (0 129 10) | 0 12 10 | (40 4 10) | (19 6) | (0 14 10) | 0162.10 | (0 155 0) | 0.40 80 | 10 074 10) | (01 01 1) | 001 00 | 0 874 10) |
| ; | 0.568 | 1.04 | 0.65 | 127 | 8.74 | 1.15 | 5.57 | 28.4 | 2.93 | 234 | 23.5 | 436 | 3291 | 5592 | 5.65 | 4.6 | 0.699 | 1.97 | 1.89 | 4.19 | 6.69 | 138.32 |
| Z | (0.332, 9) | (0.539, 10) | (0.27, 8) | (258, 10) | (8.17, 10) | (0.747, 10) | (7.09, 10) | (55.9, 9) | (2.29, 10) | (580, 10) | (3.78, 10) | (0.943, 10) | (2064, 10) | (14741, 8) | (2.42, 10) | (1.33, 10) | (0.911, 9) | (0.995, 10) | (1.07, 10) | (3.21, 10) | (59.3, 9) | (53.3, 10) |
| Ta | 98.3 | 80.6 | 30.2 | 1151 | 215 | 195 | 85.66 | 263 | 474 | 808 | 9310 | 8759 | 157 | 20496 | 179 | 9883 | 60.1 | 522 | 41.7 | 36.2 | 666 | 7213 |
| 1 | (71.3, 10) | (21.8, 10) | (11.5, 10) | (3225, 10) | (199, 10) | (119, 10) | (54.4, 10) | (222, 10) | (185, 10) | (868, 10) | (1206, 10) | (2699, 10) | (112, 10) | (18631, 10) | (155, 10) | (2998, 10) | (41.4, 10) | (349, 10) | (30.1, 10) | (25.4, 10) | (425, 9) | (2594, 10) |
| Ga | 618.0 | 2.24 | 151.0 | 73.3 | 13.8 | 0.768 | 0/.1 | 3.31 | 1.52 | 0.71 | 8.31 | 61.2 | 01210 | 614 | 9.35 | 129 | 0.403 | 1.43 | 101 | 1.45 | 5.62 | 0.8253 |
| | 0.600 | 0.774, 10) | 0 326 | (1188, 10) | (01,1.0) | 0 161 | (01, 00) | (3.4.9) | (01,616.0) | (01 (23.9, 10) 8 54 | (01,46.10) | 0.892, 10) | 0.287, 10) | (/4.2, 8) 85 | (01 °(./.) | 0.785, 10) | (0.386, 10) 0.403 | 0.778, 10) | 0.511, 10) | 0.577 | (18.7, 9) 5 30 | 0.907, 10) |
| g | (0 532 8) | (0 181 0) | (0.787.8) | 101 890 | 01.77.0 | 196 7 | 0 37 8) | 131.50 | (0186.10) | 185.80 | 01 242 | 10 292 101 | 0.137.10 | T 200 | 12.01.81 | (0 439 10) | 0 298 6) | (0 598 8) | 0177.10 | (0 232 10) | 13.33.01 | (0 579 8) |
| | 2.69 | 15.2 | 141 | 25.9 | 13.8 | 4.05 | 6.71 | 17.7 | 67 | 15.9 | 824 | 1200 | 1735 | 10140 | 16.1 | 2018 | 41.4 | 12.1 | 140 | 65.4 | 43.8 | 177.2 |
| As | (1.47, 10) | (4.72, 10) | (0.372, 10) | (44.2, 10) | (10.2, 10) | (2.01, 10) | (3.96, 10) | (12.9, 10) | (3.57, 10) | (23.6, 10) | (145, 10) | (440, 10) | (1124, 10) | (10398, 10) | (10.5, 10) | (569, 10) | (19.5, 10) | (5.70, 10) | (58.4, 10) | (23.8, 10) | (11.4, 9) | (75.8, 10) |
| Mo | 0.385 | 0.169 | 0.105 | 2.56 | 0.769 | 0.16 | 0.161 | 0.424 | 0.38 | 0.487 | 1.05 | 0.186 | 0.173 | 0.342 | III | 0.206 | 0.179 | 0.518 | 36.3 | 18 | 0.631 | 1.325 |
| | (0.142, 10) | (0.085, 9) | (0.058, 8) | (4.77, 10) | (0.518, 10) | (0.092, 10) | (0.07, 9) | (0.398, 8) | (0.367, 10) | (0.872, 10) | (0.184, 10) | (0.128, 8) | (0.084, 10) | (0.201, 6) | (1.13, 10) | (0.156, 9) | (0.072, 8) | (0.395, 10) | (11.6, 10) | (3.25, 10) | (0.752, 8) | (1.22, 10) |
| Ae | 359 | 78.1 | 326 | 479 | 103 | 40.6 | 14.4 | 123 | 78.4 | 29.6 | 068 | 1772 | 6548 | 2601 | 432 | 2212 | 7.62 | 14.4 | 12.4 | 14.9 | 401 | 461.4 |
| f | (141, 10) | (53.2, 10) | (171, 10) | (345, 10) | (34.1, 10) | (6.96, 10) | (6.06, 10) | (53.5, 10) | (25.7, 10) | (44.3, 10) | (344, 10) | (212, 10) | (2997, 10) | (1403, 10) | (297, 10) | (494, 10) | (14.5, 10) | (3.46, 10) | (12.3, 10) | (7.87, 10) | (135, 9) | (167, 10) |
| Cd | 161.0 | 0/1-0 | 0/0.0 | 101 23 101 | C8870 | 101 222 0 | 0.335 | 1.0010 | 1/20 | 1.09 | 1170 | 1.14 | 101 120 0 | 103 | C 16 10 | 145 | 850.0 | 101 001 0 | CC5.0 | (0.191.10) | 18.6 | SU/.C |
| | 0.034 | (01 (mon) | 9000 | 2.16 | (01, CLC.0) | 0.024 | 0,007 | 0.445 | 0.214 | 0.181 | 256 | (01 (Jac) | (01 (1 (0))) 65.5 | 455 455 | 2.46 | (01 (14T)) 80.9 | 0.008 | 0.053 | 0.029 | 0.017 (ULT 0.017 | 0.209 | 0.04026 |
| 9 | (0.075, 9) | (0.002, 8) | (0.004, 9) | (3.72, 9) | (1.26, 10) | (0.047, 6) | (0.005, 9) | (0.493, 10) | (0.321, 10) | (0.339, 8) | (34.9, 10) | (28.1, 10) | (30.1, 10) | (763, 10) | (3.64, 10) | (17, 10) | (0.005, 9) | (0.095, 10) | (0.072, 9) | (0.014, 9) | (0.138, 9) | (0.008, 10) |
| Cn. | 0.312 | 0.187 | 0.513 | 23.2 | 5.1 | 1.29 | 0.39 | 25.5 | 111 | 3.47 | 86870 | 3407 | 839 | 21613 | 16.6 | 4416 | 0.262 | 1.18 | 1.09 | 2.64 | 5.53 | 24.112 |
| | (0.265, 10) | (0.107, 10) | (0.233, 10) | (67.5, 10) | (3.94, 10) | (3.07, 10) | (0.251, 10) | (27.3, 10) | (0.981, 10) | (5.07, 10) | (15974, 10) | (1023, 10) | (1319, 10) | (23952, 10) | (27.8, 10) | (911, 10) | (0.125, 10) | (1.35, 10) | (0.697, 10) | (2.49, 10) | (3.78, 9) | (4.29, 10) |
| 9S | 0.138 | 0.155 | 0.076 | 1.05 | 1.07 | 191.0 | 140.0 | 1.28 | 0.232 | 0.472 | 326 | 347 | 9646 | 1269 | 1.33 | 396 | 0.328 | 0.169 | 0.847 | 0.538 | 1.50 | 8.238 |
| | (01,801.0) | (0.175 0.175 | 0.053, 9) | 0.461 | (01, 50.10) | (01,001,00) | 0.057 | (01 (c0.1) | (01,200, 10) | (01,44,10) | (01,5.0/) | (01 (01) | (01 ,1260) 1 566 | (18/9, 10) 51.0 | (1.49, 10) 1.75 | (01,5-45) 10) | 0.006 | (8,191,8) A A1 | 01213, 10) | 01,293, 10) | (I'UI') | 01 (9766 |
| đ | (0.026, 8) | (0.188, 8) | (0.057, 8) | (1.03, 8) | (101, 9) | (0.04, 10) | (0.05, 8) | (1.12, 10) | (0.016, 9) | (0.084, 9) | (0.049, 10) | (1.69, 10) | (0.943, 10) | (58.1, 8) | (1.1, 8) | (14.6, 10) | (0.004, 6) | (0.014, 8) | (0.035, 9) | (0.024, 7) | (0.764, 8) | (0.281, 10) |
| | 0.014 | 0.009 | 0.004 | 0.078 | 0.089 | 0.009 | 0.002 | 0.537 | 0.033 | 0.018 | 106 | 103 | 471 | 325 | 0.186 | 114 | 0.006 | 0.008 | 0.007 | 0.011 | 0.038 | 1806.0 |
| nv | (0.013, 9) | (0.004, 10) | (0.003, 9) | (0.095, 9) | (0.07, 9) | (0.009, 8) | (0.001, 4) | (0.43, 8) | (0.03, 10) | (0.016, 8) | (9.39, 10) | (36.3, 10) | (305, 10) | (384, 10) | (0.457, 9) | (23.9, 10) | (0.005, 7) | (0.006, 8) | (0.005, 10) | (0.008, 10) | (0.036, 9) | (0.215, 10) |
| Hg | 0.749 | 0.59 | 0.597 | 1.63 | 0.823 | 0.292 | 0.28 | 3.86 | 0.506 | 0.677 | 0.321 | 0.624 | 0.786 | 009 | 5.14 | 0.435 | 0.461 | 0.32 | 61.7 | 3.23 | 150 | 126.7 |
| | (01 '7cT'0) | (01,090) 1 48 | (0.142, 10) 1 46 | (2.33, 10) 50.4 | (01,522), 10) 30.6 | 0.004, 10) | (01, (0.0) | (01, 6.8) | (01 %7T.0) | (0.86, 10) | (0.11, 10) 15370 | (0.14, 10) | 10477 | (III (COIII) 86473 | (01, 10) 56.5 | (01,811.0) 8773 | (01,202, 10) 1 35 | (01,085, 10) 3.17 | (01,62) | (01,22.2) | (01.1, 9) | (01,5,10) |
| Pb | (26.4.10) | (0.625, 10) | (1.6.10) | (96.4.10) | (24.3, 10) | (0.492.10) | (1.25, 10) | (151, 10) | (4.51, 10) | (10.10) | (1185, 10) | (1612, 10) | (6248, 10) | (96402.10) | (53.9.10) | (2276.10) | (1.47.10) | (5.18, 10) | (37.4.10) | (76.7. 10) | (122.9) | (396, 10) |
| 2 | 0.228 | 0.211 | 0.058 | 0.77 | 1.51 | 0.067 | 0.13 | 3.04 | 0.222 | 0.753 | 192 | 188 | 176 | 340 | 2.56 | 224 | 1.634 | 0.074 | 0.028 | 0.637 | 1.28 | 1.4547 |
| 18 | (0.146, 10) | (0.091, 10) | (0.048, 10) | (1.39, 10) | (1.06, 10) | (0.046, 10) | (0.204, 10) | (5.89, 10) | (0.278, 10) | (1.16, 10) | (77.8, 10) | (121, 10) | (98.1, 10) | (264, 10) | (2.46, 10) | (135, 10) | (4.79, 9) | (0.086, 10) | (0.016, 10) | (1.88, 10) | (0.661, 9) | (0.656, 10) |
| ¹ Values out. | side of brack | kets are average | ge values base | d on 'n' analyse | | | | | | | | | | | | | | | | | | |
| ² Values insi | de of bracke | ets represent ± | t s.d and 'n' a | unalyses | | | | | | | | | | | | | | | | | | |
| ³ Respective | archeologic | al sites are list | ted below eac | h artifact numb | er | | | | | | | | | | | | | | | | | |
| ⁴ GLR = Ga | spereau Lab | te Reservoir | | | | | | | | | | | | | | | | | | | | |

| Flamont | 819 | 820 | 821 | 822 | Rlake | 851 | 859 | 863A | 863B |
|---------|--------------|--------------|--------------|--------------|-------------|--------------|--------------|--------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Trement | Muskrat Cove | Muskrat Cove | Muskrat Cove | Muskrat Cove | Rafter Lake | Sellars Cove | Sellars Cove | Sellars Cove | Sellars Cov |
| 6 | 375 | 193 | 204 | 316 | 179 | 175 | 208 | 362 | 416 |
| 0 | (107, 10) | (18.7, 10) | (42.5, 10) | (152, 10) | (55.9, 10) | (17.4, 10) | (50.9, 10) | (44.5, 6) | (76.3, 5) |
| ć | 2182 | 1.71 | 28.2 | 126 | 22.5 | 0.717 | 384 | 118 | 93.3 |
| 5 | (1175, 10) | (1.30, 10) | (34.2, 10) | (166, 10) | (48.2, 8) | (0.269, 9) | (962, 10) | (32.9, 6) | (72.6, 5) |
| | 2.86 | 0.103 | 21.9 | 1.57 | 4.01 | 0.107 | 1.97 | 12.3 | 21.1 |
| IIM | (1.63, 10) | (0.028, 8) | (16, 10) | (1.36, 10) | (3.37, 8) | (0.057, 7) | (1.62, 9) | (3.21, 6) | (10.8, 5) |
| E. | 11199 | 1.19 | 374 | 3136 | 676 | 5.72 | 1805 | 261 | 206 |
| P.C | (9360, 10) | (1.12, 10) | (560, 10) | (4082, 10) | (1504, 9) | (1.53, 10) | (3068, 10) | (91.7, 6) | (225, 5) |
| | 24.4 | 0.069 | 0.47 | 1.02 | 0.563 | 0.074 | 0.31 | 0.066 | 0.071 |
| 3 | (14.9, 10) | (0.055, 4) | (0.66, 7) | (1.73, 9) | (0.72, 4) | (0.057, 6) | (0.404, 9) | (0.035, 5) | (0.071, 4) |
| | 104 | 0.31 | 1.13 | 3.36 | 2.3 | 0.49 | 1.24 | 0.95 | 0.71 |
| R | (43.9, 10) | (0.176, 4) | (1.29, 8) | (4.23, 10) | (1.64, 5) | (0.468, 8) | (1.33, 8) | (0.145, 6) | (0.285, 3) |
| ł | 33321 | 4.11 | 81.3 | 196 | 3.5 | 0.758 | 27.2 | 41.4 | 15.1 |
| 17 | (11161,10) | (4.10, 10) | (39.3, 10) | (162, 10) | (3.76, 8) | (0.287, 10) | (23.8, 10) | (2.83, 6) | (5.81, 5) |
| ć | 5.97 | 0.134 | 0.902 | 1.72 | 0.584 | 0.071 | 0.778 | 1.53 | 1.94 |
| 5 | (3.16, 10) | (0.083, 6) | (1.05, 10) | (0.479, 8) | (0.686, 8) | (0.072, 9) | (1.09, 9) | (0.629, 6) | (2,5) |
| ć | 5.46 | 0.212 | 0.667 | 0.521 | 1.57 | 0.247 | 0.321 | 0.578 | 0.458 |
| 3 | (1.92, 10) | (0.249, 5) | (0.668, 8) | (5.98, 10) | (0.952, 5) | (0.126, 7) | (0.572, 8) | (0.35, 5) | (0.211, 5) |
| | 592 | 0.705 | 7 | 6.10 | 1.09 | 1.17 | 11.3 | 49.9 | 28.6 |
| SV. | (253, 10) | (0.486, 10) | (4.9, 10) | (0.921, 8) | (0.978, 8) | (0.339, 10) | (8.79, 10) | (4.57, 6) | (15.9, 5) |
| | 0.931 | 0.164 | 0.332 | 0.656 | 0.325 | 0.067 | 0.27 | 0.248 | 0.3 |
| OIM | (0.195, 10) | (0.07, 9) | (0.2, 10) | (56.9, 10) | (0.145, 4) | (0.048, 7) | (0.233, 10) | (0.076, 6) | (0.121, 4) |
| | 734 | 515 | 559 | 90.6 | 16.7 | 34.3 | 105 | 32.9 | 63.1 |
| ŝ | (353, 10) | (649, 10) | (397, 10) | (0.105, 10) | (5.34, 10) | (13.8, 10) | (53.5, 10) | (23.6, 6) | (35.6, 5) |
| P.C | 6.93 | 0.041 | 0.101 | 0.167 | 0.162 | 0.026 | 0.259 | 0.713 | 0.288 |
| 3 | (8.42, 10) | (0.029, 9) | (0.094, 8) | (0.144, 10) | (0.116, 6) | (0.023, 6) | (0.129, 10) | (0.128, 6) | (0.118, 5) |
| -1 | 334 | 0.002 | 0.094 | 0.097 | 0.014 | 0.007 | 0.028 | 0.012 | 0.005 |
| 1 | (188, 10) | (0.002, 5) | (0.191, 9) | (143, 10) | (0.007, 7) | (0.008, 7) | (0.068, 9) | (0.008, 6) | (0.002, 4) |
| -0 | 94000 | 0.095 | 5.33 | 86.7 | 0.141 | 1.76 | 1.07 | 3.45 | 0.741 |
| IIC | (57736, 10) | (0.075, 9) | (2.52, 10) | (2.35, 10) | (0.253, 9) | (2.84, 10) | (1.01, 10) | (2.72, 6) | (0.539, 5) |
| 45 | 199 | 0.039 | 0.762 | 1.08 | 0.154 | 0.029 | 0.089 | 0.057 | 0.048 |
| 00 | (65.5, 10) | (0.021, 10) | (1.4, 10) | (0.00, 1) | (0.094, 7) | (0.037, 6) | (0.116, 7) | (0.028, 6) | (0.03, 4) |
| f | 0.179 | 0.009 | 0.236 | 0.18 | 0.061 | 0.137 | 0.058 | 0.039 | 0.127 |
| ar | (0.148, 8) | (0.003, 5) | (0.209, 5) | (0.944, 10) | (0.057, 4) | (0.113, 6) | (0.043, 7) | (0.053, 3) | (0.025, 2) |
| | 41.1 | 0.018 | 0.174 | 0.252 | 0.011 | 0.005 | 0.02 | 0.008 | 0.004 |
| nv | (18.3, 10) | (0.017, 10) | (0.094, 10) | (0.231, 10) | (0.014, 4) | (0.003, 6) | (0.016, 8) | (0.001, 2) | (0.001, 2) |
| n. | 1.29 | 6.30 | 2.77 | 1.54 | 50.2 | 8.40 | 86.3 | 3.73 | 3.59 |
| Å | (0.518, 10) | (3.79, 10) | (2.37, 10) | (0.944, 10) | (53.3, 10) | (1.37, 10) | (50.2, 10) | (1.45, 6) | (1.57, 5) |
| h | 41030 | 0.136 | 5.34 | 10.6 | 0.376 | 0.128 | 3.19 | 1.26 | 0.496 |
| 2 | (21854, 10) | (0.271, 10) | (3.64, 10) | (12.6, 10) | (0.528, 10) | (0.159, 10) | (4.87, 10) | (0.441, 6) | (0.098, 5) |
| ia | 68.6 | 0.005 | 0.641 | 0.273 | 0.018 | 0.004 | 0.111 | 0.04 | 0.013 |
| 5 | 101 1 202 | | 10.0 000 00 | | | | | | the second secon |

(20.1. 10) (20.2. 11) (20.2. 11) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12) (20.2. 12)

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3.4.2 Group II

Group two (Figure 3.6C & D) only contains two artifacts (64, 230). This group contains very low concentration relationships for the indicator elements and nearly matches the artifacts found in group three. These two artifacts have a low Ag vs Pb relationship (8.02 – 26.05 ppm vs 6.86 - 7.59 ppm), and moderate Hg vs Bi relationship (6.42 - 22.97 ppm vs 0.18 - 0.55 ppm). The relationship that makes group two unique however, is the concentration of Zn (53.06 - 144 ppm) vs that of As (50.4 - 87.81 ppm). Most of the other groups have much higher concentrations of Zn, generally double or higher the concentration of As, however in this case there is not as big of a range. Larger scale differences are seen in the concentration of Sn (0.083 and 13.1 ppm) as well as the relationships between Ag and Pb, (Figure 3.6C&D). Artifact 64, has a higher concentration of Ag with respect to Pb (26.1 vs 7.59 ppm), whereas artifact 230 has a very small relationship between Ag and Pb (8.02 vs 6.86 ppm).

3.4.3 Group III

Artifacts in groups one through four, are all different than the last six groups, as they all contain extremely low Ag vs Pb relationships, in some instances, there are even artifacts that have diagnostically high Pb and low Ag as is the case with group four. Group three (Figure 3.6E& F) has an interesting Ag to Pb relationship, as they are both present in almost equal quantities. In fact, artifact 8579 has a Ag concentration of 226 ppm and a Pb concentration of 212 ppm. Relationships between Hg and Bi are low, with Hg still being more enriched than Bi (0.38 - 27.63 ppm s 0.06 - 7.51 ppm), and Zn to As relationships that are still high (60.9 - 5921 ppm vs 1.54 - 127 ppm). In group three, the concentration of Sn (1.45 - 170 ppm) is greater than the concentration of Sb (0.05 - 8.16 ppm), however

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the Sb: Te relationships are lower than in the first four groupings which sets this group apart. The highest average concentration of Sb is 8.16 ppm and the highest concentration of Te is only 2.38 ppm, nearly four times higher. Artifacts 8566, 8579, 8580, 8594, and 8597, all belong to provenance group five. These artifacts show good homogeneity (Figure 3.5E& F) in the overall trace element patterns for the group, however very slight differences are seen in the ranges of Cd (0.25 - 11.8 ppm), In (0.002 - 2.86 ppm), Te (0.09 - 2.38 ppm) and Bi (0.06 - 7.51 ppm), yet if the patterns between Zn and As, as well as Ag and Pb are examined closer, we see the same continuous relationships, albeit at slightly higher or lower orders of magnitude.

3.4.4 Group IV

The fourth provenance group (Figure 3.6G & H) is characterized by high concentrations of As vs Zn (65.36 - 139 ppm vs 36.2 - 41.7 ppm), high Pb vs Ag (102 - 112 ppm vs 12.4 - 14.9 ppm), and high Hg vs Bi (3.23 - 7.19 vs 0.03 - 0.64) relationships. However artifacts classified in this group also have relatively high enrichments in Mo as compared with the rest of the copper collection (18 and 36 ppm). Indium, Te, Au and Bi are all comparable to the depletions of these elements in other artifacts (tenths to hundredths of ppm), yet the majority of the other artifacts have depletions of Mo as well. Artifacts 99 and 211 are the two sole artifacts that have anomalously high concentrations of Mo. The most notable differences in chemistry between these two artifacts is the difference in Sn and Bi concentrations. Artifact 211 has a greater concentration in Bi and Sn (0.64 ppm and 2.64 ppm respectively), making it have a lower Hg vs Bi relationship, and a higher Sn: Sb relationship as compared with artifact 99 which has 0.03 ppm Bi and 1.09 ppm Sn.

3.4.5 Group V

The fifth provenance group (Figure 3.7A &B) is where we begin the high Ag vs Pb relationships instead of the low Ag vs Pb or high Pb vs Ag relationships. This provenance group contains artifacts 2015, 1949, 5377, 8568 and 8569. Diagnostically high relationships for this group are seen in Ag vs Pb, Hg vs Bi, Zn vs As. The range of silver concentrations is between 87 and 281 ppm, whereas the range for Pb is significantly smaller and is only between 0.31 and 3.47 ppm. Hg values range between 0.06 and 386 ppm yet the Bi values are low again and only run between 0.01 and 0.1 ppm. The relationships between Zn and As are also favourable to Zn (24.1 - 157 ppm) when compared to the small range of As concentrations (1.24 - 8.52 ppm). What separates this group apart from group six, is the relationship between Sn and Sb. They share similar concentration ranges (0.13-0.45 ppm for Sn and 0.06 - 0.49 ppm for Sb) yet are significantly higher than those of Te which only range between 0.01 and 0.08 ppm. This is one of the groups that must be differentiated using the relationship between Sb and Sn, as it bears a strong resemblance to the chemistry of artifacts in the sixth provenance group. Differences are seen in the concentration of In (0.00 and 0.47 ppm) as well as the orders of magnitude in the concentration of Hg (Figure 3.7A &B), yet not different enough to separate them into other groupings at this time. When more sources are found to compare with, this group may be revisited.

3.4.6 Group VI

The sixth group (Figure 3.7C & D) contains artifacts RLAKE, 173, 820, 2158, 2225, 8572, and 8584. This group is characterized by high Ag vs Pb relationships (16.7 – 11458 ppm Ag vs 0.14 – 91.2 ppm Pb), high Hg vs Bi relationships (3.2 – 315 ppm Hg vs 0.00 –

1.28 ppm Bi), and high Zn vs As relationships (3.5 - 993 ppm Zn vs 0.71 - 43.7 ppm). Sn is also more concentrated than Sb and Te which is the separator between groups five and six. The relationship between Sn (0.09 - 5.53 ppm), Sb (0.04 - 1.5 ppm) and Te (0.01 - 0.82 ppm) is a linear decreasing one whereas in group five there is more scatter in the relationship between these three elements. Group six does not present with the best homogeneity as compared with the other provenance groupings, as there is variation in the orders of magnitude between each of the artifacts, as well as significant variation in Pb (0.14 - 91.2 ppm), Cd (0.04 - 5.87 ppm), In (0.00 - 0.27) and to a lesser degree, Zn (3.5 - 993 ppm). Artifact 820 also presents with diagnostically higher Au (0.003 ppm), as compared to the rest of the artifacts not reduced by Fe (0.02 ppm) artifact 820 falls better into the grouping presented here.

3.4.7 Group VII

The seventh provenance group created (Figure 3.7E& F) has significantly higher Ag vs Pb (34 - 4494 ppm vs 0.13 - 5.22 ppm) and Hg vs Bi (0.54 - 86.3 ppm vs 0.00 - 0.11 ppm relationships, however the relationship between Zn (0.76 - 41.3 ppm) and As (1.17 - 41.4 ppm) is much smaller than the others. Sn is also much more concentrated in this group than in group eight, ranging between 0.32 and 3.45 ppm. After the Fe reduction had taken place, the orders of magnitude of trace element signatures are quite different (Figure 3.7E& F), however the patterns remain similar amongst the artifacts. Another notable difference in this group compared to the others is the enrichment of Te compared to Sb. In the majority of artifacts, the concentration of Sb (0.03 - 0.09 ppm) has often been higher than that of Te, yet in this group it remains the opposite with Te concentrations ranging between 0.04

and 0.19 ppm. Differences in the concentration of Cd (0.03 - 0.71 ppm) and In (0.00 - 0.54 ppm) are notable in the group, yet again, not significantly enough to warrant separation into additional provenance groups. Artifacts sorted into the seventh provenance group include 851, 859, 863A, 863B 8577, and 8581.

3.4.8 Group VIII

Artifacts 8610 and 8590 have chemistries different enough to warrant an additional provenance grouping (Figure 3.8A&B). This group contains a higher Ag (29.7 – 78.1 ppm) vs Pb (1.35 – 1.48 ppm) relationship, however the concentration relationship between Hg and Bi is unique to this group as the concentrations of Bi (1.63 and 0.21 ppm respectively) are higher than those of Hg (0.46 and 0.59 ppm respectively). Also notable relationships exist between Zn and As where Zn concentrations are 60.1 ppm for artifact 8610 and 80.7 ppm for artifact 8590, and As concentrations are 41.4 and 15.2 ppm for each respective artifact. Similar relationships exist in the relationship between Sn and Sb. Most other groupings show higher Sn or higher Sb, yet in group eight, the concentrations of these elements are very similar with Sn concentrations of 0.24 and 0.19 ppm, and Sb concentrations of 0.33 and 0.15 ppm for artifact 8610 and 8590.

3.4.9 Group IX

Provenance group nine (Figure 3.8C &D) has diagnostically high Ag (14.4 – 559 ppm) to Pb (1.44 – 56.5 ppm) and higher Zn (78.8 – 1042 ppm) to As (6.1 – 112.3 ppm) relationships, with moderate to low Hg (0.28 - 5.41 ppm) to Bi (0.07 - 2.56) relationships. However the notable relationship in this group is that which exists between Sn (0.39 - 86.7 ppm), Sb (0.07 - 1.33 ppm) and Te (0.01 - 1.25). Even after the reduction by Fe has taken place (Figure 3.8D) there is still a significant enrichment in the concentration of Sn in this

artifact group. Variation among this artifact group exists in the concentration of Cd (0.10 - 3.03 ppm), Te, and Au (0.00 - 0.25 ppm). Differences in the concentration of Pb are visible before the reduction by Fe (Figure 3.8C) had taken place yet afterwards, these differences are slight. Artifact 821 also contains a greater concentration of Au than in the other elements (0.25 ppm), however the remainder of the relationships in the other elements are well enough to include that artifact in this provenance group.

3.4.10 Group X

The final provenance group created from this study contains artifacts 8576, 8589, 8591, 8592, 8595 and 8598 (Figure 3.8E& F). This group is characterized by high Ag vs Pb (40.6 – 479 ppm vs 0.21 - 50.4 ppm), and Zn: As (19.2 – 1511 ppm vs 0.75 - 25.9 ppm) relationships. The tenth provenance group has a significantly lower Hg vs Bi relationship as compared with the others (0.29 - 1.63 ppm vs 0.06 - 0.89 ppm), as well as a decreasing relationship between Sn (0.28 - 23.2 ppm) Sb (0.04 - 1.05 ppm) and Te (0.02 - 0.46 ppm) which separates these artifacts from the previous group. Variation of this grouping exists between Pb (0.21 - 50.4 ppm) and Cd (0.06 - 2.89) and in some instances In (0.00 - 2.16 ppm). These variations are viewed in lesser extent after the reduction by each respective concentration of Fe (Figure 3.8F). Overall, the concentration relationships of Ag vs Pb and Zn vs As are still high after the reduction has taken place (Figure 3.8F), and many of the patterns are still similar, yet the differences and variations of most elements are only seen in the non-reduced versions of the trace element patterns(Figure 3.8E).

4.0 Discussion

4.1 Provenance Groups and Source Location

The final fifty seven copper artifacts were compared against the six native source locations, and the expectation was to see all of the trace element signatures match those of Michigan USA, based on previous studies performed (Hancock et al. 1997; Rapp et al. 2000; Levine, 2007; Cooper et al. 2008;). However upon comparison of trace element concentrations between all fifty three artifacts with six different samples from copper mines in Michigan, none of the artifacts in this copper collection were a match. The concentration of As in the Michigan samples relative to the other samples, was too high. When compared to the other samples, there were artifacts that match copper from Nova Scotia, European sources, and unknown locations. Table 4.1 summarizes all provenance determinations.

4.1.1 Cap d'Or

Provenance group V (Figure 3.3, artifacts 8566, 8579, 8580, 8582, and 8594) have trace element chemistry that match the samples from Cap d'Or. The artifacts have similar relationships of the indicator elements such as Ag and Pb, Hg and Bi, Ni and As. When not reduced by the Fe content (Figure 3.2) the artifacts in this provenance group appear to have similar relationships compared to the source samples, albeit in lower orders of magnitude. This could be attributed to a number of different factors, such as weathering and the production of corrosion material (Dussubieux et al. 2008), referred to in this paper as patina, exact area where the copper was collected (cliff face copper vs copper from the centre of the deposit) and treatment and conservation products. An argument for the use of Nova Scotian copper was made in the accounts of Samuel de Champlain when he and his

| Table 4.1 | Summary data table sho | wing all artifacts a | nd their resepective provenance groupings | | | | | | |
|-----------|------------------------|----------------------|-----------------------------------------------|-------------------------------|----------|--------------------|----------------------------|-------------------------------------------------|-------------------------------|
| Artifact | Archeological Site | Provenance group | Diagnostic elemental relationships | Provenance Location | Artifact | Archeological Site | Provenance group | Diagnostic elemental relationships | Provenance Location |
| 2 | Margaretsville | I | high concentration of all trace elements with | Europe | 2225 | Enfield | IV | high Ag:Pb, Hg:Bi, Zn:As, moderate Sn:Sb | Unknown IV |
| 19 | Burnt Bone Beach | Ι | emphasis on high Au | Europe | 8572 | GLR | N | high Ag:Pb, Hg:Bi, Zn:As, moderate Sn:Sb | Unknown IV |
| 20 | Burnt Bone Beach | Ι | high concentration of all trace elements with | Europe | 8584 | GLR | N | high Ag:Pb, Hg:Bi, Zn:As, moderate Sn:Sb | Unknown IV |
| 21 | Clam Cove | Ι | emphasis on high Au | Europe | RLAKE | Rafter Lake | IV | high Ag:Pb, Hg:Bi, Zn:As, moderate Sn:Sb | Unknown IV |
| 819 | Muskrat Cove | Ι | high concentration of all trace elements with | Europe | 851 | Sellars Cove | ПЛ | high Ag:Pb, Hg:Bi, low Zn:As | Margaretsville |
| 8604 | GLR ¹ | Ι | emphasis on high Au | Europe | 859 | Sellars Cove | ПЛ | high Ag:Pb, Hg:Bi, low Zn:As | Margaretsville |
| 8605 | GLR | I | high concentration of all trace elements with | Europe | 8577 | GLR | ПЛ | high Ag:Pb, Hg:Bi, low Zn:As | Margaretsville |
| 8606 | GLR | Ι | emphasis on high Au | Europe | 8581 | GLR | ПЛ | high Ag:Pb, Hg:Bi, low Zn:As | Margaretsville |
| 8607 | GLR | Ι | high concentration of all trace elements with | Europe | 863A | Sellars Cove | ПЛ | high Ag:Pb, Hg:Bi, low Zn:As | Margaretsville |
| 8609 | GLR | Ι | emphasis on high Au | Europe | 863B | Sellars Cove | ПЛ | high Ag:Pb, Hg:Bi, low Zn:As | Margaretsville |
| 818 | Muskrat Cove | Ι | European copper zinc alloy | Europe | 8590 | GLR | ШЛ | high Ag:Pb, Hg:Bi, moderate Zn:As | Unknown V |
| 64 | Clam Cove | п | low Ag:Pb, moderate Hg:Bi, Zn:As | Unknown I | 8610 | GLR | ШЛ | high Ag:Pb, Hg:Bi, moderate Zn:As | Unknown V |
| 230 | Clam Cove | п | low Ag:Pb, moderate Hg:Bi, Zn:As | Unknown I | 821 | Muskrat Cove | IX | high Ag:Pb,moderate Hg:Bi, high Zn:As Sn:Sb | Unknown VI |
| 8566 | GLR | Η | low Ag:Pb, Hg:Bi, high Zn:As | Cap d'Or | 822 | Muskrat Cove | IX | high Ag:Pb,moderate Hg:Bi, high Zn:As Sn:Sb | Unknown VI |
| 8579 | GLR | Η | low Ag:Pb, Hg:Bi, high Zn:As | Cap d'Or | 8567 | GLR | IX | high Ag:Pb,moderate Hg:Bi, high Zn:As Sn:Sb | Unknown VI |
| 8580 | GLR | Η | low Ag:Pb, Hg:Bi, high Zn:As | Cap d'Or | 8573 | GLR | IX | high Ag:Pb,moderate Hg:Bi, high Zn:As Sn:Sb | Unknown VI |
| 8582 | GLR | Η | low Ag:Pb, Hg:Bi, high Zn:As | Cap d'Or | 8574 | GLR | IX | high Ag:Pb,moderate Hg:Bi, high Zn:As Sn:Sb | Unknown VI |
| 8594 | GLR | Π | low Ag:Pb, Hg:Bi, high Zn:As | Cap d'Or | 8587 | GLR | IX | high Ag:Pb,moderate Hg:Bi, high Zn:As Sn:Sb | Unknown VI |
| 8597 | GLR | Η | low Ag:Pb, Hg:Bi, high Zn:As | Cap d'Or | 8596 | GLR | IX | high Ag:Pb,moderate Hg:Bi, high Zn:As Sn:Sb | Unknown VI |
| 66 | Isle Haute | IV | low Ag:Pb, high Hg:Bi, low Zn:As | Unknown II | 8599 | GLR | IX | high Ag:Pb,moderate Hg:Bi, high Zn:As Sn:Sb | Unknown VI |
| 211 | Isle Haute | IV | low Ag:Pb, high Hg:Bi, low Zn:As | Unknown II | 8603 | GLR | IX | high Ag:Pb,moderate Hg:Bi, high Zn:As Sn:Sb | Unknown VI |
| 1949 | Enfield | ٧ | high Ag:Pb, Hg:Bi, Zn:As, low Sn:Sb | Unknown III | 8098 | GLR | IX | high Ag:Pb,moderate Hg:Bi, high Zn:As Sn:Sb | Unknown VI |
| 2015 | Enfield | Λ | high Ag:Pb, Hg:Bi, Zn:As, low Sn:Sb | Unknown III | 8576 | GLR | X | high Ag:Pb,moderate Hg:Bi, high Zn:As low Sn:Sb | Unknown VII |
| 5377 | Enfield | ٧ | high Ag:Pb, Hg:Bi, Zn:As, low Sn:Sb | Unknown III | 8289 | GLR | X | high Ag:Pb,moderate Hg:Bi, high Zn:As low Sn:Sb | Unknown VII |
| 8568 | GLR | ٧ | high Ag:Pb, Hg:Bi, Zn:As, low Sn:Sb | Unknown III | 8591 | GLR | Х | high Ag:Pb,moderate Hg:Bi, high Zn:As low Sn:Sb | Unknown VII |
| 8569 | GLR | Λ | high Ag:Pb, Hg:Bi, Zn:As, low Sn:Sb | Unknown III | 8592 | GLR | X | high Ag:Pb,moderate Hg:Bi, high Zn:As low Sn:Sb | Unknown VII |
| 173 | Jeddore Harbour | IV | high Ag:Pb, Hg:Bi, Zn:As, moderate Sn:Sb | Unknown IV | 8595 | GLR | X | high Ag:Pb,moderate Hg:Bi, high Zn:As low Sn:Sb | Unknown VII |
| 820 | Muskrat Cove | IV | high Ag:Pb, Hg:Bi, Zn:As, moderate Sn:Sb | Unknown IV | 8298 | GLR | X | high Ag:Pb,moderate Hg:Bi, high Zn:As low Sn:Sb | Unknown VII |
| 2158 | Enfield | Ŋ | high Ag:Pb, Hg:Bi, Zn:As, moderate Sn:Sb | Unknown IV | | | | | |
| 1. GLR = | Gaspereau Lake Reserv | oir | | | | | | | |

French explorers visited what is now North America "I went to the river St John, to find the Indian named Secoudon... Having found him I begged him to accompany us to which he very readily agreed and came with us to show [the copper] to us..." (Biggar, 1992, in Levine, 2007). This historic passage dates back to 1604 when Champlain arrived in the Bay of Fundy, and affirms that local aboriginal peoples did have knowledge of native copper present in Nova Scotia. Other studies, namely Rapp et al. 2000; Levine, 1996, 2007a, 2007b; Hill, 2012, have all hypothesized that samples could come from Nova Scotia, however the samples used in those studies were from Cumberland County – where Cap d'Or is found. This limitation of samples from only one area of the province, can be misleading. At one time the pre-contact archaeologists believed that all copper came from Michigan, and we now know this not to be the case, so why limit all source copper samples to one area of this province? By sampling more copper deposits and copper occurrences in Nova Scotia, we've begun to create a larger copper database for comparisons with other artifacts.

4.1.2 Margaretsville

Source samples from Margaretsville contain diagnostically high concentrations of Ag. All artifacts that also contain high Ag concentrations and low Pb concentrations, were compared to the Margaretsville sources, however only provenance group I, was determined to match the Margaretsville copper. The artifacts from Margaretsville have trace element patterns similar to the native source samples but again the exact concentrations appear lower after the reduction by Fe. Similar to the Cap' d'Or samples, this could be a function of weathering processes, and geochemical zonation in the copper being used. Dussubieux et al. (2008) also describe in depth how different elements such as Pb and Zn are distributed through copper samples that have been subject to major corrosion and how samples that have a thick coating of patina, tend to be preferentially depleted in Zn. In the case of the artifacts from Margaretsville, we see that as Zn is depleted from the samples, As is as well. These relationships are important to understand not only as geochemical signatures at the time of sampling, but also regarding how elements behave in the copper over time.

Also important in the understanding of trace-element patterns in copper, is how the people using the copper were working this malleable metal. Ethnologists, and historians have known for years that for people in North America, the best way to work with copper at the time, was to anneal it by rolling and hammering pieces together (Hancock et al. 1991; Fitzgerald et al. 1993; Hancock et al. 1995; Leonard, 1996; Erhrhardt et al. 2000; Bourque 2001; Fenn, 2001; Hancock et al. 2007; Lattanzi, 2007; Cooper et al. 2008; Erhrhardt, 2009; Cooper, 2011; Hill, 2012; Michelaki et al. 2013). This method as it did not involve heat, or smelting processes, would only account for element transfer to the outer coating of the copper artifacts, and would no contaminate all the way through to the core of the copper sample (Harbottle et al, 1982; Jackson, 1992; Fitzgerald et al. 1993; Junk, 2001; Kennet et al. 2001; Aeschliman et al. 2004; Hancock et al. 2007; Frame et al. 2013.) Trace element fingerprints for copper that has been smelted or alloyed – such as the samples from European sourced copper, are very easily distinguished from non-smelted copper (Turgeon, 1990; Fitzgerald et al. 1993, Whitehead et al. 1998; Levine 2007; Dussubieux et al. 2008).

4.1.3 European

Nine of the artifacts sampled, contained trace elements with chemistry that were well above the other forty six artifacts in terms of concentration. These artifacts were not sourced from samples found in North America and in fact come from the early contact period when aboriginal people were trading with the European settlers. Large copperalloyed kettles were brought over by the French and Spanish (Mason, 1981; Turgeon, 1990; Hancock et al., 1991; Biggar, 1992; Fitzgerald et al., 1993; Hancock et al., 1995; Leonard, 1996; Wilson et al., 1997; Whitehead et al., 1998; Moreau & Hancock, 1999; Rapp et al. 2000; Bourque, 2001; Fenn, 2001; Glascock & Neff, 2003; Anselmi, 2004; Levine, 2007; Dussubieux et al., 2008; Ehrhardt, 2009; Cooper, 2011; Hill, 2012; Hodge et al., in preparation) and these "copper kettles were not as pure as the native American Copper (Turgeon, 1990; Fitzgerald et al., 1993; Moreau & Hancock, 1999; Dussubieux et al., 2008; Lattanzi, 2008;) as they had been smelted by the Europeans and other metals had now been contaminated into the copper. Much like the work done by Dussubieux et al. (2008) in this study, we discovered that certain elements, notably Fe, Cr, and S, were being over reported by the data reduction methods when the purity of copper was imputed as 99%. After seeing the over estimation of these elements, the artifacts were then analyzed by a SEM (Figure 2.1D) and it was determined that the concentration of copper was between 95 and 97 percent pure copper. After this had been changed the concentration of many of the trace elements remained orders of magnitude higher than those found in North America. These artifacts match sources from Spain, Germany and Sweden and refined European copper, copper- Zn alloys, and copper- Zn- Sn alloys (Hodge et al. in preparation). According to Turgeon (1990), aboriginal peoples would often reuse and recycle many of their goods into other things, and that is what I suggest has happened to the artifacts that match the European samples. Some of the samples that match the high copper-Zn alloyed metals, are consistent with brass kettles that were brought over by the French, and have been found in areas of the province (Turgeon, 1990; Hancock et al., 1991; Whitehead et al., 1998; Levine, 2007; Dussubieux et al., 2008).

4.1.4 Artifacts with undetermined provenance groups

Three different provenance groups formed in the study, were found to match three different source areas, two in Nova Scotia, and then one group from Europe which is consistent with the literature (Turgeon, 1990; Fitzgerald et al., 1993; Moreau & Hancock, 1999; Dussubieux et al., 2008; Lattanzi, 2008;). This still leaves seven provenance groups of the ten unaccounted for. One would think that there would be artifacts that match the Michigan samples as mentioned by other sources (Harbottle et al., 1982; Hancock et al., 1991; Ehrhardt et al., 2000; Rapp et al., 2000; Anselmi, 2004; Cooper, 2011; Michelaki et al., 2013; Abel & Burke, 2014), however in this study, all of the Michigan source samples contained higher than average concentrations of As, much too high to match any artifacts present in the collection from the Nova Scotia Museum. A much larger known copper source location database must be created using LA-ICP-MS methods in order to have a higher certainty and understanding of provenance determinations. Work on narrowing down the exact source locations of the European artifacts, is being continued by Hodge et al. (in preparation.) Emphasis must be placed on the collection of more samples from places in north eastern North America such as has been suggested by Levine (2007a; 2007b). Comparisons must be made against sources from Newfoundland, New Brunswick, Quebec, Maine, New York, New Jersey etc. and with hopes of the comparisons being made by LA-ICP-MS. By expanding the collection of source samples, exact provenance of the remaining seven groups could eventually be made. This would inform the reconstruction of trade networks as currently understood, as well as contribute to a deeper understanding

of how local aboriginal people were evolving their copper technology. For anyone continuing studies such as this, expanding the database of sources is imperative.

4.2 Laser ablation as an archeological tool

The use of laser ablation in chemical analysis is not a new notion. There have been scientists using laser ablation as far back as the early 1980s (Gray, 1985; Jackson et al., 1992; Aeschliman et al., 2004). However only recently has it been put to the test in archaeology (Junk, 2001; Garrison, 2003; Aeschliman et al., 2004; Cooper et al., 2008; Dussubieux et al., 2008; Lattanzi, 2008; Hill, 2012). Dominant methods for chemical characterization of trace elements were, for the most part, X-Ray Florescence (XRF) (Harbottle et al., 1982; Wisseman et al., 1998; Fitzgerald et al., 1993; Kobyliński et al., 1993; Bendall, 2003; Garrison, 2003; Constantinescu et al., 2001; Rapp & Hill, 2006; Abel & Burke 2014) and Instrumental Neutron Activation Analysis (INAA) (Rapp Jr et al., 1984; Turgeon, 1990; Hancock et al., 1991; Fitzgerald et al., 1993; Hancock et al., 1995; Leonard, 1996; Whitehead et al., 1998; Levine, 1999; Moreau & Hancock, 1999; Rapp et al., 2000; Garrison, 2003; Glascock et al., 2003; Anselmi, 2004; Rapp & Hill, 2006; Hancock et al., 2007; Levine, 2007a, 2007b; Mulholland & Pulford, 2007; Cooper et al., 2008; Pevarnik et al., 2008; Erhardt, 2009; Klein et al., 2010; Frame et al., 2013; Michelaki et al., 2013). These methods were considered for the most part to be the most nondestructive methods for chemical characterization of historical artifacts – until now. XRF and INAA methods require small pieces (no less than 100mg) of the artifact to be removed such as filings, or scrapings of the artifacts, whereas LA-ICP-MS can be performed on the entire artifact as one intact piece. The challenge with mounting the entire artifact into the ablation cell, is that pieces that are mounted are restricted by their size in the cell

(McFarlane, 2013 pers. comm.) Some pieces such as tiny artifacts like 863A and 863B, can be held in paraffin wax in hollowed epoxy pucks as mentioned above, and others can be mounted in bricks of paraffin wax to allow for stability. Overly large artifacts can have small portions of their edges analyzed as well, as was the case with 8609. A piece of the artifact which had already been compromised (<0.05 mg), was loaded into the ablation chamber and analyzed in lieu of the entire pot. Neutron activation also has the bonus addition of radiation in its methodology which means samples that have been analyzed cannot be returned to the collection. (Glascock et al., 2003; Rapp & Hill, 2006). Using laser ablation in the above mentioned methods, artifacts were able to be loaded directly into the ablation chamber, analyzed and then returned to the collection (Figure 2.1). LA-ICP-MS methodologies also have the added benefit of being a method of conducting in-situ analyses and not just bulk analyses (Aeschliman et al., 2004; Dussubieux et al., 2008; Cooper et al., 2008; Hill 2012) This means that any micro-inclusions of other minerals can be identified, and if need be, excluded (Figure 3.9, 3.10), whereas bulk analyses of the artifacts by INAA does not allow for this component. As the majority of provenance studies have stated the Michigan has been the most important source of copper this again brings into question how precise the INAA methods may actually be (Rapp Jr et al., 1984; Turgeon, 1990; Hancock et al., 1991; Fitzgerald et al., 1993; Hancock et al., 1995; Leonard, 1996; Whitehead et al., 1998; Levine, 1999; Moreau & Hancock, 1999; Rapp et al., 2000; Garrison, 2003; Glascock et al., 2003; Anselmi, 2004; Rapp & Hill, 2006; Hancock et al., 2007; Mulholland & Pulford, 2007; Cooper et al., 2008; Pevarnik et al., 2008; Erhardt, 2009; Klein et al., 2010; Frame et al., 2013; Michelaki et al., 2013). If inclusions were present in the studies performed by the above mentioned authors, the data could have been potentially skewed

in favour of Michigan, when in actuality, they matched samples from north-eastern North America. The only way to verify this hypothesis, would be to retest all of the artifacts analyzed by other authors using LA-ICP-MS methods and comparing the results to those obtained using INAA.

In terms of the ability of LA-ICP-MS to be a non-destructive method of trace-element analyses, the process of actually creating laser – ablation pits is ideal in comparison to methods such as XRF and INAA, as there is no need to drill into the artifact to obtain fresh copper. As the laser ablation occurred, it removed the layers of patina until the freshest copper of the core was exposed (Figure 2.1). Doing this leads to no visible or structural changes to the artifact, as pits are only visible at the microscopic level. Once the analyses of the artifacts were conducted, select artifacts were then verified using an SEM to determine if fresh copper had been reached (Figure 2.1 E & F), and in this case it was.

Limitations to LA-ICP-MS are notably the size of an artifact, and the appropriateness of standards created by analytical laboratories. Artifacts that were larger than the ablation cell, and did not have any already compromised edges, were excluded from the study as there was no adequate way to remove a piece of the artifact without compromising the structural integrity of the piece, this however can be avoided in the future as manufacturers of these machines have already begun to build larger and larger ablation cells (McFarlane, 2013 pers. comm.) Sizes and shapes of artifacts also presented limitations during analyses as irregular shaped artifacts had to be mounted in bricks of paraffin wax, but mounted in such a way as to still be visible and clear in the camera of the laser ablation chamber. Artifacts out of focus had to be removed from the cell, adjusted and then returned to try again this adds on to the sample preparation time, and eventually the analytical time which

is not always the most cost-effective way to analyze the artifacts, yet it still provides more accurate readings (Glascock, 2003; Rapp & Hill, 2006; Dussubieux et al., 2008; Hill, 2012). The appropriateness of standards was an issue during the first round of analyses in June of 2013, whereupon it was discovered that standards from the National Institute of Standards and Technology (NIST) were not ablating the same way as normal native copper. The first standards were flakes of copper and as the laser was striking the flakes, they were not ablating small craters like what was happening to the artifacts. This meant having to search out new copper standards that had a wide variety of elements already quantified, like what was found with the standards from MBH lab. As these standards came as pucks, it was easy to cut off edges, and mount them in epoxy for analyses. Once analyses had begun, these standards were checked to see if the ablation method was working. After analyses, the new standard were compared against their standard concentration certificates to determine what elements were being reported by the laser in the correct and acceptable concentrations. Doing such a quality control check using laser ablation allows for more standards to be used in quantification to ensure the highest possible levels of accuracy for the concentration (Lattanzi, 2007; Dussubieux et al., 2008; Hill, 2012). Another way to ensure the best possible results for chemical characterization is to use LA-ICP-MS with other bulk methods such as solution ICP-MS, and INAA, much like the work done by Cooper et al., (2008); Dussubieux et al., (2008); and Hill, (2012). The down side to using multiple methods of comparison, is the cost that would be associated with multiple types of analyses. As its own standalone method, especially in terms of non-destructive, in-situ analyses, laser ablation appears to be the most appropriate method that we have today (Rapp & Hill, 2006; Lattanzi, 2007; Dussubieux et al., 2008; Hill, 2012).

4.3 Implications in archaeology

This study has attempted to address several questions, however it now seems to have posed more than answered. Questions such as: what tools the aboriginal peoples were using to shape their tools, and how those tools may have allowed for contamination to either the copper piece or the tool? Bourque (2001) suggests that the aboriginal people were using stone tools and implements to pull small pieces of copper out of outcrop and cliff faces. If this was the case, when they were using cold annealing techniques, how did they avoid getting small fragments of their stone tools in the copper, or did they? By using LA-ICP-MS we can now begin to analyze micro-inclusions in the copper artifacts and continue working with archaeologists to determine if the inclusions are fragments or slags from other pieces or if they are geological inclusions, something already implied by Lattanzi (2007) and Hill (2012).

How and where aboriginal people were procuring the copper, whether it be from outcrop, or as many suggest: float copper moved during glaciation time (Turgeon, 1990; Hancock et al., 1991; Fitzgerald et al., 1993; Hancock et al., 1995; Leonard, 1996; Whitehead et al., 1998; Levine, 1999; Moreau & Hancock, 1999; Rapp et al., 2000; Mulholland & Pulford, 2007; Michelaki et al., 2013). Biggar (1992) suggests that the aboriginal people were picking it up off the ground and along beaches, however if copper was being collected from specific outcrops – as this study suggests, especially with the Cap d'Or samples – did these specific outcrops have a spiritual significance or were they being accessed just out of need, or convenience?. If this was the case, economic questions of supply and demand are then posed, and whether or not the limited availability of copper for use encouraged larger trade networks amongst several aboriginal groups and not just

necessarily other Mi'kmaq tribes. Turgeon (1990) talks in great detail about the significance placed on copper once it was in use, and how the Mi'kmaq were assigning spiritual meaning to different sources of copper. For example, aboriginal people believed that "red copper" – copper found and procured in North America was valuable spiritually and representative of blood, and that "yellow copper" - the higher Zn containing copper that was coming from the Europeans – was also special as it was unlike anything the Mi'kmaq could procure here (Turgeon, 1990). The findings in this study help to affirm that the Mi'kmaq did in fact highly value their yellow copper, as they would have been recycling and reusing it for other purposes. The artifacts in provenance group I have chemistries consistent with the literature for the type of copper being brought over by the Europeans as pots, even though the pieces look nothing like pots now. Larger pieces may have become damaged or no longer required and turned into something else, similar to what we see with the tinkling cone that is artifact 20. It is also possible that if one aboriginal group no longer needed specific copper items, they could have been trading with another group who then could have turned pieces into other things (Hancock et al., 1991; Turgeon 1991; Fitzgerald et al., 1993; Whitehead 1993; Hancock et al., 1995; Leonard 1996; Whitehead 1997; Rapp et al., 2000; Bourque, 2001; Fenn, 2001; Lattanzi, 2007; Cooper et al., 2008; Dussubieux et al., 2008; Ehrhardt 2009; Klein et al., 2010; Cooper 2011; Hill, 2012; Michelaki, 2013).

Further work should also be done with archaeologists and environmental geologists to study soil samples from the archaeological sites, and better understand the weathering processes. Doing this will help to ensure a better understanding of how elements such as Zn are "preferentially depleted" in highly weathered samples (Dussubieux et al., 2008) and how the trace elements may leech into the soil surrounding the immediate area the artifacts were uncovered. This could also be useful in better understanding how the reverse could happen, and trace elements from deep within the ground could begin to affect the chemistry of the patina coating an artifact, or even the artifact itself. This would be an additional check again to see if the patina of an artifact can be used to test for provenance and once again negate the requirement to have fresh exposed copper from an artifact.

5.0 Conclusion

The main goal of this study was to determine the geological provenance of copper used by the pre- to post-contact aboriginal peoples in Nova Scotia through non-destructive analytical methods. The ability to determine the original source of copper now contained within artifacts, and to discriminate between natural copper and copper of European origin helps to increase our understanding of the lives of aboriginal people, how they made objects of spiritual or functional value, where they travelled and who they traded with. Using a relatively non-destructive (compared to bulk methods used in other studies), it was possible to determine with an acceptable level of certainty, the provenance of approximately a third of the Nova Scotia Museum copper collection in this historical context. Three definitive groups were identified: two groups sourced from within what is now Nova Scotia (Margaretsville, and Cap d'Or) and one group of European-sourced copper (refined copper and copper-based alloys with Sn, Zn and other metals). These artifacts have been analyzed, and returned to the copper collection of the Nova Scotia Museum, to be curated for exhibits, and used again in future studies. No artifacts used in this study were compromised visually or structurally; there were no negative impacts to the value of these cultural objects. Rather, the study has provided an opportunity to develop positive insights concerning the copper procurement traditions of the Mi'kmaq who clearly utilized their own copper from outcrops in what is now Nova Scotia in conflict with the Lake Superior model, and concerning the trade and reuse of copper brought over by European settlers and explorers. Future work stemming from this project should include the creation of a larger database of source copper localities to explain (hopefully) the provenance of the remaining two thirds of the copper artifact collection that was not Michigan-sourced, nor from key copper areas of the

Bay of Fundy. Work in progress by Hodge et al. (in preparation) is narrowing down the sources copper used in the European artifacts. Increasing the size of the database for sources will aide us in understanding further copper was being gathered and how it moved to its final place in the possession of aboriginal peoples in Nova Scotia before its discovery through archaeological excavation. The project has raised several key questions that could be addressed through integration of the chemical provenance data and archaeological data as well as further study:

- Why was Michigan copper not used? Did this reflect a lack of trading relationship with other groups that had access to this copper? Was NS copper preferred because it was easier to manipulate and work (i.e., small crystals vs. large float fragments) or was it preferred because of spiritual connection or tradition?
- 2. What are the sources to explain the seven unknown provenance groups? Were these local sources and if so, are the documented currently or historically? If they were sourced from other parts of what is now the Maritime region or north-eastern United States, how does this better inform us of the relationships between neighbouring aboriginal groups?
- 3. Can the diversity in sources for artifacts recovered at an individual archaeological site reflect reuse of copper sourced from different areas over generations? Are variations in source material represented in artifact populations linked to the age of a particular area of the site and do these variations reflect changes in the availability of copper from different localities with time?
- 4. Was NS copper more prevalent than previously thought? Given the limitations in bulk analytical methods discussed here, will reanalysis of samples from other sites

in North America by LA-ICPMS tighten constraints on copper provenance, revealing a greater role for copper from the Bay of Fundy region in North American aboriginal cultures prior to European contact?

5. Where was the copper in European objects originally derived? Can constraints on their provenance and the production history for refined metals in Europe in general allow a better understanding of the age of sites of habitation, contact and trade involving Mi'Kmaq and European explorers and colonists? Can the chemistry of refined copper fragments be used to identify the European nation that brought the original objects (e.g., trade kettles) to eastern Canada?

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Appendix A – Laser Ablation Data for Artifacts

| | ³¹ P | Ste | ³ Cr | ⁵⁵ Min | ⁵⁶ Fe | ⁵⁹ Co | IN09 | uZ ⁵⁶ Zn | 71Ga | ⁷² Ge | 75As | oW ²⁶ | ¹⁰⁷ Ag | m cd | IISIN . | ¹¹⁸ Sn | 121Sb | ¹²⁵ Te | ¹⁹⁷ Au | ²⁰² Hg | ²⁰⁸ Pb | ²⁰⁹ Bi |
|------------------------------------------|-----------------|--------|-----------------|-------------------|------------------|------------------|----------|---------------------|-------|------------------|----------|------------------|-------------------|------|---------|-------------------|----------|-------------------|-------------------|-------------------|-------------------|-------------------|
| A 0570 1 | 60 1191 | 40 HBM | ADD 09 | ICCHW | 00 HBM | MBH 09 | 40 LIGIN | 40 HBM | ICCPU | 00 LIGIN | 40 LIGIN | ICCHM | 40 HBM | 00 U | ADD 09 | 7/ HBM | 0 HBH 09 | 0 1 Q | 00 HBM | ICCEN | 00 HBM | 00 HBM |
| 1-6000 | 010 | 162 | 6.7 | | 000 | 0.15 | 1.1 | 10 | 0.10 | 15 | 210 | 0.10 | 010 | 66.0 | 10.0 | 50 | 0.14 | 01.0 | 0.00 | 0.66 | 10.1 | 20.06 |
| 8569-3 | 550 | 189 | 0.75 | 1 | 42 | 0.08 | 1.24 | 18.3 | 0.22 | 0.6 | 1.31 | 0.41 | 220 | 0.15 | 0.01 | 1.70 | 0.2 | 10.0 | 0.02 | 0.64 | 0.46 | 0.02 |
| 8569-4 | 580 | 211 | 0.95 | 0.64 | 42 | 0.17 | 2.5 | 18 | 0.24 | -0.04 | 1.38 | 0.1 | 56 | 0.12 | 0.01 | 0.04 | 0.16 | 0.03 | 0 | 0.64 | 0.14 | 0.02 |
| 8569-5 | 131 | 215 | 0.64 | 0.78 | 21 | 0.04 | 0.56 | 7.5 | 0.03 | 0.27 | 0.9 | 0.15 | 195 | 0.34 | 0.01 | 0.05 | 0.04 | 0.05 | 0 | 0.39 | 0.19 | 0.01 |
| 8569-6 | 340 | 250 | 1.58 | 1.19 | 210 | 0.04 | 1.3 | 15.3 | -0.06 | 0.75 | 1.48 | 0.23 | 139 | 0.12 | 0 | 0.03 | 0.12 | 0.02 | 0 | 0.48 | 0.27 | 0.01 |
| 8569-7 | 92 | 267 | 0.38 | 1.38 | 70 | 0.04 | 9.0 | 7.4 | 0.27 | 0.31 | 0.86 | 0.24 | 272 | 90.0 | 0.01 | 0.03 | 0.08 | 0.08 | 0 | 0.42 | 0.12 | 0.02 |
| 8569-8 | 257 | 271 | 1.29 | 0.24 | 09 | 0.09 | 0.8 | 14.1 | 0.14 | 0.00 | 0.74 | 0.15 | 101 | 0.03 | 0 | 0.02 | 0.05 | 0.07 | 0 | 0.47 | 0.13 | 0 |
| 8569-9 | 480 | 194 | 1.03 | 16:0 | 28 | 0.16 | 0.58 | 34 | 0.20 | -0.49 | 1.55 | 0.1 | 319 | 0.15 | 0 | 0.04 | 0.12 | 0.01 | 0 | 0.36 | 0.15 | 0.01 |
| 8569-10 | 880 | 215 | 1.4 | 4.4 | 200 | 0.21 | 0.71 | 27 | 0.16 | 0.37 | 1.61 | 0.08 | 1090 | 0.18 | 0 | 0.11 | 0.01 | 0.04 | 0 | 0.72 | 0.24 | 0.01 |
| 8596-1 | 17200 | 315 | 15.7 | 1080 | 680 | 2.7 | 47 | 369 | 2.63 | 1.17 | 14.4 | 0.18 | 19.6 | 0.53 | 0.04 | 0.78 | 0.14 | 0.05 | 0 | 0.34 | 1.92 | 0.68 |
| 8596-2 | 28700 | 536 | 23.1 | 750 | 630 | 2.98 | 17 | 500 | 3.70 | 0.69 | 16.5 | 0.16 | 10.4 | 1 | 0.05 | 0.83 | 0.48 | 0.1 | 0 | 0.41 | 2.67 | 0.04 |
| 8596-3 | 11300 | 328 | 10.1 | 150 | 320 | 0.7 | 5.2 | 157 | 1.12 | 0.65 | 8.7 | 0.24 | 12.6 | 0.55 | 0.01 | 0.38 | 0.21 | 0.05 | 0 | 0.26 | 4 | 0.05 |
| 8596-4 | 17100 | 393 | 11.7 | 150 | 270 | 1.64 | 10.7 | 159 | 1.67 | 0.37 | 8.6 | 0.14 | 4.5 | 0.82 | 0.02 | 0.18 | 0.22 | 0.01 | 0 | 0.19 | 1.36 | 0.04 |
| 8596-5 | 15000 | 367 | 10.9 | 630 | 168 | 0.97 | п | 121 | 0.68 | -0.29 | 9.9 | 0.1 | 6.6 | 0.45 | 0.01 | 0.21 | 0.04 | 0.06 | 0 | 0.26 | 1.26 | 0.04 |
| 8596-6 | 13200 | 344 | 11.5 | 8 | 145 | 0.84 | 6.2 | 95 | 06.0 | 0.43 | 10.4 | 0.2 | 2 | 0.3 | 0.01 | 0.56 | 0.09 | 0.04 | 0 | 0.15 | 1.13 | 0.07 |
| 8596-7 | 45600 | 362 | 33.5 | 254 | 308 | 3.1 | 42 | 350 | 2.97 | 1 | 21.2 | 0.27 | 28.9 | 0.66 | 0.08 | 0.25 | 2 | - | -0.01 | 0.39 | 4.1 | 60.0 |
| 8596-8 | 15200 | 351 | 10.9 | 135 | 152 | 1.03 | 4 | 170 | 0.96 | 0.33 | 16.3 | -0.01 | 15.7 | 0.4 | 0.01 | 0.19 | 0.08 | 0.02 | 0 | 0.22 | 1.16 | 0.03 |
| 8596-9 | 20400 | 403 | 14.9 | 101 | 133 | 1.65 | 10.4 | 185 | 0.46 | 0.23 | 14.7 | 0.12 | 13.8 | 0.9 | 0.02 | 0.16 | 0.07 | 0.06 | 0 | 0.33 | 0.88 | 0.03 |
| 8596-10 | 50900 | 549 | 30.5 | 300 | 280 | 1.51 | 10.9 | 276 | 1.95 | -0.06 | 21.3 | 0.04 | 17.1 | 2.19 | 0.01 | 0.32 | 0.15 | 0.16 | 0 | 0.21 | 3.4 | 0.25 |
| 8584-1 | 97200 | 286 | 6.7 | 214 | 150 | 0.47 | 3.5 | 211 | 2.3 | 0 | 38.5 | 0.36 | 2070 | 1.15 | 0.33 | 0.38 | 0.4 | 0.12 | 0.01 | 6 | 5.7 | 0.02 |
| 8584-2 | 153000 | 657 | 9.1 | 376 | 262 | 0.38 | 3.3 | 243 | 3.2 | - | 38.7 | 0.05 | 21900 | 0.82 | 0.02 | 0.45 | 0.36 | 0.05 | 0.01 | 21.6 | 1.87 | 0.03 |
| 8584-3 | 151000 | 671 | 10.4 | 656 | 980 | 0.4 | 6 | 325 | 5 | 0.15 | 34.2 | 0.17 | 5800 | 1.26 | 0.05 | 0.46 | 0.2 | 0.01 | 0.01 | 7.6 | 1.54 | 0.02 |
| 8584-4 | 127000 | 462 | 8.0 | 820 | 580 | 0.29 | 4.62 | 266 | 4.43 | 0.93 | 33 | 0.37 | 1230 | 0.97 | 0.01 | 0.21 | 0.39 | 0.1 | 0 | 10.9 | 3.3 | 0.06 |
| 8584-5 | 120000 | 401 | 7.36 | 557 | 1050 | 1.8 | 10.6 | 204 | 5.7 | 0.41 | 34.7 | 0.21 | 1330 | 0.72 | - | 1.8 | 0.31 | 0.17 | 0.01 | 7.9 | 2.6 | 0.14 |
| 8584-6 | 172000 | 731 | 9.2 | 920 | 640 | 0.37 | 4.3 | 410 | 10.9 | 2.4 | 31.7 | 0.41 | 1820 | 1.31 | 0.01 | 0.39 | 0.33 | 0.03 | 0.01 | 12 | 4.9 | 0.02 |
| 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1- | 180000 | 108 | 8.8 | 876 | 0511 | 1.0 | 4.2 | 356 | 19.5 | 19.0 | 30.1 | 0.38 | 1290 | 1.03 | 0.02 | 0.12 | 0.22 | 0.03 | 0.04 | | 1.4 | 10.0 |
| 8-9868 | 1/3000 | 140 | C.6 | 066 | 0/71 | 91.0 | 4.0 | 675 | 5.0 | • : | 8.17 | /0.0 | 14/0 | 1.05 | 70'0 | /1.0 | 01.0 | 0.0 | 10.0 | 11 | t.0 | c0.0 |
| 8584-10 | 117000 | 305 | 10.4 | 010 | 430 | 10.0 | 0.0 | 176 | 0.6 | 11 | 37.4 | 4.7 | 0671 | 3.4 | 10.0 | 0.19 | 41 | cn.0 | C7.0 | 3 5 | 25 | 570 |
| 8603-1 | 110000 | 619 | v | 000 | 008 | 200 | 49 | 860 | 217 | 70.07 | 206 | 1 26 | 13.3 | 0 88 | 040 | 01 | 0.18 | 100 | 10.0 | 0.47 | 171 | 0.11 |
| 8603-2 | 45900 | 106 | 1.34 | 24.1 | 62 | 1 | 1.7 | 326 | 1.11 | 0.34 | 9.5 | 0.34 | 15.2 | 0.35 | 0 | 0.13 | 0.06 | 0.01 | 0 | 0.17 | 0.4 | 0.02 |
| 8603-3 | 52300 | 87.5 | 2.02 | 37 | 101 | 0.29 | 5.2 | 372 | 0.92 | -0.01 | 13.3 | 0.49 | 11.8 | 0.53 | 0.02 | 0.93 | 0.15 | 0.01 | 0 | 0.27 | 0.73 | 0.08 |
| 8603-4 | 38100 | 138 | 1.18 | 12.1 | 70 | 0.04 | 1.4 | 258 | 0.59 | 0.28 | 8.1 | 0.08 | 13.1 | 0.27 | 0.01 | 0.25 | 0.05 | 0.02 | 0.01 | 0.39 | 0.17 | 0.04 |
| 8603-5 | 121000 | 54.4 | 4.24 | 67 | 1400 | 3 | 6.2 | 883 | 3.10 | 0.38 | 22.9 | 0.92 | 14.4 | 0.94 | 0.14 | 1.6 | 0.15 | 0.04 | 0.01 | 0.42 | 17 | 0.3 |
| 8603-6 | 44200 | 127 | 1.53 | 12.7 | 158 | 0.44 | 1.95 | 281 | 0.7 | 1.1 | 9.5 | 0.05 | 21.4 | 0.3 | 0.01 | 0.14 | 60.0 | 0.01 | 0.02 | 0.34 | 3.8 | 0.09 |
| 8603-7 | 86600 | 72.4 | 2.35 | 33 | 580 | 0.42 | 2.16 | 570 | 1.2 | 0.01 | 14.7 | 0.39 | 22.2 | 0.48 | 0.01 | 0.16 | 0.23 | 0.04 | 0 | 0.21 | 0.49 | 0.02 |
| 8603-8 | 85100 | 91.2 | 2.54 | 41.6 | 1200 | 0.31 | 2.3 | 589 | 1.89 | 1.8 | 19 | 0.34 | 14.5 | 0.49 | 0.01 | 1.6 | 0.07 | 0.02 | 0 | 0.37 | 5.8 | 0.03 |
| 8603-9 | 63900 | 5.68 | 1.99 | 38 | 079 | 4 | 7.7 | 455 | 1.61 | -0.04 | 12.13 | 15.0 | 5.61 | 0.00 | 77.0 | 0.62 | 4.0 | 20.0 | 0 | 17.0 | c/.0 | 0.02 |
| 01-5000 | 00000 | 159 | 4 80 | 70 | 740 | 10.36 | n (* | 7/4 | 1 57 | 21.0 | C.CI | 10 | 30 | 10.0 | 0.00 | <u></u> | 10.0 | 20.0 | 10.0 | 25.0 | 16.0 | 10.0 |
| 8595-2 | 45300 | 0.90 | 2.46 | 150 | 168 | 0.38 | 35 | 908 | 0.74 | 0.65 | 624 | 0.0 | 43.7 | 0 51 | 0.04 | 0.50 | 0.16 | 0.04 | 0.01 | 0.28 | 0.8 | 0.06 |
| 8595-3 | 20200 | 126 | 1.62 | 57 | 147 | 0.10 | 0.87 | 235 | 0.65 | 0.23 | 4.86 | 0.15 | 43.4 | 0.44 | 0.05 | 0.1 | 0.11 | 0.02 | 0.01 | 0.34 | 11 | 0.04 |
| 8595-4 | 32800 | 126 | 1.63 | 30 | 11 | 0.14 | 1.5 | 184 | 0.58 | 0.33 | 4.2 | -0.17 | 43.9 | 0.38 | 0 | 0.18 | 0.14 | 0.02 | 0 | 0.35 | 0.45 | 0.04 |
| 8595-5 | 27700 | 155 | 1.48 | 50 | 160 | 0.03 | 0.8 | 268 | 0.73 | 0.57 | 3.64 | -0.13 | 42.1 | 0.52 | 0.01 | 0.11 | 0.9 | 0.04 | 0 | 0.25 | 0.44 | 0.08 |
| 8595-6 | 20900 | 153 | 1.75 | Π | 34 | 0.03 | 2 | 77 | 0.15 | -0.2 | 2.7 | 0.02 | 35.2 | 0.17 | 0.01 | 0.14 | 0.04 | 0.02 | 0.01 | 0.21 | 0.22 | 0.01 |
| 8595-7 | 25500 | 131 | 1.22 | 45 | 101 | 0.11 | 1.4 | 177 | 0.39 | -0.08 | 5.1 | 0.13 | 34.0 | 0.14 | 0.01 | 0.23 | 0.13 | 0.05 | 0.01 | 0.17 | 0.33 | 0.03 |
| 8595-8 | 46300 | 127 | 2.64 | 83 | 206 | - | 4.3 | 421 | 0.88 | 0.11 | 6.1 | 0.34 | 41.6 | 0.49 | 0.01 | 1.01 | 0.11 | 0.09 | 0.0 | 0.36 | 0.79 | 0.08 |
| 8595-9 | 31000 | 122 | 1.66 | 4 6 | 140 | 0.16 | 1.38 | 164 | 0.49 | -0.02 | 4.8 | 0.15 | 42.7 | 0.28 | 0.02 | 0.07 | 0.15 | 0.08 | 0.01 | 0.32 | 0.75 | 0.08 |
| 01-0600 | 00600 | 103 | +0.4 | 007 | 450 | cc.0 | C0.C | 400 | CI | 0.42 | 01.4 | 7.0 | C.C2 | 1.01 | c0.0 | 10'0 | cc.0 | 10.0 | 10.0 | CC.0 | 0.1 | 01.0 |

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| 600 85 106 12 480 5.2 3.02 1.6 2.16 0.26 2.2 480 5.2 3.82 0.17 13.2 0.28 2.290 0.68 0.33 0.02 9.4 0.19 450 0.3 1.01 0.37 13.2 0.28 1390 0.68 0.65 0.31 11.2 0.28 1390 0.68 0.75 0.35 8.8 0.26 1000 0.32 0.75 0.35 8.8 0.26 1000 0.32 0.76 0.35 17 0.14 470 0.12 0.06 0.15 0.9 0.16 83 0.07 0.06 0.15 0.9 0.16 83 0.07 0.06 0.15 2.09 0.03 99.7 0.05 0.07 0.01 2.03 0.03 99.7 0.05 0.06 0.11 0.03 < | 600 85 106 12 480 5.2 3.22 1.6 1.2 4.80 5.2 0.33 0.17 1.3.2 0.28 1.290 0.68 0.33 0.02 9.4 0.19 450 0.3 1.01 0.37 13.2 0.28 1390 0.68 0.75 0.35 13.1 0.27 330 0.39 0.75 0.35 8.8 0.26 1000 0.32 1.84 0.35 15.6 0.24 1030 0.32 0.04 0.11 1.77 0.14 470 0.12 0.06 0.3 7 0.19 937 0.07 0.06 0.3 2.39 0.39 0.07 0.01 0.06 0.3 2.39 0.39 0.07 0.02 0.06 0.3 0.30 0.38 0.07 0.03 0.06 0.3 0.30 0.39 0.07 | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| 0.88 0.17 13.2 0.28 0.32 0.02 9.4 0.19 0.6 0.37 12.1 0.08 0.6 0.37 11.2 0.08 0.75 0.35 8.8 0.26 0.74 0.35 15.6 0.24 0.90 0.36 15.6 0.24 0.90 0.36 15.6 0.24 0.90 0.31 11.7 0.19 0.00 0.3 15.6 0.24 0.00 0.3 15.6 0.24 0.00 0.3 15.6 0.24 0.01 0.3 15.6 0.24 0.00 0.3 17 0.14 0.01 1.7 0.14 0.15 0.00 0.15 0.9 0.16 0.28 0.01 2.39 0.28 0.01 0.01 2.03 0.02 0.01 0.01 2.03 0.02 | 0.88 0.17 13.2 0.28 0.32 0.02 9.4 0.19 0.66 0.11 11.2 0.08 0.66 0.11 11.3 0.28 0.75 0.35 8.8 0.27 1.84 0.35 15.6 0.24 0.06 0.31 11.3 0.08 0.06 0.35 15.6 0.24 0.06 0.11 1.77 0.19 0.06 0.13 1.77 0.14 0.06 0.15 0.99 0.16 0.06 0.15 2.99 0.28 0.07 0.01 2.03 0.03 0.07 0.01 2.03 0.03 0.07 0.01 2.03 0.03 0.07 0.01 2.93 0.03 0.07 0.01 0.04 0.01 0.07 0.04 0.01 0.02 0.07 0.04 0.01 0.03 | 0.17 1132 0.28 0.237 112.1 0.08 0.31 113.1 0.08 0.35 15.6 0.24 0.35 15.6 0.24 0.35 15.6 0.24 0.35 15.6 0.24 0.35 15.6 0.24 0.19 0.19 0.11 11.7 0.14 0.15 0.9 0.13 0.01 2.03 0.03 0.01 2.03 0.03 0.01 2.03 0.03 0.01 0.43 0.13 0.01 0.43 0.13 0.02 0.03 0.03 0.03 |
| 0.32 0.02 0.6 0.11 0.75 0.33 0.75 0.33 0.75 0.33 0.06 0.3 0.06 0.15 0.06 0.15 0.01 0.0 | 0.37 0.65 0.75 0.75 0.75 0.36 0.11 0.36 0.15 0.06 0.15 0.06 0.15 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.01 0.01 0.01 0.02 0.01 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.01 0.02 0.01 0.01 0.01 0.02 0.01 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.01 0.02 0.01 0.01 0.01 0.01 0.02 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 | 0.02 0.11 0.11 0.35 0.36 0.13 0.13 0.14 0.01 0.01 0.01 0.01 0.01 0.02 0.02 0.02 |
| | | 0.6 0.75 0.75 0.06 0.06 0.06 0.05 0.07 0.07 0.07 0.75 |
| 1.3 145 1.7 53 0.1 7.9 1.3 115.1 0.1 7.9 0.8 22.1 0.6 8.1 0.6 4.0 | Li 113 114 117 117 113 114 113 114 01 01 01 01 01 01 01 01 01 01 01 01 01 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| 2.65 0.06 1 0.38 1.9 0 0.22 0.17 1 0.46 0.25 0 1.28 0.15 0 1.28 0.15 0 0.15 0 0.17 0 0.17 0 0.15 0 0.17 0 0.15 0 0.17 0 0.15 0 0.00 0 0.15 0 0.00 0 0.15 0 0.00 0 0.15 0 0.00 0 0.15 0 0.00 0 0.15 0 0.00 0 0 0.00 0 0.00 0 0.00 0 0 0.00 0 0 0.00 0 0 0.00 0 0 0.00 0 0 0.00 0 0 0.00 0 0 0 0 0 | 2.65 0.06 1 0.38 1.9 0.05 0.46 0.27 0.17 1.28 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 | 2.65 0.06 1 0.38 1.9 0 0.38 1.9 0 0.22 0.17 1 0.46 0.25 0 1.37 0.05 0 1.37 0.02 0 0.46 0.25 0 1.37 0.02 0 0.42 0.03 0 0.42 0.03 0 0.42 0.01 0 0.35 0.01 0 0.35 0.01 0 0.35 0.01 0 0.35 0.01 0 1.27 0.14 0 1.700 0.15 0 1.790 0.11 0 |
| 03 0.96 0.22 22 4.4 0.46 31 2.74 1.28 31 1.85 1.37 | 03 0.96 0.22 222 4.4 0.46 31 2.74 1.28 331 1.85 1.37 0.8 0.5 0.42 0.8 0.5 0.42 0.1 0.33 0.36 0.7 1.36 1.27 0.7 1.34 3.33 | 0.22 0.46 0.46 1.37 0.36 0.36 1.27 1.27 1.790 1500 |
| 228 0.31 205 0.31 107 0.08 | 0.01 0.02 0.07 0.07 0.07 | 2.74 1.85 0.5 0.33 1.86 1.86 1.47 147 50 |
| 7/1 | | 0.01 0.33 0.07 1.86 0.26 1.34 1.05 147 0.31 50 |

| - 000 | MBH 66 | 0.29 | 0.19 | 0.18 | 0.08 | 0.15 | 51.0 | 0.28 | 0.38 | 0.17 | 1.1 | 0.74 | 1.38 | 1.08 | 1.15 | 1.32 | 2.56 | 1.76 | 0.80 | 2.60 | 10.0 | 0.01 | 0 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.07 | 0.01 | 0 | 0 | 0 0 | 0.07 | 0 | 0.01 | 0.02 | 0 | 0.03 | 0.03 | 0.01 | 0.03 | 0.04 | 0.16 | 0.16 | 0.24 | |
|-------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|---------|-------|---------|---------|---------|---------|---------|---------|-------|----------|----------|---------|--------|--------|----------|----------|----------|----------|-----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|---------|---------|-------|---------|---------|---------|---------|---------|-------|
| 306 | MBH 66 | 1.39 | 1.11 | 0.74 | 0.77 | 0.95 | 15.7 | 1.45 | 1.49 | 2.33 | 384 | 256 | 766 | 756 | 408 | 261 | 770 | 1137 | 908 | 1480 | 60.0 | 75.0 | 0.43 | 0.51 | 1.03 | 0.51 | 0.29 | 0.14 | 1.48 | 0.55 | 1.5 | 0.28 | 0.19 | 0.14 | 0.22 | 0.18 | 0.14 | 0.66 | 9.4 | 6 | 1.86 | 3.1 | 6.08 | 6.52 | 1.61 | 7.9 | |
| WC | ISSIM | 0.64 | 0.57 | 0.47 | 0.45 | 0.55 | 0.65 | 0.53 | 0.6 | 0.73 | 265 | 81 | 96 | 217 | 60 | 88 | 147 | 153 | 41 | 611 | 041 | | 508 | 233 | 264 | 128 | 113 | 09 | 240 | 82 | 46.2 | 134 | 58.2 | 53.7 | 50.9 | 60.3 | 56 | 218 | 1.11 | 10.9 | 5.62 | 10.3 | 30.7 | 39.5 | 26 | 32.2 | |
| 107 . | MBH 66 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 | 10.0 | 10.0 | 0.01 | 0.01 | 0.79 | 0.77 | 0.88 | 0.75 | 0.96 | 1.05 | 1.41 | 1.02 | 0.68 | 0.77 | | 0 0 | | 0 | 0.01 | 0.01 | 0.01 | 0.01 | 0 | 0 | 0.01 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0.03 | 0.01 | 0 | 0.01 | 0.01 | 0.02 | 0 0 | 0 | |
| 176 | MBH 69 | 0.02 | 0.11 | 0.05 | 0.14 | 0.11 | -0.04 | 01.0 | 0.17 | 0.62 | 0.66 | 0.57 | 0.76 | 96.0 | 0.36 | 0.87 | 1.4 | 0.92 | 0.0 | 8/.0 | 40.0 | 70.0 | 0.03 | -0.02 | 0.01 | 0.03 | 0.07 | 0.04 | -0.01 | 0.01 | 0.02 | 0 | 0.04 | 0.04 | 0.0 | 0.03 | 0.06 | 0.05 | 0.08 | 0.01 | 0.07 | 0.07 | -0.09 | 0.22 | 0.16 | 60.0 | |
| 121- | MBH 69 | 0.18 | 0.17 | 0.1 | 0.11 | 0.11 | 0.10 | 60.0 | 0.14 | 0.13 | 6.90 | 3.6 | 12.6 | 12.3 | 4.3 | 4.8 | 5.68 | 10.3 | 6.1 | 14 | 0.00 | 70.0 | 0.03 | 0.01 | 0.07 | 0.08 | 0.01 | 0.03 | 0.22 | 0.1 | 0.23 | 0.07 | 0.22 | 0.03 | 0.05 | 0.03 | 0.05 | 0.1 | 0.17 | 0.23 | 0.06 | 60.0 | 0.19 | 0.19 | 0.62 | 1.9 | 0 20 |
| 118- | MBH 72 | 0.23 | 0.24 | 0.1 | 0.11 | 0.06 | 61.0 | 60.0 | 0.2 | 0.42 | 31.2 | 19.4 | 21.6 | 27 | 21.8 | 19.9 | 25.7 | 30.3 | 20.2 | 24 | 0.08 | CT'0 | 0.05 | 0.04 | 0.43 | 0.23 | 0.13 | 0 | 1.09 | 1.86 | 0.26 | 0.36 | 0.45 | 0.26 | 0.17 | 0.06 | 0.01 | 0.09 | 28 | 21 | 2.05 | 2.9 | 16 | 1.7 | 24.3 | 6.4 | 00 |
| 116. | MBH 69 | 0.01 | 0 | 0 | 0 | 0 0 | 0 | 10.0 | 0 | 0 | 0.05 | 0.03 | 0.04 | 0.05 | 0.04 | 0.04 | 0.04 | 0.04 | 0.02 | c0.0 | | | | 0 | 0.01 | 0 | 0 | 0 | 0.01 | 0 | 0 | -0.01 | 0 | 0 | 0 | 0.01 | 0 | 0 | 0.01 | 0.01 | -0.01 | 0.02 | 0.02 | 0.12 | 1.0 | 0.27 | 0.18 |
| 111 | MBH 69 | 0.22 | 0.17 | 0.17 | 0.14 | 0.15 | 010 | 0.22 | 0.07 | 0.26 | 4.72 | 2.97 | 7.36 | 8.9 | 2.77 | 4.08 | 5.57 | 11.1 | 27.0 | cl.1 | 0.07 | 10.0 | 0.16 | 0.15 | 0.16 | 0.16 | 0.17 | 0.06 | 0.69 | 0.07 | 0.24 | 0.92 | 0.34 | 0.11 | 0.21 | 0.2 | 0.08 | 0.16 | 0.39 | 0.87 | 0.29 | 0.54 | 1.88 | 2.59 | 2.95 | 1.85 | 1 0 |
| 107 . | MBH 69 | 55 | 60.4 | 53.3 | 42.4 | 42 | 617 | 212 | 83 | 84 | 270 | 558 | 367 | 372 | 423 | 582 | 850 | 462 | 405 | 525 | 671 | 102 | 318 | 144 | 217 | 354 | 226 | 248 | 256 | 225 | 132 | 307 | 479 | 262 | 212 | 167 | 68.4 | 127 | 6.04 | 64.5 | 25 | 59 | 10.9 | 13.5 | 19.8 | 15.7 | 000 |
| 04.10 | MASSI | 0.29 | 0.28 | 0.13 | 0.02 | 0.13 | 61.0 | 0.11 | 0.17 | -0.04 | 2.49 | 0.82 | 0.53 | 4.2 | 0.43 | 1.01 | 1.74 | 1.35 | 0.34 | 0.34 | CI.U | 00.0 | 0.27 | 0.05 | 0.12 | 0.17 | 60.0 | 0.1 | 0.1 | 0.22 | 0.08 | 0.25 | 0.19 | 0.22 | 0.07 | 0.15 | 0.21 | 0.1 | 0.57 | 0.62 | 0.57 | 0.66 | 0.85 | 0.66 | 1.41 | 0.79 | 1 8 |
| 74 . | MBH 69 | 22.7 | 17.1 | 17 | 14.6 | 18 | 10.3 | 13.5 | II | 5.9 | 134 | 66 | 194 | 250 | 93 | 67 | 159 | 310 | 111 | 667 | 1.14 | 04-1 | 1.17 | 1.27 | 2.09 | 1.47 | 1.05 | 0.92 | 5.7 | 1.03 | 1.22 | 1.05 | 1.24 | 0.67 | 0.88 | 0.87 | 0.31 | 1.57 | 24.8 | 64.8 | 12.9 | 37.4 | 131.7 | 125 | 213 | 89.2 | 015 |
| - 11 | MBH 66 | 0.15 | 0.13 | 0.36 | 0.38 | 0.19 | 0.07 | 69.0 | 0.15 | 0.4 | -0.25 | 0.12 | 0.18 | 0.28 | 0.09 | 1.25 | 1.57 | 0.32 | 0.11 | -0.31 | 95.U | cc.0 | 10.0- | -0.1 | 0.28 | -0.1 | 0.06 | -0.11 | 0.43 | 0.11 | 0.11 | -0.1 | 0.06 | 0.16 | 0.4 | 0.08 | 0.21 | 0.13 | 0.45 | 0.31 | 0.18 | 0.31 | 0.43 | 0.94 | 5.0 | 0.19 | 0 87 |
| - 16 | MASSI | 3.69 | 2.72 | 1.98 | 1.75 | 2.54 | 7 96 | 2.23 | 1.82 | 0.81 | 1.06 | 0.5 | 0.14 | 1.41 | 0.27 | 3.11 | 0.91 | 0.4 | 0.23 | 0.22 | 61.0 | 01.0 | 60.0 | 0.11 | 0.17 | 0.19 | 0.19 | 0.1 | 1.86 | 0.16 | 0.12 | 0.14 | 0.15 | 0.16 | 0.18 | 0.19 | 0.19 | 0.14 | 0.37 | 0.55 | 0.15 | 0.49 | 1.84 | 2.4 | 15.8 | 1.95 | 2 67 |
| | MBH 69 | III | 92 | 84 | 85 | 84.7 | 13.1 | 11 | 09 | 37.4 | 7700 | 4840 | 6800 | 13100 | 3800 | 7740 | 8800 | 7680 | 0000 | 0/.99 | 4.60 | 0.40 | 47.3 | 38.2 | 58.0 | 48.2 | 64.0 | 26.8 | 174 | 38.7 | 21.8 | 29.8 | 24 | 17 | 29 | 43 | 32 | 58 | 70 | 50 | 9.7 | 16 | 103 | 134 | 550 | 119 | 174 |
| | MBH 69 | 1.15 | 0.64 | 0.57 | 0.66 | 0.17 | 7.06 | 1.25 | 1.2 | 1.3 | 135 | 88 | 121 | 256 | 65.1 | 161 | 169 | 161 | 1.101 | 126 | 0.32 | | -0.21 | 0.19 | 0.03 | 0.38 | 0.05 | 0.05 | 7.9 | 0.45 | 0.65 | 1.29 | 0.47 | 1.28 | 0.13 | 0 | -0.27 | 0.58 | 7 | 1.16 | 0.33 | 0.93 | 5.6 | 6.1 | 99 | 4.8 | 8 4 |
| 40- | MBH 69 | 0.21 | 0.22 | 0.13 | 0.04 | 0.17 | 60.0 | 0.22 | 0.29 | -0.01 | 1.2 | 0.92 | 0.85 | 2.33 | 0.36 | 3.03 | 1.64 | 0.85 | 0.45 | 10.0 | 10.0 | 70.0- | 0.02 | -0.01 | 0.03 | 0.02 | -0.03 | -0.04 | 3.16 | 0.01 | -0.01 | 0.04 | 0.03 | 0.01 | 0.18 | 0.18 | 0.01 | -0.04 | 0.43 | 0.26 | 0.08 | 0.22 | 2.59 | 2.02 | 20.9 | 2.03 | 3 14 |
| ck | MBH 66 | 1470 | 960 | 780 | 621 | 800 | 1330 | 1060 | 1200 | 800 | 1220 | 980 | 300 | 2100 | 260 | 4490 | 1670 | 1330 | 208 | 320 | 8/ | 5 | 18 | 4 | 129 | 84 | 84 | 16.2 | 9400 | 45 | 39.3 | 57 | 12 | 6 | 13 | 58 | 17 | 34 | 330 | 301 | 49 | 231 | 1860 | 2360 | 14700 | 1500 | 2230 |
| | MASSI | 59 | 39 | 14.2 | 13.8 | 19 | 4/1 | 24 | 99 | 21.2 | 43 | 25.3 | 4.6 | 87 | 7.4 | 91 | 59 | 26 | 71 | 7.0 | 1.1 | 0.1 | 8.2 | 6.5 | 7.8 | 7.22 | 8.4 | 2.22 | 910 | 7.6 | 10.1 | 9.3 | 6.88 | 2.71 | 6.3 | 11.9 | 26 | 8.1 | 38 | 89 | 10.5 | 33 | 1420 | 1380 | 2480 | 006 | 1700 |
| -13 | MBH 69 | -23.1 | -14.7 | -10.6 | -8.6 | -11.8 | -8.9 | -10.4 | -9.6 | -5.3 | 2.36 | 1.49 | 0.91 | 4.2 | 0.39 | 2.85 | 2 | 1.31 | 6/.0 | 1.21 | /1.0 | 71.0 | 0.40 | 0.09 | 0.42 | 0.19 | 0.28 | 0.22 | 5.33 | 0.19 | 0.33 | 0.33 | 0.31 | 0.11 | 0.1 | -0.05 | 0.2 | 0.05 | 0.41 | 0.59 | 0.11 | 9.0 | 1.26 | 1.9 | 23.4 | 1.59 | 1 73 |
| 24- | VIBH 69 | 79.3 | 103 | 119 | 135 | 113 | 1001 | 141 | 161 | 157 | 235 | 212 | 224 | 259 | 227 | 276 | 257 | 235 | 877 | 117 | 6/1 | 117 | 188 | 165 | 181 | 197 | 204 | 171 | 324 | 182 | 173 | 197 | 170 | 171 | 171 | 180 | 157 | 172 | 224 | 303 | 275 | 280 | 518 | 432 | 1340 | 517 | 460 |
| 31- | BH 69 1 | 130000 | 115000 | 90500 | 105000 | 110000 | 194200 | 105000 | 87000 | 52000 | 420 | 146 | 182 | 570 | 93 | 256 | 306 | 266 | 140 | 198 | 0000 | 0070 | 5860 | 3660 | 6290 | 3530 | 4800 | 2330 | 32700 | 5440 | 4200 | 4630 | 3360 | 2020 | 3920 | 5670 | 3890 | 7400 | 1250 | 4140 | 720 | 2210 | 13980 | 19100 | 19400 | 11300 | 10800 |
| - w ymnaddy | M | 8590 - 1 | 8590 - 2 | 8590 - 3 | 8590 - 4 | 8590 - 5 | 0 - 0608 | 8290 - 8 | 8590 - 9 | 8590 - 10 | 002 - 1 | 002-2 | 002 - 3 | 002 - 4 | 002 - 5 | 002 - 6 | 002 - 7 | 002 - 8 | 6-200 | 002 - 10 | 1 - 5105 | 7- 5102 | 2015-4 | 2015-5 | 2015 - 6 | 2015 - 7 | 2015 - 8 | 2015 - 9 | 2015 - 10 | 2158 - 1 | 2158 - 2 | 2158 - 3 | 2158 - 4 | 2158 - 6 | 2158 - 7 | 2158 - 8 | 2158 - 9 | 2158 - 10 | 064 - 1 | 064 - 2 | 064-3 | 064 - 4 | 064 - 5 | 064 - 6 | 064 - 7 | 064 - 8 | 0-4-0 |

| - | MBH 66 | -0.01 | 0 | 0.01 | 0 | 0.01 | 0 | 0 | 0 | 0 | 0 | 0.71 | 0.24 | 0.03 | 0.07 | 0.53 | 0.25 | 0.46 | 0.39 | 0.05 | 0.01 | 0.26 | 0.24 | 0.58 | 0.16 | 0.13 | 0.09 | 0.68 | 0.05 | 0.09 | 0.2 | 1.38 | 3.52 | 3.21 | 1.36 | 0.98 | 0.52 | | 0.4 | | 0.98 | 1.7 | 0.98 1.7 0.87 | 0.98 1.7 0.87 2 | 0.98 1.7 0.87 2 1.43 | 0.98 1.7 0.87 2 1.43 0.82 | 0.98 1.7 0.87 2 1.43 0.82 0.82 | 0.98 1.7 0.87 2 1.43 0.82 0.82 0.86 | 0.98 1.7 0.87 0.87 0.87 0.87 0.86 0.86 0.86 |
|---|-----------|---------|-------|-------|-------|-------|-------|-------|-------|-------|----------|---------|---------|---------|---------|---------|---------|-------|---------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|----------|----------|----------|----------|----------|----------|----------|--------|----------|-----------|---------|---------------------|--------------------------|----------------------------------|------------------------------------------|--------------------------------------------------|----------------------------------------------------------|---------------------------------------------------------------------|
| | ABH 66 | 0.05 | 0.08 | 0.07 | 60.0 | 0.09 | 0.08 | 0.58 | 0.11 | 0.08 | 0.06 | 36 | 8.2 | 0.78 | 0.66 | 23.4 | 3.45 | 23.4 | 8.9 | 1.01 | 0.52 | 6.6 | 80 | 7.5 | 11.3 | 5.2 | 4.7 | 3.09 | 2.62 | 4.5 | 5 | 90 | 36 | 67 | 49 | 20.7 | 26.2 | 6 | 8.4 | 39 | 19.3 | | 37 | 37 96 | 37 96 44.3 | 37 96 34 3 | 37 96 44.3 34 62.4 | 37 96 44.3 34 62.4 | 37 96 44.3 34 62.4 45.4 |
| | MASSI | 6.6 | 8.04 | 6.92 | 11 | 7.31 | 7.16 | 7.06 | 8.9 | 8.35 | 9.32 | 2.44 | 1.53 | 0.63 | 0.49 | 2.4 | 1.76 | 2.87 | 2.25 | 0.66 | 0.34 | 0.34 | 0.48 | 0.17 | 0.42 | 0.75 | 0.3 | 0.17 | 0.21 | 0.38 | 0.55 | 0.78 | 1.14 | 2.11 | 0.47 | 0.43 | 0.62 | 0.47 | 0.4 | 1.15 | 0.66 | | 140 | 140 283 | 140 283 116 | 140 283 116 120 | 140 283 116 120 | 140 283 116 120 139 | 140 283 116 120 139 8 8 8 |
| | MBH 66 | 0 | 0.01 | 0.01 | 0 | 0 | 0 | 10.0 | 0 | 0 | 0 | 0.52 | 0.2 | 0.04 | 0.02 | 0.37 | 0.21 | 0.63 | 0.47 | 0.03 | 0.02 | 0.03 | 0.14 | 0.02 | 0.01 | 0.02 | 0.02 | 0.08 | 0.02 | 0.01 | 0.11 | 0.18 | 0.02 | 0.16 | 60.0 | 0.11 | 0.17 | 0.02 | 10.0 | 0.04 | 0 | 0.05 | | 0.02 | 0.02 0.02 | 0.02 0.02 0.04 | 0.02 0.02 0.04 0.03 | 0.02 0.04 0.03 0.03 | 0.02 0.04 0.03 0.03 0.01 |
| | MBH 69 | 0.02 | -0.05 | 0.04 | -0.04 | -0.02 | -0.03 | 0.31 | 0.21 | 0.17 | 0.07 | 0.18 | -0.1 | -0.1 | -0.08 | -0.09 | -0.2 | -0.45 | -0.14 | -0.06 | -0.05 | 0.44 | 2.1 | 0.4 | 0.11 | 0.0 | -0.02 | 1.8 | 0.18 | 0.07 | 0.19 | 0.22 | 0.52 | 3.5 | 0.71 | 0.53 | 0.37 | 0.58 | cc.0 | 0.46 | -0.01 | 0.82 | | 2.5 | 2.5 | 2.5 0.8 0.68 | 2.5 0.8 0.68 1.1 | 2.5 0.8 0.68 0.18 | 2.5 0.8 0.18 0.18 0.18 |
| | MBH 69 | -0.01 | 0.03 | 0.1 | 0.03 | -0.02 | 0 | -0.01 | -0.03 | 0.02 | 0.01 | 1.04 | 0.23 | 0.07 | 0.06 | L.T | 0.26 | 0.75 | 0.63 | 0.05 | 0 | 1.02 | 3.8 | 0.3 | 0.62 | 0.21 | 0.16 | 0.15 | 0.1 | 0.12 | 0.27 | 2.2 | 0.4 | 3.7 | 1.09 | 0.61 | 0.28 | 0.68 | 0.00 | | 0.1 | 1.37 | 0 | 6.1 | 1.05 | 1.05 0.87 | 1.05 0.87 1 | 1.05 0.87 1.32 1.32 | 1.05 1.05 0.87 1.32 0.84 |
| | MBH 72 | 0.33 | 1.52 | 1.09 | 1.52 | 1.05 | 1.47 | 1.6 | 0.39 | 0.33 | 0.24 | 430 | 33 | 6.05 | 2.76 | 56 | 20.7 | 260 | 51 | 5.23 | 2.7 | 5.2 | 1.03 | 2.9 | 2.52 | 1.21 | 0.81 | 0.51 | 1.32 | 0.71 | 0.4 | 11.4 | 4.4 | 9.2 | 6.2 | 2.4 | 1.81 | 3.7 | 0.99 | 8.9 | 5 | 1.82 | 66 | 0.0 | 4.2 | 4.2 5.7 | 5.7 6 | 5.7 5.7 5.7 | 5.7 5.7 5.5 5.5 |
| | 09 HBM | 0.01 | 0 | 0 | 0 | 0.01 | 0 | 0.02 | 0 | 0 | 0 | 0.42 | 0.04 | 0.01 | 0 | 0.09 | 0.03 | 0.3 | 0.07 | 0.01 | 0 | 0.06 | 3.2 | 0.15 | 0.08 | 0.04 | 0.01 | 0.08 | 0.01 | 0.01 | 0.06 | 1.7 | 0.58 | 3 | 1.6 | 0.42 | 0.05 | 0.34 | 0.02 | 3.5 | 0.29 | 0.04 | 0.23 | | 0.14 | 0.14 0.13 | 0.14 0.13 0.13 | 0.14 0.13 0.13 0.18 | 0.14 0.13 0.13 0.13 0.17 |
| | MBH 69 | -0.02 | -0.02 | -0.03 | 0.01 | 0.01 | 0.02 | 0.07 | 0.02 | -0.07 | 0.04 | 0.31 | 0.29 | 0.07 | 60'0 | 0.11 | 0.19 | 0.24 | 0.27 | 60.0 | 0.02 | 3.4 | 13.2 | 5.81 | 11.4 | 28.9 | 16.7 | 9.25 | 12.3 | 13.1 | 4.2 | 3.2 | 0.48 | 1.5 | 0.66 | 0.59 | 0.28 | 1.2 | 0.21 | 0.36 | 0.37 | 6.2 | 11.5 | | 4.5 | 4.5 4.52 | 4.5 4.52 5.43 | 4.5 4.52 5.43 5.6 | 4.5 4.52 5.43 5.6 4.45 |
| | MBH 69 | 22.1 | 31.8 | 41.7 | 25.3 | 36.9 | 26.6 | 24.6 | 20.2 | 61.9 | 52.1 | 101 | 108 | 32.8 | 32.7 | 87.5 | 78 | 81 | 149 | 25.9 | 210 | 50.6 | 52.3 | 35.4 | 31.2 | 31.3 | 30.6 | 33.7 | 18.6 | 18.6 | 46.5 | 148 | 36.4 | 60 | 89.1 | 132 | 139 | 106 | 0.00 | 112 | 108 | 480 | 560 | | 313 | 313 317 | 313 317 218 | 313 317 218 530 | 313 317 218 530 216 |
| | MASSI | -0.03 | 0.1 | 0.0 | 0.03 | -0.01 | 0.07 | 0.15 | 0.05 | -0.01 | 0.07 | 0.39 | 0.23 | 0.04 | -0.04 | 2.8 | -0.15 | 0.76 | 0.86 | 0.11 | 0.06 | 0.67 | 1.3 | 0.42 | 0.48 | 0.25 | 0.28 | 0.37 | 0.24 | 0.27 | 0.24 | 1.05 | 0.44 | 1.54 | 0.65 | 0.79 | 0.69 | 0.35 | 0.16 | 1.7 | 0.32 | 0.69 | 1 | | 0.29 | 0.29 0.44 | 0.29 0.44 -0.03 | 0.29 0.44 0.13 0.13 | 0.29 0.44 0.13 0.18 0.18 |
| | MBH 69 | 1.04 | 1.18 | 1.07 | 1.19 | 0.66 | 0.84 | 0.94 | 1.53 | 1.78 | 1.46 | 14.9 | 6.9 | 0.8 | 0.82 | 16.4 | 2.58 | 8.5 | 8.6 | 0.88 | 0.61 | 15.8 | 18.2 | 6 | 13.3 | 9.1 | 4.8 | 8.4 | 5.2 | 8.7 | 16.6 | 25.5 | 11.3 | 37 | 14.2 | 7.4 | 7.6 | 6.9 | 90.5 | 15.7 | 8.8 | 48.8 | 65 | | 39.6 | 39.6 34.9 | 39.6 34.9 30.5 | 39.6 34.9 30.5 46.1 | 39.6 34.9 30.5 30.5 30.2 |
| | MBH 66 | 0.46 | -0.19 | 0.12 | 0.37 | -0.45 | 0.25 | 0.13 | 0.19 | 0.21 | -0.05 | -0.5 | 1.3 | 0.29 | 0.21 | 11 | 0.32 | 0.8 | -0.8 | 0.11 | 0.04 | 1.7 | 5.7 | 0.38 | 1.37 | 2.8 | 0.26 | 0.7 | 0.09 | 0.9 | 9.0 | 7 | 3.4 | 8.9 | 2.28 | 1.38 | 12 | 1.43 | 0.48 | 3.7 | 2.4 | 1.76 | 11.1 | | 2.71 | 2.71 5.1 | 2.71 5.1 6.1 | 2.71 5.1 6.1 8.5 | 2.71 5.1 6.1 8.5 5.6 |
| ; | MASSI 1 | 0.04 | -0.02 | 0.11 | 0.02 | 0.16 | 0.21 | 0 | 0.02 | 0.03 | 0.06 | 0.76 | 4.3 | 0.25 | 0.15 | 3.92 | 0.61 | 3.4 | 2.72 | 0.71 | 0.33 | 4.46 | 2.91 | 2.03 | 6.4 | 4 | 2.01 | 2.06 | 1.96 | 3.29 | 3.38 | 27 | 11.7 | 35.3 | 11.7 | 2.6 | 2.2 | 6.5 | 52 | 16 | 13.1 | 8.8 | 65 | | 16 | 16 30.7 | 16 30.7 36.1 | 16 30.7 36.1 41.2 | 16 30.7 36.1 41.2 38.2 |
| | nZ° | 0.8 | 62.0 | 161 | 117 | .78 | .74 | | .45 | 22 | .72 | 230 | 184 | 8.3 | 6.8 | 311 | 149 | 200 | 100 | 5.5 | 13.8 | 816 | 732 | 180 | 160 | 565 | 327 | 342 | 345 | 009 | 910 | 190 | 129 | 990 | 6/1 | 130 | 81 | 106 | 41 | 218 | 121 | 330 | 020 | | 865 | 598 330 | 598 330 130 | 598 330 130 | 598 330 130 180 |
| | . WE | | J | | | | | | | | ~ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| * | 9 MBH (| 0.06 | 0.87 | 0.18 | 0.72 | 0.34 | 0.11 | 0.24 | 1.4 | -0.1 | -0.4 | 4 | 3.1 | 0.29 | 0.36 | 14.1 | 2.1 | 6.3 | 2 | 0.92 | 0.43 | 6.9 | 8.9 | 7.83 | 13.7 | 19.5 | 11.8 | 9.4 | 12.2 | 9.2 | 4.41 | 21 | 6.9 | 26 | 7.1 | 4.4 | 3.4 | 3.6 | 1.40 | 9.2 | 4.3 | 5.8 | 135 | | 28 | 28 | 28 101 87 | 28 101 87 165 | 28 101 165 89 |
| 1 | MBH (| -0.15 | 0.04 | 0.18 | 0.06 | -0.0 | -0.1 | 0.07 | 0.08 | 0.02 | -0.07 | 1.21 | 0.76 | -0.01 | 0.04 | 5.5 | 0.22 | 0.79 | 0.58 | 0.07 | 0.05 | 1.41 | 2.5 | 1.03 | 2.44 | 2.37 | 1.9 | 1.23 | 2.03 | 0.93 | 0.88 | 7.4 | 1.71 | 5.6 | 2.35 | 1.6 | 1.6 | 1.35 | 4.0 | 3.29 | 2.1 | 2.14 | 54 | | 6 | 32.4 | 9 32.4 26.4 | 9 32.4 26.4 59 | 9 32.4 59 35.2 |
| | MBH 66 | 5.10 | 3.36 | 5.30 | 5.70 | 4.1 | 6.2 | 4.7 | 8.4 | 7.3 | 2 | 2850 | 5600 | 220 | 220 | 13100 | 663 | 5200 | 3100 | 290 | 123 | 4300 | 3300 | 1670 | 5100 | 2240 | 970 | 618 | 730 | 1210 | 1000 | 8600 | 3060 | 10700 | 3950 | 1760 | 1590 | 1810 | 130 | 3380 | 2700 | 2160 | 25900 | | 6150 | 6150 21100 | 6150 21100 22200 | 6150 21100 22200 45900 | 6150 21100 22200 45900 34200 |
| | MASSI | 1.04 | 0.58 | 0.56 | -0.23 | 1.13 | 0.25 | 0.0 | 0.72 | 0.68 | 0.89 | 330 | 76 | 11.5 | 3.26 | 235 | 45.7 | 480 | 99 | 11.8 | 2.49 | 1270 | 1250 | 1020 | 3180 | 2850 | 1680 | 1030 | 1510 | 1400 | 780 | 860 | 303 | 1230 | 360 | 204 | 154 | 155 | 2 | 367 | 218 | 1080 | 3800 | | 860 | 860 1490 | 860 1490 2300 | 860 1490 3850 3850 | 860 1490 3850 1830 |
| | MBH 69 | 0.03 | 0.17 | -0.05 | 0.03 | 0.11 | 0.15 | 0.15 | -0.02 | -0.04 | 0.11 | 1.16 | 2.55 | 0.28 | 0.2 | 4.2 | 1.46 | 2.2 | 2.9 | 0.57 | 0.19 | 35.6 | 43.2 | 30.2 | 46.8 | 55.4 | 74.4 | 50.8 | 16 | 142 | 107 | -289 | -85 | -204 | -79 | -33.8 | -38 | -30 | -14.9 | -70 | -35.2 | -52 | -303 | | -101 | -101 | -101 -271 -238 | -101 -271 -238 -387 | -101 -271 -238 -343 -343 |
| | Ste | 213 | 181 | 184 | 188 | 181 | 169 | 159 | 159 | 160 | 160 | 323 | 447 | 172 | 150 | 517 | 304 | 531 | 401 | 164 | 153 | 114 | 217 | 240 | 323 | 308 | 326 | 243 | 349 | 315 | 180 | 145 | 183 | 275 | 156 | 193 | 162 | 145 | 1/0 | 208 | 189 | 450 | 4100 | | 667 | 1110 | 667 1110 3380 | 667 1110 1030 | 667 3380 1030 1590 |
| | 41 69 HBM | 750 | 610 | 590 | 570 | 418 | 480 | 357 | 537 | 610 | 470 | 1990 | 4470 | 545 | 617 | 8300 | 950 | 6100 | 5700 | 006 | 854 | 90200 | 88000 | 62300 | 45800 | 58100 | 38400 | 54400 | 41800 | 71300 | 154000 | 126000 | 49000 | 86000 | 50600 | 38400 | 40900 | 49500 | 20500 | 70100 | 58500 | 343000 | 530000 | | 212000 | 212000 212000 | 212000 212000 270000 | 212000 212000 270000 325000 | 212000 212000 325000 148000 |
| | | 851 - 1 | 851-2 | 851-3 | 851-4 | 851-5 | 851-6 | 851-7 | 851-8 | 851-9 | 851 - 10 | 822 - 1 | 822 - 2 | 822 - 3 | 822 - 4 | 822 - 5 | 822 - 6 | 822-7 | 822 - 8 | 822 - 9 | 822 - 10 | 8582 - 1 | 8582 - 2 | 8582 - 3 | 8582 - 4 | 8582 - 5 | 8582 - 6 | 8582 - 7 | 8582 - 8 | 8582 - 9 | 8582 - 10 | 8594 - 1 | 8594 - 2 | 8594 - 3 | 8594 - 4 | 8594 - 5 | 8594 - 6 | 8594 - 7 | 8- 468 | 8594 - 9 | 8594 - 10 | 173 - 1 | 173 - 2 | | c - c/1 | 173 - 4 | 173 - 5 173 - 4 173 - 5 | 1/3 - 5 173 - 5 173 - 5 173 - 6 | 1/3 - 5 173 - 4 173 - 5 173 - 6 173 - 7 |

| ²⁰⁹ Bi | MBH 00 | 3 | 0.79 | 0.24 | 0.12 | 0.29 | 0.19 | 0.11 | 0.13 | 0.15 | -0.02 | 0.15 | 1.33 | 0.05 | 0 | 0.02 | 0 | 0.01 | 0.43 | 291 | 33.5 | 19.3 | 24.8 | 72.5 | 17.4 | 19.8 | 26.7 | 27.3 | 63.9 | 4 | 40.9 | 52.2 | 69.8 | 75.7 | 94.4 | 57.3 | | 59.8 | 59.8 128 | 59.8 128 0.17 | 59.8 128 0.17 0.05 | 59.8 128 0.17 0.05 0.02 | 59.8 128 0.17 0.05 0.02 0.01 | 59.8 128 0.17 0.05 0.02 0.01 | 59.8 128 0.17 0.05 0.02 0.01 0.53 | 59.8 128 0.17 0.05 0.01 0.01 0.01 0.01 | 59.8 128 0.17 0.05 0.01 0.01 0.01 0.00 |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------|-------------|-------|---------|---------|---------|---------|---------|-------|----------|---------|-------|-------|-------|-------|-------|-------|---------|-------|----------|---------|---------|---------|---------|---------|--------|---------|---------|-------|-------|--------|---------|---------|-------|--------|-------|-------|----------|-------------|---------------------|-----------------------------|-------------------------------------|---------------------------------------------|---------------------------------------------|-------------------------------------------------------|-------------------------------------------------------------|-------------------------------------------------------------|
| ²⁰⁸ Pb | 00 HBH 00 | 3.66 | 4.80 | 15.6 | 4.08 | 10.7 | 4.9 | 4.9 | 3.59 | 6.6 | 0.4 | 2.85 | 0.52 | 2 | 1.65 | 0.65 | 0.25 | 1.23 | 0.48 | 2310 | 24200 | 21200 | 26900 | 10200 | 6190 | 7000 | 8400 | 18000 | 37000 | 27800 | 41100 | 23200 | 34700 | 23100 | 67200 | 39800 | 25400 | 00000 | 91000 | 91000 | 91000 4.96 1.52 | 91000 4.96 1.52 0.79 | 91000 4.96 1.52 0.79 0.28 | 91000 4.96 1.52 0.79 3.52 | 91000 4.96 1.52 0.79 3.52 3.52 0.77 | 91000 4.96 1.52 0.79 0.28 3.52 0.77 | 91000 4.96 0.79 0.28 3.52 0.44 0.44 |
| 202Hg | ICCEM | 6.14 5.9 | 7.6 | 5.13 | 6.5 | 6.5 | 6.16 | 8.3 | 6.3 | 5.73 | 4.44 | 1.83 | 2.56 | 2.11 | 11.1 | 10.2 | 5.12 | 1.57 | 2.54 | 5500 | 4.76 | 5.33 | 4.71 | 2.14 | 2.28 | 2.17 | 2.8 | 14.5 | 1.35 | 0.67 | 1.23 | 0.57 | 1.52 | 1.24 | 2.05 | 1.32 | 0.86 | 2.12 | | 154 | 154 | 154 72 41.4 | 154 72 41.4 47.5 | 154 72 41.4 47.5 175 | 154 72 41.4 47.5 175 60 | 154 72 41.4 47.5 175 60 59.1 | 154 72 41.4 47.5 175 60 59.1 63.7 |
| 197 Au | 00 LIGIN | 0.02 | 0.05 | 0.11 | 0.04 | 0.11 | 0.03 | 0.04 | 0.01 | 0.02 | -0.01 | 0 | 0 | 0.01 | -0.01 | 0.03 | 0.01 | 0.01 | 0.01 | 4 | 21.6 | 12.85 | 11.66 | 16.3 | 19.5 | 21.8 | 21.8 | 20 | 58 | 26 | 38 | 16 | 43.5 | 32.5 | 54 | 27.7 | 37 | 61 | 0.03 | | 0.02 | 0.02 | 0.02 0.01 0 | 0.02 0.01 0.06 | 0.02 0.01 0.06 0.02 | 0.02 0.01 0.06 0.02 0.02 | 0.02 0.01 0.06 0.02 0.02 0.02 |
| ¹²⁵ Te | VIBIN 09 | 0.14 | 0.79 | 0.25 | 0.8 | 0.87 | 0.7 | 0.61 | 0.23 | -0.02 | -0.8 | 0.01 | 0 | 0.27 | 1.2 | 0.3 | 1 | 0.15 | -0.08 | 510 | 1.36 | 0.29 | 0.57 | 1.47 | 0.73 | 0.95 | 0.59 | 1.71 | 0.48 | 0.11 | 0.03 | 0.15 | 0.27 | 0.08 | 0.25 | -0.16 | -0.03 | 0.07 | 0.05 | 000 | 0.03 | -0.01 | -0.01 0.07 | 0.01 -0.01 0.06 | 0.03 -0.01 0.06 -0.03 | 0.03 0.07 0.06 0.03 -0.03 | 0.03 0.07 0.06 0.05 0.03 0.06 |
| 121Sb | 0 UBH 09 | 0.13 | 1.0 | 1.4 | 0.16 | 0.89 | 0.1 | 0.18 | 0.31 | 0.15 | -0.11 | 0.09 | 0.04 | 0.07 | 0.1 | 0.21 | -0.19 | 0.03 | 0.05 | 240 | 280 | 199 | 217 | 161 | 134 | 149 | 232 | 238 | 176 | 105 | 200 | 150 | 232 | 206 | 301 | 171 | 143 | 306 | 0.11 | 0.04 | 5.5 | 0 | 0.01 | 0 0.01 0.01 | 0 0.01 0.01 0.01 | 0.01 0.01 -0.01 -0.02 | 0 0.01 -0.01 -0.02 0.07 |
| 118Sn | 7/ U9W | 0.57 | 0.5 | 1.06 | 0.86 | 1.8 | 0.42 | 0.82 | 0.66 | 0.56 | 0.74 | 0.29 | 0.13 | 0.41 | 1.1 | 1.88 | 0.96 | 0.25 | 0.11 | 264 | 1180 | 525 | 551 | 758 | 721 | 844 | 910 | 920 | 71400 | 38200 | 128000 | 66600 | 78200 | 81600 | 107200 | 71000 | 55800 | 242000 | 3.6 | 0 97 | | 0.67 | 0.67 | 0.67 0.54 1.83 | 0.67 0.54 1.83 0.47 | 0.67 0.54 1.83 0.47 0.24 | 0.67 0.54 1.83 0.47 0.24 0.4 |
| 115In | 40 LI DA | 0.12 | 0.4 | 0.32 | 0.15 | 0.14 | 0.57 | 0.31 | 0.05 | 0.01 | -0.01 | 0 | 0.01 | 0.02 | 0.02 | 0 | -0.01 | 0 | 0 | 5 | 22.8 | 12.6 | 11.4 | 18.2 | 15.6 | 19.5 | 18.3 | 21.9 | 298 | 137.5 | 442 | 214 | 286 | 293 | 442 | 246 | 193.4 | 790 | 0.02 | 0.01 | 10.0 | 0.01 | 0.01 | 0.01 0.01 | 0.01 0.01 0 | 10:0 0.01 0 0 | 0.01 0 0 0 0 0 0 |
| III Cd | 40 HBM | 0.73 | 0.52 | 0.83 | 0.56 | 1.9 | 0.64 | 1.06 | 0.66 | 0.74 | 0.06 | 0.58 | 0.02 | 0.19 | 0.21 | 0.02 | 0.06 | 0.19 | 0.11 | 170 | 0.78 | 2.27 | 2.14 | 1.49 | 0.61 | 0.94 | 1.05 | 2.05 | 7.65 | 0.87 | 10.6 | 0.84 | 1.85 | 4.31 | 10 | 2.64 | 5 | 28.5 | 0.34 | 0.25 | | 0.21 | 0.21 0.27 | 0.21 0.27 0.19 | 0.21 0.27 0.19 0.13 | 0.21 0.27 0.19 0.13 0.17 | 0.21 0.27 0.19 0.13 0.17 0.17 |
| 107 Ag | 40 LIGIN | 6.8 | 6.8 | 10.6 | 8.3 | 6.6 | 8.7 | 9.6 | 5.85 | 6.27 | 11.42 | 18.5 | 184 | 216 | 143 | 229 | 200 | 219 | 329 | 2950 | 560 | 499 | 530 | 608 | 675 | 622 | 678 | 860 | 1090 | 294 | 610 | 405 | 743 | 580 | 1400 | 710 | 430 | 1080 | 101 | 138 | | 128 | 128 159 | 128 159 89.3 | 128 159 89.3 125 | 128 159 89.3 125 131 | 128 159 89.3 125 131 160 |
| oW ₅₆ | ICCEM | 3.12 | 2.75 | 5.2 | 2.58 | 1.99 | 1.89 | 2.73 | 2.90 | 3.58 | 0.68 | 0.57 | 0.32 | 0.11 | -0.08 | -0.03 | -0.21 | 0.69 | 0.26 | 190 | 0.70 | 0.67 | 0.64 | 0.21 | 0.39 | -0.21 | 0.22 | 0.76 | 0.88 | 0.97 | 0.98 | 69.0 | 0.74 | 0.91 | 0.85 | 0.9 | 0.98 | 1.41 | 0.31 | 0.23 | | 0.19 | 0.19 0.08 | 0.19 0.08 0.17 | 0.19 0.08 0.17 0 | 0.19 0.08 0.17 0.19 | 0.19 0.08 0.17 0 0.19 0.19 |
| 75As | 60 LIGIN | 52.7 | 45.6 | 39.5 | 42.7 | 29.4 | 42.7 | 39.1 | 71.2 | 90.6 | -0.14 | 11.7 | 4.62 | 3.55 | 0.85 | 0.86 | 0.37 | 5.11 | 2.14 | 3440 | 853 | 536 | 671 | 348 | 248 | 266 | 436 | 740 | 477 | 320 | 470 | 355 | 572 | 532 | 1050 | 629 | 465 | 1020 | 31.4 | 12.6 | | L | 5.9 | 5.9 6.8 | 7 5.9 6.8 7.1 | 7 5.9 6.8 7.1 4.75 | 7 5.9 6.8 7.1 4.75 3.63 |
| ⁷² Ge | 00 LISIN | 0.67 | 1.11 | 2.3 | 1.6 | 0.61 | 1.07 | 1.25 | 1.33 | 0.83 | 0.8 | 0.39 | 0.35 | 0.01 | 2.3 | 0 | 1 | 0.16 | -0.01 | 310 | 1.94 | 1.38 | 1.62 | -0.18 | 0.42 | 1.39 | 0.68 | 1.6 | 5.9 | 3.99 | 3.15 | 4.83 | 7 | 5.4 | 6.8 | 4.3 | 3.68 | 9.5 | 0.02 | -0.06 | | +0.0- | 0.03 | 0.03 | -0.34 0.03 0.41 | -0.34 0.03 0.41 0 | 0.03 0.03 0.41 0 0 |
| 71Ga | ICCEM | 1.41 | 2.15 | 1.45 | 3.13 | 1.76 | 2.5 | 1.43 | 1.58 | 1.48 | -0.62 | 0.17 | 0.18 | 0.12 | 5.44 | 0.1 | -0.16 | 0.15 | 0.03 | 410 | 4.74 | 3.54 | 3.31 | 1.58 | 1.17 | 1.24 | 1.76 | 6.9 | 6.19 | 3.5 | 4.46 | 3.74 | 5.81 | 6.51 | 14 | 4.69 | 3.22 | 7.54 | 0.93 | 0.37 | | 7.0 | 0.52 | 0.52 | 0.22 0.52 0.32 | 0.52 0.52 0.32 -0.04 | 0.2 0.52 0.23 0.32 0.16 |
| uZ ⁵⁶ Zn | KO LIGW | 24 | 20 | 129 | 28.1 | 100 | 63 | 18 | 16 | 20.8 | 3.4 | 14.7 | 7.14 | 12.8 | 105 | 9.2 | 2.7 | 7.9 | 4.6 | 1900 | 256000 | 594000 | 543000 | 322000 | 139000 | 286600 | 179900 | 524000 | 32600 | 23350 | 44200 | 19400 | 35320 | 30500 | 36800 | 25620 | 27720 | 57700 | 45.0 | 21.6 | | 10 | 6.8 | 6.8 6.8 26.2 | 18 6.8 9.2 | 18 6.8 9.2 8.2 | 18 6.8 9.2 8.2 6 |
| Nobility in the second | 60 LIGIM | 1.43 | 2.8 | 3.57 | 6.9 | 4 | 3.16 | 1.47 | 2.2 | 1.35 | 5.8 | 0.23 | 0.63 | 0.65 | 15.5 | -0.5 | -5.2 | 0.34 | -0.62 | 9300 | 214 | 320 | 307 | 156 | 65.2 | 135 | 88 | 277 | 71.7 | 115 | 213 | 70.5 | 117 | 70.3 | 88 | 70.8 | 101 | 126 | 1.16 | 0.47 | 1.05 | 1.00 | 0.1 | 0 1.42 | 0.0 1.42 -0.3 | 1.00 0 -0.3 -0.3 | 0.1.00 0.1.42 -0.3 0.11 |
| 59Co | WIBH 0A | 69.0 | 1.1 | 2.5 | 2.32 | 5 | 1.4 | 1.9 | 0.66 | 0.73 | -0.08 | 0.05 | 0.38 | 0.07 | 5.83 | -0.13 | 0.21 | 0.06 | 0.11 | 1340 | 13.2 | 27.7 | 24.6 | 14.3 | 5.32 | 12.2 | 6 | 21 | 21.3 | 13.3 | 14.6 | 12.8 | 1.9.1 | 29.2 | 30 | 21 | 19 | 63.1 | 0.7 | 0.11 | 0.16 | 01.0 | 0.15 | 0.15 | 0.15 0.07 0.07 | 0.15 0.07 0.07 -0.02 | 0.15 0.07 0.07 0.02 0.02 |
| ^{sé} Fe | 00 LIGIN | 3840 | 5900 | 6100 | 11200 | 5400 | 8000 | 2950 | 3840 | 3860 | 2.1 | 58 | 372 | 41 | 8190 | 4.5 | 2 | 11.7 | 90 | 366000 | 31800 | 22300 | 30200 | 6060 | 1720 | 2080 | 4080 | 28700 | 6020 | 3670 | 7000 | 5740 | 7150 | 7840 | 26900 | 10400 | 6970 | 30300 | 1080 | 600.0 | 767 | 707 | 108 | 108 | 202 320 360 | 202 108 320 330 | 202 320 360 330 192 |
| uM ²⁵ | ICCHM | 36.1 | 91 | 121 | 252 | 270 | 302 | 76 | 58 | 52 | 1.9 | 11.7 | 12.5 | 17.2 | 746 | -0.4 | -0.8 | 4.17 | 2.24 | 9200 | 289 | 130 | 226 | 78 | 28.2 | 78 | 58 | 272 | 1280 | 870 | 2260 | 1430 | 2000 | 1880 | 4600 | 2020 | 1580 | 3900 | 31.1 | 30.0 | 080 | 207 | 3.9 | 3.9 | 3.9 16.9 14.9 | 3.9 16.9 14.9 10.4 | 3.9 16.9 14.9 9.5 |
| 53Cr | KO LIGIN | 102 | 75 | 81 | 60.1 | 23 | 30.5 | 23 | 27 | 23.7 | 0.3 | 0.97 | 1.17 | 0.63 | 4.8 | -0.2 | -0.4 | 0.32 | 0.18 | 440 | 1.94 | 1.14 | 2.4 | 0.87 | 0.33 | 0.63 | 0.23 | 3.04 | 2.02 | 2.07 | 1.97 | 1.71 | 2.37 | 2.4 | 7.3 | 3.3 | 2.4 | 3.1 | 3.43 | 1.0 | 1 35 | | 0.95 | 0.95 | 0.95 0.89 0.9 | 0.95 0.89 0.9 | 0.95 0.89 0.9 1.1 |
| S ⁴⁶ | KO LIGIN | 188 | 258 | 173 | 227 | 168 | 172 | 250 | 211 | 212 | 135 | 272 | 240 | 246 | 279 | 207 | 139 | 250 | 250 | 309000 | 245 | 300 | 302 | 182 | 184 | 182 | 177 | 334 | 363 | 267 | 413 | 277 | 308 | 340 | 536 | 378 | 292 | 579 | 181 | 193 | 174 | | 173 | 173 183 | 173 183 199 | 173 183 225 | 173 183 199 187 |
| ³¹ P | 40 LIGN | 6390 | 7700 | 6500 | 6850 | 5100 | 5260 | 7500 | 5710 | 5730 | 17 | 1370 | 1980 | 530 | 29 | 15 | 11 | 460 | 149 | 17300 | 5120 | 2350 | 3140 | 562 | 158 | 96 | 580 | 3120 | 38100 | 20290 | 52000 | 21200 | 33500 | 35000 | 65300 | 35500 | 29900 | 125000 | 52600 | 18800 | 0100 | DATC. | 5900 | 5900 8000 | 5900 8000 8100 | 5900 8000 5400 5400 | 5900 8000 8100 5400 5600 |
| | 1 000 | 230-2 | 230-3 | 230 - 4 | 230 - 5 | 230 - 6 | 230 - 7 | 230 - 8 | 230-9 | 230 - 10 | 021 - 1 | 021-2 | 021-3 | 021-4 | 021-5 | 021-6 | 021-7 | 021 - 8 | 021-9 | 021 - 10 | 19a - 1 | 19a - 2 | 19a - 3 | 19a - 4 | 19a - 5 | 19a-6 | 19a - 7 | 19a - 8 | 819-1 | 819-2 | 819-3 | 819 - 4 | 819 - 5 | 819-6 | 819-7 | 819-8 | 819-9 | 819 - 10 | 859 - 1 | 859 - 2 | 859 - 3 | | 859 - 4 | 859 - 4 859 - 5 | 859 - 4 859 - 5 859 - 6 | 859 - 4 859 - 5 859 - 6 859 - 7 | 859 - 4 859 - 5 859 - 6 859 - 7 859 - 8 |

| 312 | | | | | | | | | | | | | | | | | | | | | |
|---------|----------|------------------|-----------|---------------|------------------|------------------|------------------|--------|---------------|------------|------------------|-------------------|-----------|---------------|---------------|---------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 4 | 34S | ⁵³ Cr | 55Min | s6Fe | ⁵⁹ Co | iN ⁰⁰ | uZ ⁹⁹ | 71Ga | 72Ge | 75As | oW ₅₆ | ¹⁰⁷ Ag | III Cd | II5In | 118Sn | 121Sb | ¹²⁵ Te | ¹⁹⁷ Au | ²⁰² Hg | ²⁰⁸ Pb | ²⁰⁹ Bi |
| H 69 | MBH 69 | MBH 69 | MASSI | MBH 66 | MBH 69 | MBH 69 | MBH 69 | MASSI | MBH 66 | MBH 69 | MASSI | MBH 69 | MBH 69 | MBH 69 | MBH 72 | MBH 69 | MBH 69 | MBH 66 | MASSI | MBH 66 | MBH 66 |
| 000000 | 5400000 | 36000 | 240000 | 42000000 | 15000 | 146000 | 3600000000 | 890000 | 1030000 | 610000 | 4300 | 750000 | 101000000 | 1720000 | 1530000 | 5600000 | 3700 | 90 | 1310000 | 72000000 | 17400 |
| 00000 | 2400000 | 98000 | 340000 | 18000000 | 100000 | 16000 | 3100000000 | 200000 | 82000 | 340000 | 8200 | 830000 | 4300000 | 720000 | 1180000 | 290000 | 3000 | 20 | 3500000 | 54000000 | 13500 |
| 00000 | 680000 | -800 | 28000 | 2240000 | 200 | 6800 | 000000069 | 38000 | 3700 | 26000 | 1800 | 106000 | 13900000 | 102000 | 172000 | 58000 | 660 | 12 | 670000 | 147000000 | 3000 |
| 000000 | 4100000 | 00066 | 1060000 | 42000000 | 12000 | 87000 | 2600000000 | 330000 | 94000 | 330000 | 600 | 730000 | 4700000 | 730000 | 700000 | 280000 | 1300 | -67 | 1390000 | 59000000 | 14200 |
| 000000 | 5660000 | 101000 | 850000 | 3000000 | 4100 | 167000 | 2290000000 | 479000 | 171000 | 299000 | 9200 | 1120000 | 2860000 | 726000 | 1010000 | 602000 | 2300 | 90 | 1190000 | 80000000 | 22300 |
| 000000 | 6140000 | 108000 | 560000 | 4000000 | 11600 | 122000 | 2260000000 | 343000 | 146000 | 306000 | 3300 | 1150000 | 5990000 | 804000 | 1120000 | 741000 | 1000 | 57 | 1870000 | 86900000 | 18900 |
| 000000 | 6220000 | 45000 | 83000 | 4360000 | 3300 | 170000 | 2170000000 | 479000 | 200000 | 637000 | 5100 | 1110000 | 5580000 | 796000 | 814000 | 000668 | 3100 | 78 | 2640000 | 55700000 | 25900 |
| 000000 | 2500000 | 0000006 | 520000 | 10300000 | -19000 | 140000 | 240000000000 | 770000 | 510000 | 820000 | 300000 | 2200000 | 38000000 | 3700000 | 5200000 | 500000 | 55000 | -300 | 1800000 | 440000000 | 93000 |
| 400000 | 10700000 | 53000 | 50000 | 6220000 | 6700 | 118000 | 44400000000 | 547000 | 338000 | 00069 | -600 | 1150000 | 59400000 | 827000 | 800000 | 1150000 | 1400 | 06 | 2850000 | 129000000 | 29000 |
| 0000001 | 5800000 | 58000 | 124000 | 790000 | 4500 | 233000 | 2260000000 | 386000 | 157000 | 360000 | 2600 | 890000 | 17300000 | 610000 | 753000 | 600000 | 5400 | 56 | 1830000 | 49000000 | 19400 |
| 14800 | 141 | 73 | 16 | 690 | 155 | 7300 | 230 | 1 07 | 0.35 | 4130 | 0.36 | 12700 | 0.18 | 70 | 130 | 19500 | 3 40 | 010 | 1 36 | 18500 | 351 |
| 00001 | 120 | 17 | 14.0 | 007 | 197 | 00001 | 001 | 10.1 | 04.0 | OFIC | 100 | 00/71 | 01.0 | 51 7 | 001 | 15400 | 23.0 | 000 | 1.2 | 00001 | 100 |
| 00071 | 961 | 1.0 | 14.0 | 000 | 151 | 0++0 | 190 | 10.0 | 0.40 | 0407 | 17.0 | 0006 | 11.0 | 1.10 | 190 | 00401 | CC.7 | 006 | 1.0 | 00071 | 077 |
| 4720 | 159 | 9 | 5.2 | 240 | 59 | 2700 | 67 | 0.47 | 0.52 | 1400 | 0.14 | 5400 | 0.06 | 40.9 | 62 | 8800 | 1.09 | 312 | 0.61 | 8500 | 162 |
| 2910 | 155 | 4 | 8.7 | 360 | 80 | 2000 | 203 | 0.35 | 0.2 | 665 | 0.06 | 4120 | 0.08 | 112 | 4440 | 4190 | 0.88 | 217 | 0.46 | 5400 | 70.00 |
| 7300 | 141 | 6 | 12.4 | 492 | 91 | 2940 | 118 | 0.68 | 0.52 | 1930 | 0.25 | 6040 | 0.19 | 68 | 880 | 11200 | 2.01 | 641 | 0.96 | 10900 | 202 |
| 3150 | 174 | 2 | 4.2 | 320 | 84 | 1560 | 194 | 0.19 | 0.2 | 730 | 0.12 | 3670 | 0.06 | 69 | 1220 | 4800 | 1.06 | 219 | 0.54 | 5020 | 65.8 |
| 2340 | 121 | 19 | 7 | 212 | 28 | 1180 | 13.4 | 0.67 | 0.4 | 525 | 0.13 | 2890 | 0.24 | 16.7 | 116 | 3500 | 0.47 | 145 | 0.52 | 3150 | 49.3 |
| 15600 | 178 | 10 | 76.0 | 970 | 127 | 3410 | 400 | 0.76 | 0.21 | 2120 | 0.18 | 0069 | 0.2 | 105 | 360 | 11500 | 1.64 | 458 | 0.64 | 12800 | 177 |
| 8100 | 170 | 7 | 7.8 | 342 | 88 | 3700 | 102 | 0.44 | 0.3 | 2380 | 0.11 | 9100 | 0.08 | 77 | 360 | 12400 | 1.79 | 548 | 0.68 | 22400 | 293 |
| 2850 | 180 | 5 | 3.06 | 98 | 46 | 1680 | 51 | 0.17 | 0.52 | 929 | 0.16 | 5600 | 0.04 | 35.4 | 630 | 5170 | 0.6 | 239 | -0.07 | 5600 | 174 |
| 6000000 | 51000000 | 860000 | 7800000 | 57000000 | 200000 | 320000 | 910000 | 145000 | 40000 | 152000 | 100000 | 3600 | 60000 | -20 | 9200 | 28000 | -34000 | 900 | 84000 | 132000 | 140 |
| 0000006 | 70000000 | 1600000 | 2630000 | 47000000 | 75000 | 150000 | 180000 | 152000 | 38000 | 240000 | -13000 | -3800 | 19000 | 1600 | 21000 | 23300 | 23000 | -220 | 86000 | 280000 | 1230 |
| 9300000 | 26300000 | 2100000 | 5700000 1 | 39000000 | 243000 | 660000 | 640000 | 420000 | 80000 | 183000 | 7300 | 4200 | 5700 | 1760 | 54000 | 2000 | 0 | 260 | 29000 | 259000 | 1160 |
| 3200000 | 14100000 | 1880000 | 3400000 | 85000000 | 130000 | 420000 | 270000 | 192000 | 56000 | 43000 | 1100 | 1300 | 3700 | 1150 | 32000 | 10500 | -3500 | 70 | 0006 | 72000 | 6- |
| 400000 | 26000000 | 11300000 | 2210000 1 | 32000000 | 160000 | 540000 | 450000 | 330000 | 71000 | 92000 | 4100 | 1800 | -3800 | 1670 | 51000 | 26100 | 12000 | 80 | 17400 | 159000 | 370 |
| 340000 | 68000000 | -7400000 1 | 0200000 | 76000000 | 83000 | 295000 | 310000 | 243000 | 160000 | 137000 | 2900 | 1400 | 80000 | 1050 | 44000 | 95000 | 25000 | 60 | 42000 | 201000 | 750 |
| 100000 | 18000000 | -1790000 | 2900000 | 87000000 | 119000 | 360000 | 239000 | 221000 | 51000 | 84000 | 5500 | 18000 | 400 | 1320 | 29000 | 18400 | 3700 | 90 | 11600 | 122000 | 550 |
| 8900000 | 16900000 | -1530000 | 2070000 1 | 48000000 | 153000 | 621000 | 350000 | 337000 | 94000 | 71000 | 1800 | 1950 | 5400 | 1400 | 51500 | 7600 | 80000 | -85 | 10100 | 72000 | 290 |
| 0000000 | 92000000 | -2100000 1 | 4400000 2 | 380000000 | 290000 | 610000 | 1580000 | 400000 | 700000 | 330000 | 40000 | 11800 | 11000 | 300 | 73000 | 80000 | 700000 | -500 | 118000 | 265000 | 1300 |
| 6000000 | 58000000 | -200000 | 1250000 | 70000000 | 29000 | 63000 | 1490000 | 194000 | 40000 | 350000 | 28000 | 10300 | 11000 | 300 | 19000 | 46000 | 34000 | 440 | 00009 | 177000 | 06- |
| 50 | 158 | 4.6 | 1.1 | -6.6 | 0.44 | -1.9 | -0.76 | -0.32 | -1 | -0.2 | 0.37 | 24.9 | 0.17 | 0.01 | 0.01 | -0.12 | -0.05 | 0.03 | 29.4 | 0.03 | -0.01 |
| 41 | 131 | 5.4 | 0 | 10.6 | -0.07 | 1.3 | 0.5 | 0.1 | 2.3 | 0.23 | 0.40 | 25.1 | -0.01 | 0.01 | 0.06 | -0.13 | 0.03 | 0 | 37.1 | 0.05 | -0.01 |
| 0 | 153 | -1.8 | -0.6 | 1.5 | 0.01 | -0.4 | -0.29 | 0.19 | 2 | -0.38 | -0.07 | 10.5 | 0.15 | 0.01 | 0.03 | -0.09 | 0.01 | -0.01 | 56.3 | 0.11 | 0.02 |
| 52 | 154 | 4.3 | -1.2 | 15.2 | 0.19 | -0.4 | 5.2 | 0.14 | -1.15 | 1.48 | -0.03 | 15.5 | 0.14 | 0.02 | 60.0 | 0.12 | -0.02 | 0.01 | 38.9 | 0.39 | 0.04 |
| 176 | 286 | 10.8 | 141.0 | 4660 | 1.61 | 5.2 | п | 2.21 | 1.35 | 3.28 | 0.11 | 9.48 | -0.17 | 0.03 | 0.23 | 0.11 | 0.06 | -0.01 | 16.8 | 1.26 | 0 |
| 39 | 175 | 1.3 | 14.1 | 390 | -0.08 | 1.8 | 1.29 | 0.58 | 2.2 | 0.45 | -0.59 | 18.4 | 0.06 | 0.02 | 0.01 | 0.24 | -0.05 | 0 | 25.1 | 0.15 | 0 |
| 13 | 195 | 5.9 | 5.4 | 234 | -0.69 | 1.3 | 0.5 | -0.13 | 0 | 1.27 | -0.5 | 17.2 | -0.44 | 0 | 0 | 0.2 | -0.1 | -0.01 | 26.9 | 0.13 | 0.01 |
| 34 | 118 | 1.1 | 14.9 | 410 | -0.28 | 1.9 | 2.6 | 0.62 | -1.5 | 0.58 | -0.35 | 13.5 | 0.07 | 0.01 | 0.05 | 0.06 | 0.14 | -0.01 | 25.2 | 0.16 | 0 |
| S | 149 | 1 | 0.5 | T.T | -0.14 | -1.9 | 0.59 | 0.46 | -0.86 | 0.7 | -0.16 | 18.6 | -0.01 | -0.01 | -0.05 | 0.05 | -0.01 | -0.01 | 48.3 | 0.04 | 0 |
| 16 | 267 | 2.3 | 3.1 | 355 | -0.04 | -0.8 | 6.3 | 0.37 | -1.5 | 0.69 | 0.42 | 13.7 | 0.38 | -0.01 | 0.79 | 0.3 | -0.02 | 0 | 198 | 1.45 | 0.04 |
| 25900 | 176 | 31 | 32.0 | 1000 | 0.22 | 1.34 | 187 | 0.92 | 0 | 7.8 | 0.14 | 58.9 | 0.22 | 0 | 0.18 | 0.19 | 0 | 0.01 | 404 | 3.03 | 0.02 |
| 14700 | 213 | 20 | 23.0 | 380 | 0.08 | 0.65 | 126 | 0.42 | 0.12 | 5.3 | 0.13 | 65 | 0.18 | 0 | 0.1 | 3.4 | 0 | 0.01 | 232 | 1.62 | 0.01 |
| 18300 | 250 | 61 | 18.8 | 291 | 0.05 | 0.92 | 119 | 0.51 | 0.16 | 5.8 | 0.08 | 119 | 0.24 | 0 | 0.06 | 0.07 | 0 | 60.0 | 324 | 2.8 | 0.01 |
| 28100 | 229 | -429 | 85.0 | 3800 | 1.05 | 3.61 | 223 | 0.87 | 0.5 | 14.7 | 0.67 | 1210 | 0.4 | 0 | 0.3 | 0.14 | 0.03 | 1.5 | 351 | L.L | 0.03 |
| 24400 | 204 | -29 | 33.0 | 650 | 0.1 | 0.62 | 140 | 0.76 | 0.21 | 7.9 | 0.29 | 350 | 0.18 | 0 | 0.28 | 0.1 | 0.01 | 0 | 341 | 2.43 | 0.01 |
| 14500 | 219 | -5.2 | 6.4 | 218 | -0.05 | 0.58 | 90.0 | 0.34 | 0.21 | 4.9 | 0.11 | 372 | 0.14 | 0 | 0.12 | 0.03 | 0 | 0 | 183 | 1.0 | 0.01 |
| 8500 | 233 | -0.4 | 7.4 | 188 | 0 | -0.01 | 68.6 | 0.12 | 0 | 2.98 | 0.01 | 350 | 0.13 | 0.01 | 0.03 | 0.9 | -0.01 | 0 | 139 | 0.74 | 0.01 |
| 6200 | 238 | -6.2 | 3.3 | 86 | -0.05 | -0.12 | 46.3 | 0.17 | 0.22 | 2.12 | 0.2 | 60.6 | 0.14 | 0 | 0.03 | 0.03 | 0 | 0.02 | 88.7 | 0.34 | 0 |
| 6440 | 256 | -0.7 | 6.3 | 104 | 0.09 | 0.44 | 46 | 0.07 | 0.04 | 2.38 | 0.06 | 60.6 | 0 | 0.01 | 0.22 | 0.03 | 0 | 0 | 151 | 0.51 | 0 |
| 6310 | 248 | -1.6 | S | 62 | -0.09 | 0.41 | 39.9 | 0.05 | -0.29 | 2.09 | 0.14 | 172 | 0.04 | 0 | 0.02 | 0 | 0.01 | 0 | 94 | 0.35 | 0.04 |

| 69 H | S*S MBH 69 | ⁵³ Cr MBH 69 | uM ^{cc} | ²⁰ Fe MBH 66 | ⁵⁹ Co MBH 69 | wNi MBH 69 | wZn MBH 69 | MASSI | MBH 66 | ABH 69 | ⁹⁵ Mo MASSI | MBH 69 | MBH 69 | MBH 69 | ¹¹⁸ Sn MBH 72 | ¹²¹ Sb MBH 69 | ¹²⁵ Te MBH 69 | ¹⁹⁷ Au MBH 66 | ²⁰² Hg MASSI | ²⁰⁸ Pb MBH 66 | ²⁰⁹ Bi MBH 66 |
|------|---------------|----------------------------|------------------|----------------------------|----------------------------|---------------|---------------|-------|---------------|--------|---------------------------|--------|--------|--------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|----------------------------|-----------------------------|-----------------------------|
| | 166 | 3.36 | 430 | 2360 | 76.0 | 10 | 403 | 2.72 | 0.44 | 16.8 | 96.0 | 202 | 0.81 | 0.42 | 1.1 | 0.5 | 0.07 | 0.15 | 905 | 7.4 | 0.19 |
| | 194 | 0.99 | 168 | 1000 | 0.27 | 1.35 | 196 | 0.93 | 0.22 | 7.46 | 0.15 | 187 | 0.42 | 0 | 0.4 | 0.09 | 0.04 | 0.04 | 489 | 2.92 | 0.09 |
| | 167 | 1.03 | 214 | 1110 | 0.37 | 7 | 247 | 1.44 | 0.21 | 7.01 | 0.2 | 202 | 0.54 | 0.11 | 0.36 | 0.31 | 0.04 | 10.0 | 546 | 41 | 0.34 |
| | 175 | 0.0 | 126 | 363 | 0.2 | 0.93 | 158 | 0.69 | 0.23 | 13 | 0.22 | 379 | 0.38 | 0.03 | 0.2 | 60.0 | 0.01 | 10.0 | 402 | 2.5 | 0.07 |
| | 164 | 0.37 | 101 | 272 | 0.23 | 0.79 | 134 | 0.58 | 0.3 | 5.68 | 0.61 | 177 | 0.31 | 0.01 | 0.08 | 0.1 | 0.02 | 0.01 | 326 | 1.99 | 0.07 |
| | 161 | 0.26 | 76 | 219 | 0.09 | 0.94 | 100 | 0.49 | 0.33 | 5.26 | 0.05 | 239 | 0.24 | 0.01 | 0.1 | 0.05 | 0.01 | 0 | 304 | 1.43 | 0.08 |
| | 156 | 0.12 | 46 | 112 | 0.03 | 0.98 | 45.9 | 0.33 | 0.28 | 2.66 | 0.01 | 254 | 0.16 | 0 | 0.07 | 0.06 | 0 | 0 | 141 | 0.53 | 0.03 |
| | 148 | 0.08 | 53 | 122 | 0.02 | 0.8 | 56 | 0.32 | -0.04 | 3.29 | 0.07 | 281 | 0.17 | 0 | 0.06 | 0.09 | 0 | 0 | 209 | 0.94 | 0.07 |
| | 138 | 0.06 | 30 | 45 | -0.01 | 0.68 | 28.4 | 0.21 | 0.15 | 2.45 | 0.04 | 95.8 | 0.05 | 0 | 0.05 | 0.07 | 0 | 0 | 125 | 0.33 | 0.03 |
| | 260 | 1.44 | 4210 | 1960 | 1.96 | 16.1 | 273 | L.L | 1.72 | 16.8 | 0.5 | 205 | 1.3 | 0.17 | 5.9 | 0.29 | 0.01 | 0.03 | 1.19 | 6.9 | 0.18 |
| | 256 | 1.07 | 1820 | 840 | 0.82 | 11.4 | 197 | 3.59 | 1.47 | 10.3 | 0.37 | 162 | 1.63 | 0.02 | 3.0 | 0.17 | 0 | 0.04 | 0.45 | 3.83 | 0.11 |
| | 222 | 0.87 | 3250 | 1040 | 0.93 | 12.0 | 267 | 3.56 | 0.94 | 6.6 | 0.22 | 188 | 0.82 | 0.03 | 1.97 | 0.18 | 0 0 | 0.03 | 0.5 | 4.7 | 0.14 |
| | 283 | 1.24 | 1240 | 080 | 0.35 | 8.2 | 167 | 2.8 | 0.31 | 13.0 | 0.04 | 490 | 11 | 0.03 | 1.10 | 0.12 | • • | 0.04 | 0.88 | 3.06 | 0.17 |
| | 245 | 1.03 | 1110 | 83U 640 | 70.0 | 1.0 | 213 | 1 07 | 16.0 | 7.11 | 17.0 | 180 | 1.10 | 20.0 | 0.88 | 21 O | 0 | 20.0 | 0.72 | 1.89 | 1.0 |
| | 007 | 5.1 | 1110 | 000 | 0.00 | 1.0 | 160 | 121 | 0.00 0 5 0 | 1 42 | 60.0 | 310 | 1.12 | 70.0 | 0.98 | 01.0 | 10.0 | 70.0 | 0.40 | 1.04 | 0.10 |
| | 100 | 17.1 | 0101 | 440 | 0.61 | 6.4 | 100 | 1 73 | 00.0 | 6.06 | 0.53 | 5 96 | 1 57 | 100 | 0.56 | 110 | 50.0- | 20.0 | 0.47 | 1.04 | 1.0 |
| | 312 | 2.6 | 1010 | 1290 | 0.79 | 9 | 265 | 2.99 | 0.81 | 22.0 | 0.48 | 250 | 1.94 | 0.06 | 3.5 | 0.11 | 0.04 | 0.1 | 1.9 | 3.4 | 0.19 |
| | 380 | 2.7 | 830 | 940 | 0.77 | 7.3 | 228 | 6.37 | 1.07 | 13.9 | 0.02 | 152 | 2.47 | 0.01 | 0.48 | 0.27 | 0 | 0.04 | 0.35 | 1.74 | 0.11 |
| | 175 | 0.79 | 350 | 1690 | 0.56 | 2.2 | 350 | 2.91 | 0.48 | 14.1 | 0.44 | 55.4 | 1.13 | 0.05 | 3.8 | 0.33 | 0.09 | 0.12 | 444 | 3.7 | 0.23 |
| | 225 | 0.57 | 212 | 1100 | 0.37 | 1.3 | 254 | 2.17 | 6.0 | 6 | 0.17 | 80 | 1.27 | 0.05 | 10 | 0.31 | 0.03 | 0 | 287 | 3.3 | 0.2 |
| | 185 | 0.88 | 390 | 1490 | 0.84 | 2.2 | 380 | 2.7 | 0.6 | 11.6 | 1.7 | 74.2 | 1.7 | 0.39 | 0.91 | 0.51 | 0.09 | 0.17 | 247 | 6.3 | 0.27 |
| | 196 | 0.24 | 107 | 268 | 0.22 | 2.3 | 182 | 1.6 | 0.95 | 12.7 | 0.85 | 73.3 | 0.37 | 0.84 | 0.7 | 0.59 | 0.25 | 0.01 | 323 | 4.1 | 0.18 |
| | 239 | 0.53 | 82 | 357 | 0.25 | 2.8 | 210 | 1.91 | 11 | 15 | 0.8 | 103 | 1.1 | 0.31 | 1.6 | 3.6 | 0.12 | 0.06 | 840 | 5.5 | 0.2 |
| | 242 | 0.83 | 596 | 1140 | 0.4 | 0.55 | 358 | 1.91 | 0.1 | 13.7 | 0.23 | 47.6 | 2.22 | 0.01 | 0.14 | 0.12 | 0.38 | 0.01 | 297 | 2.11 | 0.19 |
| | 214 | 0.46 | 356 | 440 | 0.38 | 2.0 | 284 | 1.6 | 0.16 | 10.1 | 67.0 | 46.7 | 0.74 | 5.0 | 0.16 | 1.0 | 0.02 | 10.0 | 292 | 1.1 | 60.0 |
| | 207 | 2.1 | 250 | 860 | 0.2 | 1.09 | 420 | 2.58 | 0.59 | 13.8 | 0.36 | 148 | 0.84 | 0.27 | 0.39 | 0.31 | 0.09 | 0.03 | 203 | 3.8 | 0.17 |
| | 162 | 0.2 | 65 | 134 | 0.02 | 0.62 | 136 | 0.65 | 0.3 | 4.8 | 0.3 | 118 | 0.54 | 0.01 | 0.03 | 0.05 | 0.06 | 0 | 16 | 0.54 | 0.04 |
| | 244000 | -4900 | 430000 | 372000000 | 620 | 2000 | 341000 | 800 | 3400 | 1700 | -10 | 106 | 100 | 158 | 40000 | 130 | 41 | 15 | 1490 | 115000 | 39 |
| | 289000 | -1000 | 840000 | 41000000 | 1150 | -210 | 510000 | 80 | 3590 | 860 | 200 | 206 | -30 | 107 | 16400 | 220 | 99 | 28 | 1320 | 13700 | 48 |
| | 115000 | -5800 | 450000 | 16400000 | 282 | 1530 | 205000 | 447 | 1360 | 089 | 20 | 118 | × ; | 56 | 11000 | 66 | 32 | 6.7 | 630 | 41400 | 44.9 |
| | 000/17 | -3300 | 1440000 | 44000000 | 850 | 0096 | 352000 | 066 | 3070 | 0111 | 07- | 200 | 01- | 115 | 19600 | 107 | 10 | 2 | 1750 | 00461 | 200 |
| | 245000 | 0069- | 660000 | 41400000 | 860 | 1400 | 341000 | 410 | 3300 | 970 | -50 | 178 | 50 | 65 | 15000 | 199 | -94 | 38 | 1640 | 16400 | 8 |
| | 336000 | 3200 | 910000 | 53000000 | 890 | 400 | 50000 | 210 | 4000 | 1350 | 70 | 271 | -70 | 09 | 16600 | 151 | 50 | 18 | 1750 | 15600 | Ш |
| | 185000 | -2400 | 530000 | 312000000 | 550 | 660 | 260000 | 240 | 2040 | 1030 | -80 | 115 | 38 | 147 | 30300 | 156 | -62 | 52 | 850 | 19200 | 58 |
| | 268000 | -1700 | 570000 | 45000000 | 460 | 096 | 390000 | 290 | 3000 | 800 | 250 | 181 | -72 | 133 | 23000 | 190 | -50 | 36 | 1310 | 20200 | 56 |
| | 410000 | 5400 | 670000 | 67000000 | 760 | 500 | 450000 | 420 | 3400 | 100 | -160 | 200 | 06 | 86 | 26000 | 108 | -150 | 27 | 1010 | 37300 | 74 |
| | 100 | 1.02- | 501 | 3240 | 0.0 | 5C.2 | 0 8 | 1.83 | 0.14 | 5/-1 | 10.11 | 607 | 67.0 | 70.0 | 6/.1 | 20.0 | 0.10 | 70.0 | 0.00 | 10.4 | 50.0 |
| | 162 | 07- | 1/1 | 1090 | 0.0 | 2.06 | 76 | 1 25 | 11.0 | 15.2 | 0.00 | 2.2 | 0.11 | c0.0 | 3.6 | 10.0 | 000 | | 0.05 | 3.0 | 11.0 |
| | 246 | -35 | 88 | 3200 | 0.36 | 1.88 | 22 | 1.03 | 0.03 | 1.42 | 0.2 | 2.65 | 0.17 | 0.04 | 3.2 | 0.08 | -0.22 | 0.01 | 0.35 | 4.9 | 0.15 |
| | 305 | -55 | 105 | 1510 | 0.42 | 1.3 | 80 | 1.24 | 0.22 | 2.0 | 0.3 | 2.11 | 0.33 | 0.01 | 0.49 | -0.01 | -0.18 | 0 | 0.62 | 5.53 | 0.05 |
| | 263 | -20.1 | 80 | 1060 | 0.24 | 1.26 | 39.7 | 1.7 | 0.28 | 1.29 | 0.1 | 3.24 | 0.18 | 0.02 | 0.79 | -0.01 | 0.06 | 0.01 | 0.52 | 3.13 | 0.11 |
| | 227 | 43 | 134 | 2030 | 0.42 | 2.17 | 71.7 | 1.86 | 0.23 | 1.32 | 0.28 | 1.97 | 0.3 | 0.01 | 0.84 | 0.03 | 0.26 | 0 | 0.35 | 4.54 | 0.03 |
| | 252 | -59 | 86 | 1910 | 0.28 | 1.45 | 43.4 | 0.98 | -0.31 | 1.25 | 0.26 | 2.27 | 0.25 | 0.02 | 0.66 | 0.02 | -0.21 | 0 | 0.52 | 3.38 | 0.03 |
| | 237 | -31 | 72 | 1010 | 0.22 | 0.44 | 26.4 | 0.75 | 0.05 | 0.8 | 0.07 | 2.96 | 0.23 | 0 | 0.47 | 0.03 | -0.04 | 0 | 0.33 | 2.02 | 0.04 |
| | 284 | -95 | 106 | 2430 | 0.22 | 1.68 | 75 | 1.28 | 0.32 | 1.44 | 0.14 | 4.07 | 0.26 | 0.01 | 1.8 | 0.04 | 0.05 | 0 | 0.51 | 3.2 | 0.05 |

| | 209Bi | MBH 00 | 0.9 | 0.47 | 0.34 | 0.63 | 0.15 | 0.28 | 0.24 | 0.14 | 0.02 | 0.02 | 0.01 | 0.02 | 0.01 | 10.0 | | 0.01 | 0.01 | 0.06 | 0.04 | 0.01 | 0.01 | 0.01 | 0.05 | 0.03 | 0.01 | 0.02 | 0.02 | 0.22 | 10.0 | 0.02 | 0.03 | 0.03 | 0 | 50'O | | 0.53 | 0.08 | 0.03 | 0.1 | 0.02 | 0.12 | 0.03 | 0.03 | 0.03 |
|-------------|-----------------------|----------------|----------|----------|----------|----------|----------|----------|--------|-----------|----------|--------|----------|----------|----------|--------|--------|----------|-----------|---------|-------|-------|---------|-------|-------|-------|---------|---------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------------------------------------------------------------------------------------------------------------|
| | ²⁰⁸ Pb | 1 07 | 2.5 | 1.03 | 2.22 | 1.55 | 0.38 | 0.86 | 1.39 | 0.26 | 0.63 | 1.11 | 0.35 | 0.19 | 0.06 | 10.0 | 90.06 | 0.13 | 0.26 | 144 | 100 | 150 | 136 | 135 | 78 | 74.5 | 50.5 | 93.6 | 55.6 | 15 | 0.74 | 1.6 | 0.46 | 0.53 | 1.3 | 0.36 | 11.0 | 1 | 1.84 | 0.79 | 0.55 | 0.67 | 38 | 1.5 | 0.51 | 0 67 |
| | 202Hg | 136 | 1.32 | 0.87 | 2.5 | 1.34 | 0.66 | 0.99 | 0.93 | 0.33 | 1.79 | 0.54 | 0.44 | 0.56 | 0.56 | 0.33 | 0.24 | 0.34 | 0.4 | 4.9 | 7.96 | 6.81 | 5.64 | 6.77 | 8.34 | 13.6 | 6.55 | 5.25 | 6.03 | 1.59 | CK.0 | 1.27 | 0.55 | 0.61 | 1.5 | 6/.0 | 0.67 | 6.5 | 1.63 | 0.89 | 0.75 | 0.9 | 7.65 | 3.44 | 9 | 1 25 |
| | ¹⁹⁷ Au | 00 LIGH | 0.0 | 0.01 | 0 | 0.21 | 0.0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 0 | | 0 | 0.01 | 0.01 | 0 | 0 | 0.01 | 0.01 | 0.01 | 0.02 | 0.01 | 0.01 | 0 | 0.04 | cn:n | 0.01 | 0.06 | 0 | 0 | 0 0 | 0.01 | 0.03 | 0.09 | 0 | 0.01 | 0.01 | 0.02 | 0 | -0.01 | |
| | ¹²⁵ Te | 0 1/0 0 1/0 | 0.12 | 0.09 | -0.02 | 0.14 | 10.07 | 0.14 | 0.1 | -0.03 | 0.08 | 0.01 | 60.0 | 0.16 | -0.01 | 60.0 | 0.04 | 0.05 | 0.08 | 0.08 | 0.05 | 0.08 | 0.08 | 0.01 | 0.01 | 0.01 | 0.01 | -0.01 | 0 | 0.2 | 110 | 0.08 | 0.1 | 0.03 | 0.05 | 0.04 | 20.0 | 0.29 | 0.1 | 0.07 | 0.09 | 0.1 | 0.17 | 0.1 | 0.24 | 000 |
| | 121Sb | MBH 09 | 0.1 | 0.04 | 0.07 | 0.09 | 0.03 | 0.05 | 0.07 | 0.00 | 0.04 | 0.07 | 0.01 | 0.03 | 0.05 | 20.0 | 0.01 | 0.07 | 0.04 | 0.83 | 1.17 | 1.06 | 0.73 | 0.92 | 0.9 | 1.04 | 0.49 | 0.68 | 0.65 | 0.59 | 016 | 0.42 | 0.8 | 0.12 | 0.07 | 0.05 | 0.06 | 1.31 | 0.19 | 0.14 | 0.08 | 0.06 | 0.26 | 0.23 | 0.14 | |
| | 118Sn | 7/ HBM | 0.98 | 0.45 | 0.48 | 0.8 | 0.10 | 0.23 | 0.81 | 0.2 | 0.27 | 0.3 | 1.56 | 0.26 | 0.06 | 10.0 | 1.0 | 0.32 | 0.16 | 2.6 | 5 | 1.16 | 0.79 | 0.88 | 0.66 | 0.79 | 0.42 | 1.12 | 0.46 | 1.8 | 10.0 | 0.44 | 1.09 | 0.12 | 0.12 | 61.0 | 0.06 | 1.45 | 2.2 | 1.53 | 0.38 | 0.28 | 0.75 | 0.24 | 0.32 | |
| | пзп 1.001 | 0 11 0 | 0.02 | 0.01 | 0.24 | 0.07 | 70.0 | 0.01 | 0.01 | 0 | 0.01 | 0 | 0 | 0 | 0 0 | • | | 0.01 | 0 | 0.01 | 0.01 | 0.22 | 0 | 0 | 0.01 | 0 | 0 | 0 | 0 | 0.06 | 10.0 | 0.01 | 0.01 | 0 | 90.0 | 10.0 | 10.0 | 0.4 | 0.12 | 0 | 0 | 0.01 | 0.04 | 0.01 | 0.04 | |
| | III Cd | 0 10 V0 | 0.29 | 0.18 | 0.11 | 0.33 | 1.6 | 0.2 | 0.41 | 0.09 | 0.02 | 0.01 | 0.06 | 0.11 | 0.06 | 10.0 | 0.03 | 0.06 | 0.15 | 0.56 | 0.22 | 0.37 | 0.29 | 0.39 | 0.47 | 0.4 | 0.28 | 0.29 | 0.28 | 0.35 | 0.14 | 0.2 | 0.14 | 0.15 | 0.18 | 0.15 | 110 | 0.83 | 0.72 | 0.32 | 0.23 | 0.24 | 0.54 | 0.4 | 0.51 | |
| | 107 Ag | KO LIGIN | 257 | 221 | 810 | 612 | 205 | 491 | 263 | 930 | 76 | 48.1 | 93.3 | 36.5 | 88.3 | 40.8 | 1.00 | 42.6 | 42.6 | 4.05 | 10.9 | 5.8 | 7.64 | 7.86 | 18.1 | п | 10.5 | 2.77 | 45 | 140 | 2.00 | 19 | 115 | 111 | 40 | 4/.9 | 8 | 130 | 171 | 163 | 152 | 250 | 182 | 118 | 126 | The second se |
| | oW ⁵⁶ | ICCEM 0.2 | 03 | 0.21 | 0.47 | 0.26 | 90.0 | 0.2 | 0.26 | 0.05 | 0.89 | 1.5 | 0.48 | 2.8 | 0.4 | c6.0 | 1.27 | 6.37 | 17 | 52.9 | 28.1 | 46.4 | 34 | 44.9 | 35.7 | 36.4 | 15.1 | 45.4 | 24 | 0.32 | 21.0 | 0.1 | 0.12 | 0.12 | 0.27 | 81.0 | 21.0 | 0.7 | 0.22 | 0.15 | 0.03 | -0.03 | -0.12 | 0.27 | -0.29 | |
| | 75As | KO LIGIN | 13.1 | 8.21 | 7.46 | 10.7 | 4.83 | 1.7 | 10.5 | 3.08 | 1.56 | 1.60 | 0.41 | 1.03 | 0.11 | 15.0 | 69 0 | 4.54 | 11.5 | 145 | 93 | 154 | 143 | 174 | 93 | 130 | 98 | 281 | 83.6 | 20.2 | 5 11 | 11.8 | 8.1 | 5.3 | 4.08 | 6.24 | 276 | 10.9 | 7.4 | 4.36 | 4.09 | 2.73 | 9.4 | 10.4 | 6 | |
| | ⁷² Ge | 00 HBH 00 | 0.27 | 0.22 | 0.45 | 0.87 | 0.01 | 0.16 | 0.92 | -0.09 | 0.54 | 0.40 | 0.22 | 0.54 | 0.55 | 0.32 | 0.20 | 0.53 | 06.0 | 0.40 | 0.60 | 0.41 | 0.67 | 0.61 | 0.72 | 0.66 | 0.15 | 0.45 | 0.54 | 0.28 | 60.0 | 0.29 | 0.16 | 0.02 | 0.49 | 0.32 | 1010 | 0.38 | 0.4 | 0.27 | 0.26 | 0.4 | 0.6 | 0.83 | 1.1 | |
| | ⁷¹ Ga | 2 19 | 2.38 | 2.01 | 1.62 | 3.04 | 0.68 | 1.36 | 2.50 | 0.65 | 1.23 | 1.42 | 0.30 | 0.50 | 0.16 | 60.0 | 0.16 | 0.86 | 1.75 | 1.28 | 1.17 | 1.23 | 1.04 | 1.22 | 1.57 | 1.08 | 0.47 | 0.85 | 0.74 | 2.41 | 27.1 | 1.77 | 1.08 | 0.74 | 0.56 | 66.0 | 010 | 2.15 | 2.25 | 1.1 | 1.02 | 0.71 | 1.78 | 1.1 | 0.77 | |
| | uZ ⁵⁰ | 40 LIDIN | 121 | 74.7 | 67.3 | 85 | 90 3 | 61 | 108 | 29.5 | 14.1 | 18.8 | 4.5 | 9 | 2.1 | 4.34 | 3.4 | 9.1 | 11.8 | 33.6 | 34.7 | 84.9 | 7.66 | 61.9 | 23.3 | 16.7 | 16.3 | 28 | 17.6 | 5 | 46 | 42.4 | 27.1 | 25 | 14 | 9 5 | 12 | 246 | 164 | 118 | 113 | 78.6 | 260 | 128 | 253 | |
| | iN ⁰⁰ | 2 00 C | 1.32 | 0.91 | 0.92 | 1.39 | 40 | 0.31 | 0.79 | -0.04 | 1.91 | 2.8 | 0.62 | 1.38 | -0.3 | 77.0 | 6.0 | 2.44 | 3.91 | 3.5 | 3.88 | 1.82 | 1 | 0.8 | 2.06 | 2 | 0.93 | 1.85 | 0.7 | 1.53 | 7 0 40 | 0.89 | 0.32 | 0.46 | 0.56 | 0.47 | 20.0 | 3 | 1.22 | 1.23 | 0.82 | 0.87 | 4 | 1 | ŝ | |
| | ⁵⁹ Co | 40 LIGIN | 0.58 | 0.1 | 0.14 | 1.7 | 71.0 | 0.1 | 0.31 | 0.1 | 1.73 | 2.8 | 0.16 | 16.0 | 0.18 | 11.0 | 0.24 | 1.6 | 2.34 | 0.28 | 0.35 | 0.21 | 0.2 | 0.24 | 0.28 | 0.2 | 0.09 | 0.14 | 0.24 | 0.32 | 10 | 0.48 | 0.08 | 0.15 | 0.1 | -0.04 | 0.03 | 0.8 | 0.77 | 0.14 | 0.15 | 0.13 | 0.14 | 0.04 | 6.0 | |
| | ⁵⁶ Fe | 00 HBM | 1090 | 840 | 830 | 1130 | 000 | 680 | 1480 | 160 | 1620 | 3840 | 260 | 970 | 180 | 000 | 380 | 2560 | 5060 | 1150 | 1270 | 910 | 1200 | 930 | 1010 | 474 | 588 | 1100 | 480 | 1670 | 800 | 1370 | 630 | 245 | 140 | 117 | 46 | 402 | 359 | 213 | 175 | 183 | 390 | 123 | 16 | |
| | Min ⁵⁵ Min | TOCHW 100 | 56 | 17.4 | 23.9 | 41 | 107 | 28 | 100 | 7.3 | 31.9 | 42.2 | 3.3 | 12.7 | 2.7 | P.0. | 8.8 | 34.1 | 54.6 | 20 | 27.7 | 7.8 | 10.2 | 7 | 12.62 | 10.7 | 4.7 | 7.9 | 4.11 | 57.1 | 2.00 | 37.7 | 22.5 | 11.4 | 11.4 | 1.61 | 1.5 | 62 | 69 | 54 | 32 | 23 | 275 | 247 | 630 | |
| | ³³ Cr | MB/1 09 | 10.4 | 6.87 | 7.1 | 6.8 | 1.0 | 2.93 | 5.33 | 1.43 | 2.62 | 1.91 | 0.66 | 0.55 | 0.23 | 77.0 | 0.38 | 76.0 | 0.92 | 4.55 | 3.95 | 5.3 | 4.94 | 5.15 | 5.11 | 4.41 | 3.33 | 5.8 | 2.93 | 2.81 | 1 10 | 2.19 | 1.28 | 0.92 | 0.68 | 0.04 | 0.63 | 3.41 | 2.34 | 1.68 | 1.42 | 1.88 | 3.40 | 3.22 | 5 | |
| | S ⁴⁵ | 101 | 212 | 247 | 285 | 295 | 195 | 269 | 297 | 177 | 155 | 209 | 202 | 287 | 240 | 512 | 304 | 306 | 371 | 440 | 467 | 423 | 428 | 430 | 402 | 338 | 345 | 360 | 315 | 124 | 158 | 134 | 131 | 185 | 198 | 190 | 201 | 101 | 109 | 117 | 116 | 111 | 950 | 773 | 2350 | |
| - continued | JIP 40 | 40 LIGH | 48600 | 29700 | 25800 | 32000 | 14400 | 25000 | 30300 | 6600 | 680 | 461 | 154 | 139 | 5 | 011 | 164 | 261 | 428 | 11870 | 11800 | 16300 | 18200 | 16900 | 13200 | 13900 | 7500 | 7390 | 11400 | 67900 | 41100 | 48400 | 31800 | 22500 | 17300 | 006/7 | 7600 | 104700 | 71200 | 49300 | 40200 | 31900 | 98000 | 47800 | 44000 | |
| Appendix A | | 0507 1 | 8587 - 2 | 8587 - 3 | 8587 - 4 | 8587 - 5 | 0 - 10C0 | 8587 - 8 | 8587-9 | 8587 - 10 | 8577 - 1 | 8577-2 | 8577 - 3 | 8577 - 4 | 8577 - 5 | 0-1/02 | 8-11-8 | 8577 - 9 | 8577 - 10 | 099 - 1 | 099-2 | 099-3 | 099 - 4 | 5-660 | 9-660 | 1-660 | 8 - 660 | 6 - 660 | 099 - 10 | 8568 - 1 | 2 - 2005 | 8568 - 4 | 8568 - 5 | 8568 - 6 | 8568 - 7 | 8 - 8068 | 8568 - 10 | 8572 - 1 | 8572 - 2 | 8572 - 3 | 8572 - 4 | 8572 - 5 | 8572 - 6 | 8572 - 7 | 8572 - 8 | 0.0000 |

| Appendix A - c | Intinued | | | | | | | | | | | | | | | | | | | | |
|-------------------------|--------------------------------|------------------|-------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-------------------|--------|----------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | S _{FC} d ₁ | ³³ Cr | ⁵⁵ Min | ⁵⁶ Fe | ³⁹ Co | iN ⁰⁰ | uZ ⁹⁹ | ⁷¹ Ga | ⁷² Ge | ⁷⁵ As | ⁹⁵ Mo | ¹⁰⁷ Ag | 111 Cd | III ⁵ III | ¹¹⁸ Sn | ¹²¹ Sb | ¹²⁵ Te | ¹⁹⁷ Au | ²⁰² Hg | ²⁰⁸ Pb | ²⁰⁹ Bi |
| 001 1 0 | HBH 69 H | 9 MBH 69 | MASSI | A10 | 0.75 | MBH 69 | MBH 69 | MASSI | MBH 66 | MBH 69 | MASSI | 1500 | 0.04 | MBH 69 | MBH 72 | 0.38 | MBH 69 | 0.06 | MASSI 4 01 | 6 70 | 0 88 00 |
| 821-2 6 | 300 178 | 30 | 22 | 313 | 0.34 | 1.4 | | 1.16 | -0.65 | 14.5 | 0.23 | 317 | 5.0 | 0.04 | 0.00 | 0.62 | 10.0- | 0.14 | 2.53 | 6.9 | 0.92 |
| 821-3 1 | 520 136 | 12.3 | 1.66 | 39 | 0.23 | 0.33 | 49 | 0.17 | 0.71 | 1.53 | 0.27 | 315 | -0.01 | 0 | 1.26 | 0.11 | 0.2 | 0.05 | 1.09 | 0.84 | 0.22 |
| 821-4 3 | 300 160 | 80 | 9.2 | 175.00 | 0.31 | 1.4 | 43 | 0.36 | 0.98 | 2.57 | 0.24 | 308 | 0.05 | 0.02 | 2.14 | 0.2 | 0.04 | 0.1 | 1.17 | 1.47 | 0.46 |
| 821-5 8 | 183 183 | 4 | 1.36 | 35.8 | -0.04 | 0.2 | 45 | 0.16 | 0.08 | 1.81 | 0.07 | 296 | 0.06 | 0.01 | 2.63 | 0.11 | 0.09 | 0.06 | 1.47 | 1.39 | 0.2 |
| 821-6 2 | 430 205 | 13 | 14.7 | 209 | 0.03 | 0.4 | 49 | 0.31 | 0.26 | 5.4 | 0.1 | 414 | 0.07 | 0.03 | 5.66 | 0.15 | 0.28 | 0.21 | 2.5 | 2.51 | 0.37 |
| 821-7 14 | 1400 276 | 58 | 114.00 | 1920 | 1.95 | 4 | 124 | 3.6 | 2.1 | 14.6 | 0.71 | 940 | 0.28 | 9.0 | L.T | 4.7 | -0.09 | 0.29 | 6 | 9.5 | 1.15 |
| 821-8 7 | 100 258 | 26 | 51 | 417 | 0.18 | 13 | 125 | 1.39 | 0.65 | 10.2 | 0.45 | 758 | 90.0 | 0.07 | 7.3 | 0.75 | 0.57 | 0.32 | 2.83 | 8.7 | 0.8 |
| 821-9 | 182 222 | 16 | 29 | 107 | -0.08 | -0.1 | 54.4 | 0.39 | 0.56 | 5.3 | 0.27 | 304 | 0.21 | 0.02 | 5.7 | 0.21 | -0.01 | 0.16 | 1.35 | 10.7 | 0.23 |
| 821-10 1 | 430 218 | 17 | 4.1 | 611 | -0.11 | • : | 4.77 | 0.3 | -0.24 | 4.8 | 0.44 | 440 | 0.08 | 0 | 5.1 | 0.39 | -0.08 | 0.13 | 1.78 | 6.10 | 1.18 |
| 211-1 2 | 100 281 | 183 | 151 | 5440 | 4.35 | 13 | 107 | 3.79 | 1.06 | 117 | 22.6 | 5.6 | 0.75 | 0.05 | 9.5 | 1.31 | 0.04 | 0.03 | 3.41 | 289 | 0.0 |
| 211-2 7 | 350 236 | 61 | 39.9 | 1960 | 0.88 | 3.7 | 36.5 | 1.65 | 0.47 | 5.16 | 21.6 | 5.89 | 0.84 | 0.03 | 2.9 | 0.7 | 10.0 | 10.0 | 2.21 | 199 | 60.0 |
| 211-3 6 | 900 247 | 89 | 09 | 2080 | 1.48 | 4.7 | 33.9 | 1.59 | 0.33 | 9.69 | 19.2 | 8.6 | 0.56 | 0.02 | 1.72 | 0.48 | 10.0- | 0 | 1.96 | 131 | 0.06 |
| 211-4 6 | 010 229 | 32 | 32 | 616 | 0.72 | 1.7 | 23.7 | 0.67 | 0.25 | 48.4 | 13.2 | 22.2 | 0.4 | 0.01 | 2.1 | 4.0 | -0.04 | 0.02 | 1.76 | 71.8 | 0.03 |
| 211-5 7 | 180 214 | 26 | 38.3 | 1430 | 1.12 | 3.2 | 23.6 | 1.12 | 0.49 | 43.0 | 13.8 | 30.9 | 0.4 | 0 | 0.92 | 0.35 | 0.03 | 0 | 8.9 | 57.3 | 0.02 |
| 211-6 9 | 8/0 | 15 | 36.9 | 1280 | 0.32 | 3.4 | 31.7 | 6.0 | 0.52 | 62.0 | 20.1 | C.01 | 0.47 | 0.02 | 2.0 | cc.0 | 0.04 | 10.0 | CC.2 | | 0.03 |
| 8 1 117 | 280 230 | 31 | 7.67 | 1000 | c.0 22 | 2.69 | 27.6 | cl.1 | 0.42 | 50.6 | 11.3 | C.61 | 0.45 | 0 100 | 0.88 | 0.47 | c0.0- | 10.0 | 3.30 | 1.09 | 0.04 |
| 0 0 110 | 707 000 | 5 | 2.24 | 040 | 0 50 | | 0.70 | 011 | 71.0 | 0.70 | C.01 | 1001 | PE O | 10.0 | CO.1 | 20.0 | 00.0 | 10.0 | 201 | 1.63 | 500 |
| C 6-117 | 047 016 | 3 5 | 0.04 | 040 | 00.0 | 7.0 | 1.77 | 01.10 | 0.0 | C.04 | 7.61 | 16.01 | +0.0 | 70.0 | 2017 | CC.0 | 500 | 10.0 | 1 66 | 1.00 | 000 |
| 211 - 10 4 962 A 1 0 | 7/7 000 | 0 | 7.4.2 | 00/ | 0.02 | CC.2 | 27.5 | 01.0 | 01.0 | 1.40 | 6.11 | 7.01 | 4.0 | | 1.0/ | 0.00 | 20.0 | 10.0 | 00.1 | 4.C/ | 70.0 |
| 6 1-VC00 | 100 200 | Ø (1 | ci t | 017 | c0.0 | 1.94 | 0.16 | 61.7 | 61.0 | 7.44 | 7.0 | 0.45 | 70'0 | 70.0 | ¥.C | 60.0 | 00.0- | 10.0 | 100 | 20.1 | 50.0 |
| 003A-2 L | 2400 201 | 10 | 160 | 107 | 11.0 | C8.U | 41.8 | 1.21 | -0.08 | 1.16 | 07.0 | C.41 | 7/.0 | 10.0 | 5.0 | c0.0 | 10.0 | 10.0 | 4.09 | 000 | 20.0 |
| 1 C - WC00 | 100 353 | 71 | 130 | 320 | 11.0 | 100 | 1.34 | 10.0 | 10.0 | 1.14 | 17.0 | t : | 16.0 | 10.0 | 10.0 | 20.06 | 100 | | 10.7 | 0.00 | 10.0 |
| 1 5-VC00 | 202 0000 | 2 5 | 110 | 340 | 0.07 | 1.21 | 42.0 | 1 78 | 0.31 | 56.6 | CT.0 | 19.7 | 70.0 | 70.0 | 1 22 | 0.08 | 10.01 | | 5 86 | 0.03 | 0.00 |
| 1 9-VE98 | 700 434 | 14 | 100 | 103 | 10.0- | 00 | 40.7 | | 1 04 | 47.4 | 0.34 | 43.0 | 0.61 | 100 | 111 | 0.07 | 1004 | | 4 83 | 0.81 | 0.03 |
| 863B - 1 1 | 590 357 | 15 | 200 | 570 | 0.17 | 1 | 10.6 | 0.86 | 0.27 | 7.4 | -0.04 | 66 | 0.18 | 0 | 0.73 | 0.03 | -0.04 | 0 0 | 5.40 | 0.5 | 10.0 |
| 863B-2 5 | 800 338 | 18 | III | 281 | 0.01 | 0.43 | 15.8 | 1.15 | 0.47 | 32.1 | 0.3 | 72 | 0.32 | 0 | 0.71 | 0.04 | 0.15 | 0.00 | 2.09 | 0.5 | 0.01 |
| 863B - 3 6 | 240 530 | п | 105 | 68 | 0.03 | 0.7 | 23.9 | 5.4 | 0.8 | 39.8 | 0.47 | 31 | 0.47 | 0 | 0.55 | 0.09 | -0.1 | -0.01 | 4.26 | 0.65 | 0.01 |
| 863B-4 8 | 400 442 | 39 | 26.8 | 09 | -0.01 | -0.15 | 15.9 | 1.83 | 0.45 | 46 | 0.23 | 20.6 | 0.19 | 0 | 0.12 | 0.03 | 0.11 | 0 | 4.41 | 0.41 | 0.03 |
| 863B-5 3 | 530 413 | 22.2 | 23.7 | 53 | 0.07 | -0.43 | 9.1 | 0.44 | 0.3 | 17.7 | 0.2 | 92.7 | 0.28 | 0.01 | 1.6 | 0 | -0.02 | 0 | 1.8 | 0.41 | 0.01 |
| 8604 - 1 4 | 360 330 | 8.5 | 23.1 | 15600 | 0.87 | 25.3 | 8910 | 10.9 | 14.4 | 1070 | 1.13 | 009 | 0.26 | 325 | 126000 | 491 | 0.16 | 121 | 0.33 | 16900 | 188 |
| 8604-2 2 | 870 278 | 15.9 | 31.4 | 12780 | 0.74 | 24.8 | 9170 | 8.45 | 9.94 | 785 | 1.03 | 069 | 0.28 | 242 | 85700 | 303 | 0.17 | 104 | 0.45 | 15480 | 379 |
| 8604-3 2 | 770 269 | 17.2 | 113.5 | 11700 | 1.13 | 25.6 | 9550 | 7.21 | 8.59 | 674 | 1.42 | 1430 | 0.43 | 213 | 70500 | 256 | 0.21 | 99.5 | 0.39 | 14860 | 132 |
| 8604 - 4 2 | 390 195 | 11.4 | 23.2 | 0966 | 0.8 | 21.8 | 9220 | 7.28 | 8.88 | 692 | 0.99 | 750 | 0.34 | 217 | 73700 | 273 | 0.14 | 98.2 | 0.33 | 12950 | 145 |
| 8604-5 2 | 940 287 | 2.01 | 24 | 19500 | 0.85 | 2.62 | 11490 | 60.8 | 911.9 | 937 | 1.05 | 0811 | 0.26 | 253 | 8/300 | 344 | 0.14 | 110 | 0.29 | 15780 | 145 |
| C 0-+000 | 707 090 | 1.01 | 6000 | 0000 | 1 00 | 1.62 | 0006 | 10.0 | 0.11 | 1016 | 07.1 | 071 | 60.0 | 117 | 00/06 | 100 | CT.0 | 101 | 210 | 14600 | 122 |
| 8604-8 3 | 320 289 | 3.8 | 30.8 | 15520 | 0.87 | 25.7 | 11090 | 8.17 | 11.6 | 871 | 0.86 | 1440 | 0.21 | 250 | 82400 | 321 | 0.16 | 94.9 | 0.22 | 15460 | 141 |
| 8604-9 3 | 080 270 | 4.8 | 11.7 | 13150 | 0.74 | 18.4 | 8000 | 8.17 | 10.1 | 787 | 0.91 | 652 | 0.18 | 248 | 80600 | 314 | 0.26 | 96.2 | 0.36 | 14660 | 224 |
| 8604 - 10 3 | 470 246 | 2.8 | 25.8 | 13200 | 0.88 | 20.5 | 7950 | 9.04 | 12.4 | 856 | 0.9 | 940 | 0.23 | 299 | 97000 | 358 | 0.23 | 116 | 0.19 | 15700 | 256 |
| 8579 - 1 58 | 0000 5900 | 1000 | 37200 | 341000 | 48 | 191 | 3640 | 146 | 26.3 | 135 | 9.1 | 204 | 5.0 | 0.62 | 730 | 2.8 | -1.2 | 0.8 | 11.4 | 228 | 12.1 |
| 8579-2 52 | 0000 5700 | 880 | 37600 | 313000 | 35.3 | 171 | 4500 | 135 | 29.9 | 101 | 5.2 | 215 | 8.8 | 1.15 | 99 | L.T | 0.4 | 0.7 | 26 | 181 | 9.8 |
| 8579-3 87 | 0000 11900 | 1060 | 50800 | 318000 | 63 | 291 | 0609 | 206 | 38 | 138 | 9.5 | 370 | 7.9 | 2.0 | 380 | 48.0 | -1.5 | 2.7 | 36.4 | 208 | 8.2 |
| 8579-4 67 | 0000 9400 | 770 | 44000 | 318000 | 61 | 317 | 6100 | 155 | 29 | 107 | -1.4 | 209 | 9.4 | 1.02 | 54 | 2.6 | -0.2 | -0.01 | 25.3 | 204 | 8.5 |
| 8579-5 83 | 0066 0000 | 1030 | 44000 | 269000 | 67 | 280 | 5900 | 232 | 43 | 147 | 6.1 | 291 | 8.3 | 1.36 | 150 | 2.5 | -5.3 | -0.08 | 37.1 | 172 | 5.81 |
| 8579 - 6 82 | 0000 8600 | 820 | 52000 | 340000 | 39.6 | 217 | 6700 | 158 | 37 | 136 | 7.1 | 203 | 9.8 | 0.94 | 54 | 2.4 | 0.5 | -0.03 | 31.8 | 204 | 9.9 |
| 8579 - 7 71 | 0000 12900 | 1720 | 32300 | 460000 | 131 | 410 | 10300 | 376 | 40 | 168 | 8.7 | 204 | 1.61 | 2.19 | 126 | 3.5 | 6.9 | -0.01 | 41 | 311 | 8.4 |
| 8579-8 79 | 000/ 0000 | 890 | 34600 | 133000 | 73 | 185 | 5780 | 114 | 28 | 135 | 4.5 | 262 | 9.3 | 0.88 | 58 | 9.9 | 1.7 | 0.14 | 23.8 | 198 | 6.7 |
| 8579-9 40 40 | 0000 11000 | 020 | 15700 | 136000 | 50 | 148 | 4000 | 78 | 30 | 101 | 2.0 | 125 | 6.8 | 0.84 | 44 | 1.9 | -0.4 | 0.22 | 14.8 | 677 | 4.5 |
| CL 01-6/00 | 0000 T 1000 | 1/01 | nn/ct | NNNOCT | nc | 740 | 0070 | ŧ | 74 | IUI | 1.0 | Iou | 0.0 | 0.40 | C.04 | 0.0 | 17 | 70.0- | 1.07 | 101 | 1.4 |

| Y X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X X | - continued | | 1 | | 3 | | | | ; | 1 | , | , | | | | | | | | 1 | | |
|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|--------|---------------|-------|------------------|------------------|-----------|----------------|-------|--------|--------|--------|--------|-------------|-----------------|--------|--------|--------|--------|-------|---------|--------|
| Mit Mit <th></th> <th>Ste</th> <th>2Cr</th> <th>uWee</th> <th>^{oo}Fe</th> <th>00₆₆</th> <th>iNue</th> <th>uZoo</th> <th>''Ga</th> <th>"Ge</th> <th>SAC</th> <th>oWcs</th> <th>aP/01</th> <th>POm</th> <th>Щ_{сп}</th> <th>uSsu</th> <th>4S121</th> <th>PTcu .</th> <th>nY/61</th> <th>BH707</th> <th>qdenz</th> <th>iBin</th> | | Ste | 2Cr | uWee | ^{oo} Fe | 00 ₆₆ | iNue | uZoo | ''Ga | "Ge | SAC | oWcs | aP/01 | POm | Щ _{сп} | uSsu | 4S121 | PTcu . | nY/61 | BH707 | qdenz | iBin |
| 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | | MBH 69 | MBH 69 | MASSI | MBH 66 | MBH 69 | 69 HBH 69 | 001 100 | MASSI | MBH 66 | MBH 69 | MASSI | MBH 69 | MBH 69 | MBH 69 | MBH 72 | MBH 69 | MBH 69 | MBH 66 | MASSI | 09 HBM | MBH 66 |
| 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | - | 290 | 52 | 68 | 0269 | 64.0 | 1.0 | 129 | 1.9 | 0.00 | 10.0 | 86.0 | 484 | 1.14 | 0.0 | 17 | 1.8 | 2.4 | 0.02 | 3.0 | 37.2 | 2.0 |
| 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | 807 | 5.6 | 671 | 0667 | 0.34 | 6.0 | 16 | 4.23 | 0.1 | 1.1 | 10.0 | 1/0 | C0.0 | 70.0 | 4.1 | 10.0 | 16.0 | 10.0 | 1.1 | 17 | 0.18 |
| 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | 100 | 0.9 | 191 | 0047 | 4C.U | 0.0 | 171 | 20.0 | -0.02 | 10.2 | 67.0 | 107 | 0.11 2.1 | 10.0 | 10.0 | 14 | 6T'0 | 10.0 | 0.0 | 1.02 | 0.40 |
| 110 111 100 111 101 111 101 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 111 <td></td> <td>168</td> <td>14.3</td> <td>121</td> <td>5200</td> <td>0.58</td> <td>5.1</td> <td>114</td> <td>83</td> <td>0.91</td> <td>23</td> <td>0.86</td> <td>430</td> <td>0.15</td> <td>0.02</td> <td>5.8</td> <td>0.54</td> <td>0.7</td> <td>0.02</td> <td>4.1</td> <td>47</td> <td>423</td> | | 168 | 14.3 | 121 | 5200 | 0.58 | 5.1 | 114 | 83 | 0.91 | 23 | 0.86 | 430 | 0.15 | 0.02 | 5.8 | 0.54 | 0.7 | 0.02 | 4.1 | 47 | 423 |
| 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 | 1142 | 19.8 | 113 | 10280 | 2.41 | 7.5 | 480 | 27.2 | 6.3 | 37 | 3.8 | 630 | 7.2 | 7.5 | 83 | 5.1 | 2.3 | 1.4 | 17 | 133 | 8.7 |
| 0 113 113 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 | 0 | 428 | 2.45 | 93.9 | 1560 | 1.37 | 3.28 | 29.1 | 3.06 | 0.9 | 4.3 | 0.07 | 100 | 0.21 | 0.04 | 2.3 | 0.15 | 0.16 | 0.01 | 0.51 | 10.4 | 0.85 |
| 13 11 31 700 21 34 11 31 24 24 24 14 11 31 34 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 14 | 0 | 463 | 0.9 | 131.9 | 1050 | 0.91 | 1.3 | 28 | 1.84 | 0.57 | 3.43 | 0.08 | 76 | 0.17 | 0 | 1.1 | 0.58 | -0.04 | 0 | 0.55 | 8.1 | 1.42 |
| 13 11 54 540 101 131 141 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 131 | 8 | 612 | 19.9 | 123 | 7800 | 2.2 | 5.9 | 420 | 12.1 | 3.1 | 23 | 2.2 | 1040 | 1.2 | 6.4 | 35 | 2.2 | 1.2 | 0.14 | 8.4 | 170 | 3.1 |
| 9 11 14 01 125 14 01 125 14 01 125 14 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 0 | 00 | 1238 | 21.1 | 540 | 7400 | 0.91 | 10.3 | 134 | 17.1 | -0.8 | 19 | 1.21 | 649 | 0.55 | 0.08 | 1.7 | 0.69 | -0.27 | 0.02 | 3.82 | 60.3 | 2.13 |
| 14 51 61 70 01 14 51 00 13 15 00 01 13 15 00 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01< | 0 | 66 | 11.5 | 194 | 1440 | 0.1 | 1.26 | 311 | 0.97 | 0.19 | 8.47 | 0.11 | 280 | 0.58 | 0.02 | 1.39 | 0.18 | 0.1 | 0.01 | 0.42 | 2.9 | 0.22 |
| 18 4.1 3.3 190 0.13 7.03 1.3 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03< | 0 | 144 | 5.8 | 61 | 580 | 0.08 | 1.18 | 160 | 0.39 | 0.3 | 5.5 | 0.23 | 144 | 0.3 | 0 | 0.69 | 0.15 | 0.03 | 0 | 0.32 | 0.59 | 0.27 |
| 0 19 3 1 3 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 00 | 194 | 4.4 | 36.3 | 1400 | 0.13 | 0.76 | 173 | 0.38 | 0.25 | 4.43 | 0.27 | 71.2 | 0.27 | 0 | 6.0 | 0.06 | 0.15 | 0.02 | 0.4 | 1.01 | 0.07 |
| 0 121 77 160 170 0.14 170 0.14 170 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 0.14 | 00 | 149 | 3.9 | 32 | 152 | 0.02 | 0.74 | 156 | 0.34 | 0.11 | 3.77 | 0.15 | 186 | 0.31 | 0 | 0.48 | 0.05 | -0.03 | 0 | 0.16 | 0.68 | 0.06 |
| 0 13 57 113 860 0.03 271 360 0.33 0.34 0.3 0.01 1.3 0.06 0.13 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 <th0.03< th=""> <th0.03< th=""> <th0.03< th=""> <</th0.03<></th0.03<></th0.03<> | 00 | 221 | L.L | 430 | 1730 | 0.14 | 3.06 | 321 | 1.61 | 0.28 | 10.7 | 0.28 | 168 | 0.58 | 0.01 | 1.31 | 0.19 | 0.01 | 0.02 | 0.55 | 2.2 | 0.11 |
| 0 1 2 5 5 5 6 1 7 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 00 | 143 | 6.7 | 113 | 860 | 0.09 | 2.7 | 306 | 0.56 | 0.44 | 7.4 | -0.01 | 188 | 0.33 | 0.01 | 1.8 | 0.08 | 0.15 | 0.02 | 0.56 | 0.95 | 0.24 |
| 0 10 410 10 410 100 410 100 410 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 | 000 | 199 | 5 | 95 | 560 | 0.1 | 2.77 | 180 | 0.59 | 0.34 | 5.01 | 0.08 | 193 | 0.37 | 0.01 | 0.72 | 0.12 | 0.18 | 0.06 | 0.37 | 1.32 | 0.11 |
| 14 127 781 190 0.64 153 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35 <th0.35< th=""> 0.35 0.35<!--</td--><td>001</td><td>240</td><td>10</td><td>410</td><td>3510</td><td>0.55</td><td>7.61</td><td>338</td><td>1.28</td><td>0.59</td><td>7.8</td><td>0.26</td><td>398</td><td>0.54</td><td>0.01</td><td>1.25</td><td>0.12</td><td>0.03</td><td>0.01</td><td>0.22</td><td>1.35</td><td>0.06</td></th0.35<> | 001 | 240 | 10 | 410 | 3510 | 0.55 | 7.61 | 338 | 1.28 | 0.59 | 7.8 | 0.26 | 398 | 0.54 | 0.01 | 1.25 | 0.12 | 0.03 | 0.01 | 0.22 | 1.35 | 0.06 |
| 00 280 727 380 4100 11 11 350 137 410 11 11 350 323 410 13 211 610 32 323 131 131 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 213 | 000 | 344 | 12.7 | 781 | 1930 | 0.46 | 15.8 | 657 | 2.58 | 0.81 | 15.8 | 0.33 | 168 | 1.26 | 0.01 | 1.74 | 0.13 | 60.0 | 0.02 | 0.42 | 1.18 | 0.05 |
| 00 305 177 400 313 211 201 205 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 | 800 | 280 | 27.9 | 352 | 4120 | 1.2 | 1.11 | 362 | 1.35 | 0.45 | 22.1 | 0.47 | 210 | 0.44 | 0.01 | 0.65 | 0.17 | -0.1 | 0.01 | 0.5 | 2.22 | 0.11 |
| 00 810 7700 781 313 700 114 408 256 0.08 114 115 0.08 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 | 000 | 365 | 17.7 | 4800 | 44600 | 3.13 | 22.1 | 651 | 20.5 | 3.53 | 41.2 | 0.92 | 367 | 1.95 | 0.14 | 13 | 1.9 | 0.16 | 0.05 | 1.9 | 29.9 | 0.78 |
| 00 1210 230 1700 74 443 119 219 230 114 123 234 104 100 433 134 133 334 134 133 334 134 133 334 134 133 334 134 133 134 134 133 134 134 133 134 134 133 134 134 133 134 134 133 134 134 133 134 134 133 134 134 133 134 134 133 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 <td>000</td> <td>830</td> <td>24.7</td> <td>5440</td> <td>67700</td> <td>5.81</td> <td>36.3</td> <td>910</td> <td>29.9</td> <td>8.3</td> <td>017</td> <td>1.14</td> <td>408</td> <td>2.56</td> <td>0.08</td> <td>14</td> <td>0.86</td> <td>0.32</td> <td>0.02</td> <td>2.98</td> <td>33.3</td> <td>0.86</td> | 000 | 830 | 24.7 | 5440 | 67700 | 5.81 | 36.3 | 910 | 29.9 | 8.3 | 017 | 1.14 | 408 | 2.56 | 0.08 | 14 | 0.86 | 0.32 | 0.02 | 2.98 | 33.3 | 0.86 |
| 00 150 250 7700 88 771 100 125 036 035 035 234 123 00 150 150 150 150 150 150 150 150 150 151 150 151 150 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 151 | 000 | 1210 | 26.9 | 8300 | 77000 | 7.4 | 40.8 | 1190 | 30.1 | 5.7 | 50.1 | 1.6 | 309 | 2.99 | 0.14 | 18 | 1.38 | 0.43 | 0.00 | 4.35 | 30.4 | 1.23 |
| 00 66 1/4 279 3200 4/4 279 320 4/4 279 320 4/4 279 320 4/4 279 320 4/4 279 320 4/3 7/1 320 4/3 7/1 320 4/3 7/1 320 1/4 2/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 1/3 | 000 | 1300 | 23.0 | 5620 | 70700 | 8.8 | 47.1 | 1060 | 29 | 6.8 | 35.6 | 1.66 | 167 | 4.4 | 60'0 | 11.6 | 0.86 | 0.16 | 0.03 | 3.52 | 24.4 | 1.23 |
| 00 55 59 60 700 0.05 67 345 479 137 136 014 20 022 014 20 023 011 010 023 111 010 023 111 010 023 101 101 010 023 111 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 011 | 000 | 686 | 14.6 | 4790 | 38200 | 4.04 | 22.9 | 646 | 17.4 | 3.78 | 32.6 | 1.12 | 560 | 2.2 | 0.07 | 7.22 | 0.56 | 0.25 | 0 | 2.32 | 19.3 | 0.64 |
| 00 13 11 71 013 13 14 010 013 01 17 010 013 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 </td <td>000</td> <td>565</td> <td>5.59</td> <td>630</td> <td>7800</td> <td>0.75</td> <td>6.7</td> <td>245</td> <td>4.79</td> <td>1.87</td> <td>15.6</td> <td>0.18</td> <td>102</td> <td>2.2</td> <td>0.04</td> <td>2.0</td> <td>0.22</td> <td>0.21</td> <td>0</td> <td>1.47</td> <td>4.71</td> <td>0.67</td> | 000 | 565 | 5.59 | 630 | 7800 | 0.75 | 6.7 | 245 | 4.79 | 1.87 | 15.6 | 0.18 | 102 | 2.2 | 0.04 | 2.0 | 0.22 | 0.21 | 0 | 1.47 | 4.71 | 0.67 |
| 0 251 134 104 610 137 938 101 517 014 23 017 004 93 137 013 033 031 0101 933 137 011 033 031 0101 933 137 011 033 031 031 931 031 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 931 | 00 | 195 | 1.01 | 11 | 910 | 0.05 | 0.57 | 45.4 | 0.64 | 0.34 | 7.1 | 0.23 | 191 | 0.13 | 0 | 0.4 | 0.08 | 0.1 | 0 | 0.72 | 1.14 | 0.08 |
| 200 200 200 1500 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 <td>8</td> <td>251</td> <td>1.34</td> <td>104</td> <td>610</td> <td>0.19</td> <td>0.82</td> <td>103</td> <td>0.93</td> <td>1.01</td> <td>12.1</td> <td>0.31</td> <td>220</td> <td>0.2</td> <td>0.06</td> <td>1.5</td> <td>2.3</td> <td>0.17</td> <td>0.04</td> <td>0.95</td> <td>1.6</td> <td>0.12</td> | 8 | 251 | 1.34 | 104 | 610 | 0.19 | 0.82 | 103 | 0.93 | 1.01 | 12.1 | 0.31 | 220 | 0.2 | 0.06 | 1.5 | 2.3 | 0.17 | 0.04 | 0.95 | 1.6 | 0.12 |
| 00 -000 460 1000 460 1000 500 100 100 100 100 100 100 100 100 100 100 100 100 200 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 | 000 | 2620 | 39.8 | 13700 | 155000 | 13.7 | 94.3 | 2540 | 2 8 | 18.8 | 76 | 1.87 | 240 | 1.1 | 0.26 | 36.4 | 1.39 | 0.51 | 10.0 | 6 | 23 | 2.7 |
| $ \begin{array}{{ccccccccccccccccccccccccccccccccccc$ | 000 | 4010 | 48.4 | 20900 | 174000 | 18.5 | 105 | 3030 | 82 | 16.1 | 83.1 | 3.4 | 165 | 9.9 | 0.38 | 62.5 | 1.67 | 0.7 | 0.06 | 10.4 | 65 | 2.51 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 000 | -30000 | 24000 | 7000 | 230000 | 240 | 2/00 | 4/000 59000 | 200 | 70000 | 34000 | -1000 | 2300 | 001- | 2400 | 00025 | 2500 | 1000 | 0/11 | 000 | 148000 | 510 |
| | | 000- | 0001 | 840 | 28000 | 0007- | 007- | 30300 | 110 | 2000 | 1000 | -50 | 00000 | 41 | 58 | 0007/ | 256 | 140 | 54 | 140 | 0001051 | 208 |
| 0 211 103 333 2890 0.44 1.50 4890 19 0.8 2160 0.39 59.6 47.0 255 6.80 74.20 0.28 4940 833 00 231 101 2490 0.44 1.50 0.39 2330 0.13 2970 0.75 6.80 74.20 0.28 4940 831 00 318 0.53 50 0.39 236 0.13 2970 0.75 173 190 137 960 393 144 0.35 144 144 133 144 144 144 133 114 144 044 147 146 143 133 114 144 044 147 146 143 143 133 114 144 144 133 114 144 044 6470 235 040 83 2400 147 140 144 144 144 143 133 114 </td <td>000</td> <td>000009</td> <td>12000</td> <td>50000</td> <td>265000</td> <td>4400</td> <td>-10000</td> <td>15000</td> <td>-2200</td> <td>-12000</td> <td>19000</td> <td>-20000</td> <td>0009</td> <td>300</td> <td>300</td> <td>39000</td> <td>1100</td> <td>-6300</td> <td>710</td> <td>3500</td> <td>57000</td> <td>930</td> | 000 | 000009 | 12000 | 50000 | 265000 | 4400 | -10000 | 15000 | -2200 | -12000 | 19000 | -20000 | 0009 | 300 | 300 | 39000 | 1100 | -6300 | 710 | 3500 | 57000 | 930 |
| 0 241 0.15 10.1 249 0.43 277 400 2.99 0.31 197 56 0.36 197 56 0.36 1097 56 0.36 1097 56 0.36 1097 56 0.36 1097 56 0.37 300 440 36 173 50 373 123 114 1030 343 133 037 037 300 450 146 119 4700 247 610 314 133 114 0100 347 133 134 037 300 450 146 113 314 133 114 610 375 135 037 037 037 134 133 134 133 134 133 134 640 135 134 640 135 137 144 640 135 137 134 641 643 653 133 027 133 027 133 133 | 60 | 231 | 1.03 | 33.3 | 2890 | 0.44 | 1.50 | 4690 | 1.9 | 0.8 | 2180 | 0.57 | 1650 | 0.39 | 59.6 | 4740 | 255 | 6.80 | 74.20 | 0.28 | 4940 | 88.3 |
| 00 192 092 51 4210 0.48 59 0.77 240 0.13 2970 0.75 90 710 379 122 114 135 090 450 00 386 0.77 550 10710 0.77 123 113 114 135 040 341 133 114 640 139 057 057 050 450 070 155 173 116 8510 341 133 134 640 139 057 057 159 050 450 070 053 173 116 8510 427 73 137 134 647 070 237 039 137 049 700 139 027 037 039 053 143 173 116 8510 427 73 027 021 027 021 027 021 027 021 027 021 027 021 027 026 | 50 | 241 | 0.15 | 10.1 | 2490 | 0.43 | 2.77 | 4000 | 2.09 | 0.39 | 2330 | 0.16 | 1423 | 0.29 | 77.8 | 6610 | 301 | 19.7 | 96 | 0.36 | 10500 | 140 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 50 | 192 | 0.92 | 51 | 4210 | 0.48 | 5.9 | 6330 | 2.29 | 0.77 | 2420 | 0.13 | 2970 | 0.75 | 90 | 7110 | 379 | 122 | 114 | 1.35 | 0606 | 450 |
| 00 356 1.77 569 1071 0.77 123 15340 4.61 1.19 570 0.22 2400 131 9400 334 133 114 0.44 64700 233 0 273 1.31 1.31 1.31 1.31 1.33 1.31 1.33 1.33 1.33 1.33 1.33 0.05 3.5 4500 1.39 0.33 1.00 1.33 0.35 4500 1.39 0.33 0.06 3.59 1.35 0.25 4500 1.39 0.33 0.06 3.59 1.35 0.25 0.01 0.03 0.06 3.59 1.35 0.25 0.35 0.01 0.05 0.35 8.3 0.05 0.35 0.05 0.35 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 | 8 | 308 | 0.53 | 50 | 5490 | 0.63 | 9.3 | 11800 | 2.63 | 0.4 | 4730 | 0.55 | 1489 | 1.71 | 140 | 10300 | 343 | 5.53 | 135 | 0.37 | 32400 | 166 |
| $ \begin{array}{ ccccccccccccccccccccccccccccccccccc$ | 8 | 356 | 1.77 | 56.9 | 10710 | 0.77 | 12.3 | 15340 | 4.61 | 1.19 | 5970 | 0.2 | 2400 | 1.99 | 131 | 9400 | 334 | 13.3 | 114 | 0.44 | 64700 | 243 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 00 | 299 | 0.31 | 25.9 | 3510 | 0.55 | 00 | 12500 | 6.62 | 11 | 4870 | 0.44 | 1233 | 1.73 | 116 | 8510 | 422 | 7.8 | 120 | 0.25 | 45600 | 139 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 8 : | C'/8 | 0C.I | 01 | 1200 | 0.08 | 80.0 | 45.5 | 1.79 | 0.11 | 14.8 | 0.3 | 3900 | 0.03 | 60.0 | | 60.0 | 7.0 | 0.00 | 3.52 | 8.3 | 17.0 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 8 8 | 130 | 61.1 1 0 1 | 5.5 | 294 | c1.0 | 0.TO | 4.00 | 1.22 | 00.0- | 1.1 | 70.0- | 3320 | 10.0- | c0.0 | CO.0 | 21.0 | 0.33 | 00.0 | 4C.C | C6.1 | 50.0 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 0.00 | 54.3 | 1.24 | 1.1 | 080 | - | 6/.0 | 0.05 | 1.55 | 67.0 | 1.21 | 65.0 | 0664 | 51.0 | 06.0 | 1.0/ | CT.0 | 01.0 | c1.0 | 3.81 | 7.0 | 00.0 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 3 5 | 81.4 | 080 | | 0/5 | 1.0 | 17.1 | 2010 | 02.0 | 47.0 | 4.6 | 10.14 | 1620 | CT-0 | 50.0 | 4710 | 12.0 | 000 | 10.0 | 3 8 6 | 1.0 | 10.0 |
| 0 418 0.89 1.89 1.03 0.13 0.51 0.56 1.14 0.50 0.02 0.01 0.13 0.13 0.11 0.13 0.11 0.13 0.11 0.13 0.11 0.13 0.11 0.13 0.11 0.13 0.11 0.13 0.11 0.13 0.13 0.11 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.13 0.14 0.13 0.14 0.13 0.13 0.13 0.13 0.14 0.13 0.14 0.13 0.14 0.13 0.14 0.13 0.14 0.13 0.14 0.13 0.14 0.13 0.14 0.13 0.14 0.13 0.14 0.15 0.14 0.15 0.14 0.13 0.14 0.13 0.14 0.15 0.14 0.15 0.14 0.11 0.15 0.14 0.11 0.15 0.1 | 2 2 | 116 | 0.00 | 4 × | 717 | 24.0 | 01.0 | C. CI | 0.17 | 0.44 | 0.0 | 41.0 | 0767 | 1.0 | 00.0 | 0.16 | 10.0 | 60.0 | 500 | 2000 | 47 | 00.0 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 3 5 | 011 | 0.80 | 1 80 | 108 | 0.14 | CI.0 | 7.01 | 15.0 | 110 | 4.1 | 70.14 | 10500 | 7.0 | 10.0- | 01.0 | 20.0 | 0.18 | 10.0 | 4.60 | 80.0 | 0.01 |
| 00 658 227 82 450 062 055 80 1.19 0.4 203 0.34 2290 0.13 3.2 18 0.07 0.13 0.05 3.44 6.7 0.01 00 575 0.76 3.28 190 -0.02 0.29 13.1 0.65 0.43 6.15 0.29 7800 0.03 0 0.42 0.01 0.09 0 7.7 0.88 0.02 | 2 0 | 66.0 | 0.74 | 2.37 | 130 | 0.04 | 0.22 | 11.2 | 0.41 | 0.21 | 4.84 | 0.12 | 4880 | 0.01 | 0 0 | 0.59 | 0.01 | 0.13 | 0 | 2.57 | 3.6 | 10.0 |
| 00 575 0.76 3.28 190 -0.02 0.29 13.1 0.65 0.43 6.15 0.29 7800 0.03 0 0.42 0.01 0.09 0 7.7 0.88 0.02 | 00 | 65.8 | 2.27 | 8.2 | 450 | 0.62 | 0.55 | 80 | 1.19 | 0.4 | 20.3 | 0.34 | 2290 | 0.13 | 3.2 | 18 | 0.07 | 0.13 | 0.05 | 3.44 | 6.7 | 0.01 |
| | 8 | 57.5 | 0.76 | 3.28 | 190 | -0.02 | 0.29 | 13.1 | 0.65 | 0.43 | 6.15 | 0.29 | 7800 | 0.03 | 0 | 0.42 | 0.01 | 0.09 | 0 | 7.7 | 0.88 | 0.02 |

| | 209Bi | 201 | 318 | 144 | 83 | 211 | 140 | 264 | 137 | 171 | 263 | 127 | 275 | 124 | 467 | 202 | 9CI 93 | 80 | 100 | 12 | 0.24 | 0.71 | 0.1 | 0.1 | 0.11 | 0.04 | 1.1 | 0.14 | 3.8 | 1.7 | 0.09 | 0.05 | 19 | 0.67 | 1.53 | 6.03 | 1.25 | 0.05 | 0.02 | 0.01 | 0.08 | 0.05 | 0.06 | 0.08 | 1.0 | |
|-------------|----------------------------|----------|----------|----------|----------|----------|----------|--------|----------|-----------|----------|----------|----------|----------|----------|----------|-----------|--------|-----------|----------|--------|----------|----------|----------|----------|----------|----------|----------|-----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--------------|--|
| | 208Pb | 11100 | 11100 | 5900 | 10200 | 7800 | 8000 | 11250 | 0066 | 5210 | 8600 | 4210 | 3610 | 4110 | 4540 | 4940 | 2740 | 0102 | 3190 | 5.2 | 1 | 33.6 | 1.99 | 0.91 | 0.26 | 0.22 | 3.13 | 4.51 | 1.52 | 137 | 10.8 | 1 08 | 171 | 98 | 40.6 | 108 | 500 | 1.92 | 1.45 | 0.64 | 1.12 | 1.13 | 1.03 | 1.17 | 0.34 | |
| | BH202 | 0.39 | 0.71 | 0.39 | 0.45 | 0.47 | 10.04 | 0.39 | 0.48 | 0.46 | 0.77 | 0.4 | 0.37 | 0.55 | 0.65 | 0.68 | 6/.0 | 12.0 | 0.67 | 0.52 | 1.03 | 3 | 0.47 | 0.31 | 0.23 | 0.12 | 0.65 | 0.17 | 0.27 | 58 | 2.59 | 1 17 | 0.98 | 0.9 | 0.84 | 1.49 | 0.68 | 0.33 | 0.76 | 0.55 | 0.68 | 0.71 | 0.75 | 0.63 | 0.31 | |
| | ¹⁹⁷ Au | 145 | 112 | 121 | 93.4 | 103 | 96 | 136 | 154 | 104 | 190 | 115 | 89 | 101.1 | 89.2 | 115 | 123 | 6.03 | 7.60 | 0.02 | 0.04 | 0.04 | 0 | 0 | 0 | 0 | 0.02 | 0.01 | 0.01 | 0.63 | 0.06 | 10.0- | 1.12 | 0.53 | 0.15 | 0.86 | 0.95 | -0.01 | 0 | 0 | 0.01 | 0.01 | 0 | 0 | 10.0 | |
| | 125Te | 5.9 | 7.5 | 5.4 | 10 | 53 | 16.7 | 6.8 | 6.7 | 3.63 | 2.29 | 1.07 | 3.7 | 3.7 | 6.2 | 2.45 | 2.36 | 74.1 | 10.0 | 0.04 | 0.09 | 0.24 | -0.07 | 0.03 | 0 | 0.04 | 0 | 0.02 | 0.18 | 4 | 1.02 | 10.48 | 0.61 | 1.38 | 0.15 | 0.92 | 0.24 | 0.7 | 0.15 | 0.12 | 0.04 | 10.0 | 0.02 | 0.02 | 10.0 | |
| | 121Sb | 455 | 377 | 361 | 331 | 337 | 100 | 486 | 451 | 374 | 571 | 413 | 336 | 288 | 369 | 368 | 412 | 107 | 250 | 0.11 | 0.42 | 3.4 | 0.12 | 0.3 | 0.09 | 0.05 | 0.1 | 0.11 | 0.02 | 1.9 | 0.48 | 0.08 | 2.29 | 1.47 | 0.79 | 2.63 | 2.72 | 0.23 | 0.03 | 0.07 | 0.01 | 0.1 | 0.08 | 60.0 | 0.12 | |
| | MRH 77 | 5530 | 4720 | 5700 | 3940 | 3610 | 3370 | 5360 | 4810 | 3630 | 5260 | 3770 | 2820 | 2930 | 2960 | 3280 | 2010 | 01/27 | 2300 | 0.58 | 10.5 | 14.4 | 0.6 | 0.71 | 0.27 | 0.22 | 0.86 | 5.6 | - | 81 | 1.27 | 1 07 | 41.4 | 23.7 | 13.6 | 38.7 | 52 | 1.47 | 0.36 | 0.31 | 0.94 | 0.38 | 0.43 | 5.0 | co.u 0.32 | |
| | 115 In MRH 60 | 94 | 83.7 | 106 | 78.5 | 74.8 | CI CI | 112.7 | 119.4 | 81 | 149 | 95 | 99 | 75.1 | 76 | 86.4 | 5 5 | 0.05 | 48.8 | 0 | 0.13 | 66.0 | 0.02 | 0.26 | 0 | 0 | 0 | 0.03 | 0.01 | 1.57 | 0.04 | 10.0 | 0.54 | 0.56 | 0.24 | 0.67 | 0.77 | 0.03 | 0.01 | 0.01 | 0 | 0 | 0 | 0 | 10.0 | |
| | III Cd | 1.08 | 2.9 | 0.46 | 1.04 | 1.49 | 60.0 | 5.1 | 0.55 | 0.69 | 1.55 | 0.67 | 0.87 | 0.37 | 11.2 | 1.22 | 0.73 | 11 | 1.72 | 0.54 | 2.18 | 7.5 | 1.2 | 0.63 | 0.1 | -0.02 | 1.99 | 1.04 | 0.02 | -7 | 0.92 | 0.38 | 0.9 | 0.54 | 69.0 | 1.78 | 0.41 | 0.14 | 0.07 | 0.02 | 0.17 | 0.04 | 0.07 | -0.02 | CT.0 | |
| | 107 Ag | 2350 | 2920 | 2510 | 2150 | 2300 | 1610 | 1740 | 2960 | 1986 | 1670 | 1610 | 1840 | 1490 | 1870 | 1510 | 1905 | 0001 | 1820 | 30.4 | 38 | 152 | 14.8 | 17 | 8.9 | 6.3 | 12.3 | 4.6 | 11.5 | 117 | 220 | 001 8 | 89 | 69 | 140 | 202 | 56.8 | 107 | 294 | 294 | 459 | 488 | 699 | 087 | 98.5 | |
| | OM ²⁶ | 0.23 | 0.14 | 0.24 | 0.18 | 10.0 | 0.17 | -0.03 | 0.58 | 0.19 | 0.1 | -0.01 | -0.01 | 0.37 | 0.36 | 0.2 | 1.0 | 0.04 | 10.0 | 0.02 | 0.76 | 2.9 | 0.18 | 0.17 | 0.18 | 0.1 | 0.21 | 0.27 | 0.08 | en j | 0.32 | 0.13 | 0.4 | 0.26 | 0.28 | 1.39 | 0.28 | -0.13 | 0.13 | 0.15 | 0.11 | -0.02 | 0.04 | 0.19 | 0.1 | |
| | 75AS | 2120 | 1790 | 1490 | 1630 | 1370 | 0117 | 3250 | 2000 | 1760 | 1570 | 1220 | 1132 | 1170 | 1120 | 2120 | 1480 | 111 | 758 | 7.40 | 31.4 | 78 | 10.6 | 5.86 | 2 | 0.94 | 13.4 | 8.25 | 12 | 38 | 27.1 | 0.66 | 18.2 | 16.4 | 11.4 | 32.7 | 24.5 | 0.7 | 1.31 | 1.14 | 1.26 | 1.8 | 1.35 | cl.1 | 0.93 | |
| | ⁷² Ge | 0.83 | 0.69 | 1.62 | 0.66 | 0.56 | C+-0 | 1.76 | 1.01 | 0.8 | 0.73 | 1.41 | 0.93 | 0.54 | 0.99 | 0.87 | 0.49 | 2.0 | 0.59 | 0.3 | 7.4 | 54 | 1.64 | 0.59 | 0.01 | -0.4 | 3.7 | 0.64 | -0.27 | -51 | -0.1 | 1.1 | 2.8 | 9.0 | -0.6 | 3.0 | -0.43 | -0.8 | 0.2 | 0.04 | 0.94 | -0.09 | 0.5 | 10.0 | 77.0 | |
| | 71Ga | 2.61 | 2.36 | 2.64 | 2.12 | 1.55 | 10.1 | 3.53 | 4.1 | 2.9 | 4.13 | 3.05 | 2.25 | 1.76 | 1.54 | 1.58 | 2.52 | 2 21 | 102 | 0.81 | 46.6 | 61 | 17.8 | 0.61 | 0.27 | 0.12 | 44.8 | 3.52 | 0.14 | 4 | 3.46 | 10.1 | 3.80 | 0.62 | 2.49 | 11.50 | 2.86 | 0.04 | 0.15 | -0.02 | 0.30 | 0.16 | 0.11 | 60.0 | 10.08 | |
| | 66Zn | 12320 | 10410 | 8300 | 12660 | 15550 | 1420 | 11100 | 7460 | 6840 | 6550 | 6230 | 8170 | 5670 | 10900 | 0109 | 9480 | 11660 | 13600 | 373 | 2120 | 2540 | 681 | 700 | 129 | 43 | 1044 | 408 | 45 | 590 | 279 | 00 | 273 | 236 | 209 | 674 | 272 | 7.4 | 42 | 17.2 | 41.3 | 33.4 | 22.8 | 20.6 | 17.1 | |
| | ⁶⁰ Ni MRH 60 | 6.43 | 4.7 | 4.4 | 5.8 | 5.22 | 17.6 | 4.84 | 5.9 | 2.56 | 4.56 | 3.5 | 3.9 | 3.59 | 5.7 | 3.4 | 3.65 | 57 | 1.5 5 | 2.56 | 246 | 1870 | 70.9 | 7.33 | 0.78 | 0.84 | 124 | 12.3 | 0.36 | 170 | 2.3 | 1.6 | 1 | 3.6 | 4.4 | 56.5 | 9.2 | - | 0.19 | -0.25 | 0.38 | -0.31 | 0.51 | 6/.0 | 0.67 | |
| | ³⁹ Co | 0.49 | 0.62 | 0.41 | 0.64 | 0.4 | 0.48 | 0.52 | 0.94 | 0.43 | 0.74 | 0.34 | 0.43 | 0.32 | 0.43 | 0.50 | 0.48 | 05.0 | 50 | 0.28 | 145 | 470 | 40 | 0.28 | 0.1 | -0.03 | 84.8 | 6.7 | 0.16 | - | 0.39 | 0.41 | 1.92 | 0.23 | 0.34 | 28.4 | 0.61 | -0.28 | 0.03 | -0.03 | 0.01 | -0.01 | 0.01 | c0.0 | 70.04 | |
| | ⁵⁶ Fe | 2630 | 2130 | 1720 | 2410 | 1090 | 2100 | 1870 | 3890 | 1400 | 2760 | 1300 | 740 | 750 | 630 | 727 | 210 | 010 | 232 | 620 | 106500 | 377000 | 25130 | 1010 | 170 | 31.4 | 61400 | 4980 | 45 | 4600 | 3310 | 0/6 | 3800 | 1180 | 2480 | 49600 | 3750 | 16 | 79 | 21.4 | 125 | 4 | 42 | 17 | 11.80 | |
| | Mh ⁵⁵ Mh | LL | 10.4 | 21.4 | 58 | 10.1 | 3.5 | 10.6 | 51 | 2.76 | 19 | 4 | 9 | 15 | 9 | x | ٩ ٩ | • = | 1 | 179 | 5100 | 22300 | 1440 | 104 | 25 | 15 | 2610 | 1450 | 33 | 118 | 46.7 | 47 | 134 | 47 | 141 | 812 | 218 | 0.8 | 8.4 | 8.8 | 10.9 | 12.2 | 51 : | 4.2 | 3.9 | |
| | ⁵³ Cr | 1.23 | 1.55 | 0.43 | 1.14 | 1.01 | 950 | 0.7 | 3.0 | 1.68 | 6.0 | 0.3 | 4.7 | 4.1 | 6.3 | 3.1 | -0.60 | 170 | -8.5 | 3.92 | 136 | 11900 | 96.7 | 1.25 | -0.13 | 0.08 | 29.4 | 10.8 | 0.41 | 175 | 14.5 | 1 20 | 3.80 | 7.20 | 5.60 | 15.5 | 5.30 | -0.20 | 0.47 | 0.17 | 0.79 | 0.45 | 0.04 | 0.47 | 0.46 | |
| | 34S | 68.0 | 59.5 | 71.5 | 62.8 | 67.5 | 0.92 | 86.4 | 65.7 | 101 | 93.9 | 115 | 112 | 114 | 117 | 115 | 120 | 122 | 126 | 260 | 1790 | 6300 | 658 | 244 | 228 | 217 | 940 | 273 | 209 | -340 | 183 | 767 | 172 | 123 | 107 | 664 | 127 | 302 | 129 | 153 | 135 | 146 | 142 | 141 | 148 | |
| - continued | ³¹ P | 3120 | 3810 | 1940 | 4730 | 3140 | 1480 | 3470 | 2850 | 1710 | 6400 | 4090 | 3050 | 2700 | 2680 | 3350 | 4500 | 3030 | 1670 | 51200 | 106000 | 95000 | 44500 | 37200 | 10000 | 3900 | 39300 | 25100 | 2880 | 159000 | 111000 | 0096 | 25400 | 27600 | 25100 | 99100 | 12200 | 1014 | 4110 | 2380 | 4210 | 3650 | 2380 | 2260 | 2410 | |
| Appendix A | | 8609 - 1 | 8609 - 2 | 8609 - 3 | 8609 - 4 | 8609 - 5 | 0 - 6009 | 8-0008 | 8609 - 9 | 8609 - 10 | 8605 - 1 | 8605 - 2 | 8605 - 3 | 8605 - 4 | 8605 - 5 | 8605 - 6 | 0 5098 | 0 5098 | 8605 - 10 | 8599 - 1 | 8599-2 | 8599 - 3 | 8599 - 4 | 8599 - 5 | 8599 - 6 | 8599 - 7 | 8599 - 8 | 8599 - 9 | 8599 - 10 | 8597 - 1 | 8597 - 2 | 6 - 1609 | 8597 - 5 | 8597 - 6 | 8597 - 7 | 8597 - 8 | 8597 - 9 | 8597 - 10 | 85914 - 1 | 85914 - 2 | 85914 - 3 | 85914 - 4 | 85914 - 5 | 85914 - 6 | 8-914-8 | |

| Appendix A - c | ontinued | | | | | | | | | | | | | | | | | | | | |
|----------------|-------------------|--------------------------------|---------------------|--------------------|--------|------------------|------------------|-------|------------------|--------|------------------|---------------|--------|--------|-------------------|--------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | ³¹ P 1 | ⁴ S ⁵³ C | r ⁵⁵ Min | 1 ⁵⁶ Fe | 59 Co | iN ⁰⁹ | uZ ⁹⁹ | 71Ga | ⁷² Ge | 75As | oW ⁵⁶ | 107 Ag | 111 Cd | 115Im | ¹¹⁸ Sn | 121Sb | ¹²⁵ Te | ¹⁹⁷ Au | ²⁰² Hg | ²⁰⁸ Pb | ²⁰⁹ Bi |
| MB | H 69 MB. | H 69 MBH | 69 MASS. | 1 MBH 66 | MBH 69 | MBH 69 | MBH 69 | MASSI | MBH 66 | MBH 69 | MASSI | VBH 69 | MBH 69 | MBH 69 | MBH 72 | MBH 69 | MBH 69 | MBH 66 | MASSI | MBH 66 | MBH 66 |
| 8576 - 1 | 730 1 | 53 1.2 | 1 1.21 | 15 | 0.07 | -0.15 | 8.2 | 0.10 | -0.58 | 0.55 | 0.05 | 160 | 0 | 0 | 0.05 | 0.06 | 0 | 0 | 0.39 | 0.05 | 0 |
| 8576-2 | 730 1 | 50 1.0 | 6 4.6 | 54 | 0.04 | 0.51 | 11.7 | 0.37 | 0.32 | 0.77 | 0.26 | 174 | 0.06 | 0 | 0.2 | 0.07 | -0.04 | 0 | 0.35 | 0.21 | 0.01 |
| 8576-3 | 910 1 | 48 0.4 | 1 14 | 17 | 0.06 | 1.03 | 10.9 | 0.18 | 0.13 | 0.97 | 0.16 | 145 | 0 | 0 | 0.19 | 0.08 | -0.02 | 0 | 0.51 | 0.38 | 0.07 |
| 8576-4 | 960 1 | 31 0.9 | 2 23 | 57 | 0.03 | 0.61 | 12.7 | 0.19 | 0.38 | 0.83 | 60.0 | 184 | 0.05 | 0.01 | 0.16 | 0.01 | 0.03 | 0 | 0.33 | 0.13 | 7.6 |
| 8576-5 | 760 1 | 36 0.1 | 9 1.4 | 7 | 0.06 | 0.17 | 8.9 | 0.14 | 0.13 | 0.95 | 0.13 | 268 | -0.04 | 0 | 0.16 | 0.04 | -0.04 | 0 | 0.42 | 0.08 | 0.01 |
| 8576-6 1 | 490 1 | 30 0.2 | 5 7.7 | 106 | 0.01 | 2.79 | 24.7 | 0.02 | -0.09 | 0.78 | 0.17 | 267 | 0.02 | 0 | 1.7 | 0.05 | 0.02 | 0.01 | 0.48 | 0.58 | 0.26 |
| 8576-7 2 | 040 1 | 12 0.3 | 8 55 | 47 | 0.04 | 1.52 | 70 | -0.03 | 0.23 | 0.83 | 0.14 | 193 | 0.08 | 0 | 0.14 | 0.05 | -0.06 | 0 | 0.39 | 0.35 | 0.05 |
| 8576-8 | 650 1 | 15 0.5 | 8 3.4 | 6 | 0.06 | -0.1 | LL | 0.09 | 0.38 | 0.74 | 0.15 | 206 | -0.02 | 0 | 0.01 | 0.01 | -0.01 | 0 | 0.46 | 0.02 | 0 |
| 8576-9 1 | 340 1 | 14 2.0 | 7 15.7 | 141 | 0.14 | 3.3 | 24.8 | 0.10 | 0.46 | 0.51 | 0.15 | 750 | -0.03 | 0 | 0.18 | 0.04 | 0.02 | 0 | 0.58 | 0.24 | 0.01 |
| 8576 - 10 | 860 1 | 19 0.1 | 9 3 | 5 | -0.04 | 0.53 | 12.8 | -0.09 | 0.44 | 0.57 | 0.05 | 215 | 0.18 | -0.01 | 0.01 | 0.03 | 0.06 | 0 | 0.7 | 0.10 | 0 |
| 020-1 2 | 200 1 | 72 0.2 | 2 130 | 3010 | 46.8 | 616 | 450000 | 1.39 | 1.43 | 307 | 0.16 | 1018 | 1.07 | 53.4 | 13100 | 107 | 0.03 | 15.8 | 12.1 | 1690 | 13.6 |
| 020-2 1 | 8000 2 | 36 0.8 | 7 196 | 27000 | 11.3 | 450 | 50800 | 1.67 | 2.57 | 861 | 0.3 | 527 | 0.59 | 142 | 33800 | 499 | 0.03 | 23.6 | 1.85 | 4320 | 30 |
| 020-3 3 | 9200 3 | 24 1.1 | 4 486 | 55200 | 9.1 | 450 | 57300 | 1.95 | 1.35 | 817 | 0.23 | 432 | 1.05 | 98.8 | 19500 | 446 | 0.11 | 18.6 | 9 | 8450 | 41.6 |
| 020-4 4 | 2300 4 | 0.4 | 6 570 | 84000 | 21.9 | 1060 | 72100 | 3.05 | 2.47 | 1094 | 0.79 | 459 | 1.25 | 195 | 41700 | 1027 | 0.05 | 41 | 6.1 | 11700 | 58 |
| 020-5 3- | 4900 3 | 98 0.8 | 7 690 | 60400 | 13.7 | 429 | 94500 | 1.69 | 2.08 | 767 | 0.72 | 262 | 1.21 | 80.8 | 16460 | 382 | 0.05 | 15.5 | 4.0 | 8020 | 38.5 |
| 020-6 2 | 7100 3 | 53 0.5 | 5 583 | 40500 | 14.64 | 519 | 93500 | 1.55 | 1.25 | 561 | 0.55 | 180 | 0.99 | 78.1 | 15990 | 360 | 0.06 | 7.88 | 2.53 | 6780 | 44.6 |
| 020-7 6 | 5900 3 | 00 0.4 | 7 87 | 13800 | 15.82 | 318 | 46800 | 1.25 | 1.59 | 648 | 0.88 | 1/6 | 0.3 | 129 | 26000 | 345 | 0.04 | 29.4 | 0.95 | 3710 | 17.1 |
| 020-8 3 | 7100 5 | 47 1.4 | 2 1520 | 0 60500 | 18.5 | 641 | 123000 | 2.75 | 2.38 | 830 | 0.82 | 534 | 2.01 | 105 | 16900 | 396 | 0 | 14.3 | 4.55 | 12900 | 44.2 |
| 020-9 3 | 5700 5 | 17 1.6 | 3 1440 | 0 59800 | 16.5 | 670 | 84100 | 2.03 | 1.68 | 692 | 0.61 | 229 | 1.26 | 96 | 13500 | 364 | 0.05 | 8.42 | 4.49 | 11120 | 51.9 |
| 020-10 3 | 7800 5 | 63 0.4 | 970 | 85900 | 11.3 | 550 | 52400 | 2.21 | 1.31 | 615 | 0.72 | 234 | 1.3 | 112 | 14600 | 403 | 0.07 | 14 | 3.15 | 12370 | 46 |
| 8566-1 20 | 3000 5 | 50 25. | 9 4500 | 36200 | 6.1 | 18.2 | 910 | 13.10 | 5.9 | 32.8 | 2.2 | 161 | 3.6 | 3.3 | 28 | 4 | 0.33 | 1.1 | 3.8 | 36 | 2.2 |
| 8566-2 15 | 55000 6 | 56 11 | 2060 | 13900 | 7 | 12.6 | 663 | 7.20 | 1.34 | 19.3 | 0.49 | 133 | 1.64 | 0.05 | 6.6 | 0.74 | 0.08 | 0.01 | 1.64 | 12.3 | 0.69 |
| 8566-3 6 | 0600 3 | 61 4.3 | 1 590 | 4500 | 1.21 | 3.44 | 281 | 3.04 | 0.59 | 7.8 | 0.38 | 119 | 0.59 | 0.03 | 0.9 | 0.36 | 0.05 | 0.03 | 0.63 | 5.7 | 1.07 |
| 8566-4 3. | 2900 3 | 37 3.5 | a 134 | 1310 | 0.07 | 1.1 | 154 | 1.06 | 0.01 | 4.6 | 0.33 | 82 | 0.19 | 0.02 | 0.51 | 0.12 | 0.03 | 0.07 | 0.51 | 1.87 | 0.76 |
| 8566-5 16 | \$ 00085 | 90 15. | 2 1160 | 10600 | 2.3 | 14.3 | 740 | 7.40 | 1.9 | 18.1 | 1.04 | 138 | 2.9 | 0.54 | 4 | 2.3 | 0.32 | 0.15 | 2.8 | 170 | 1.01 |
| 8566-6 19 | 1000 8 | 164 21. | 8 1660 | 0 12800 | 1.89 | 12.6 | 670 | 5.70 | 2.6 | 56.0 | 0.03 | 138.0 | 2.28 | 0.04 | 1.39 | 0.47 | -0.05 | 0.1 | 4.1 | 15.1 | 0.77 |
| 8566-7 23 | 35000 1. | 500 30. | 2 2320 | 0 28200 | п | 22.1 | 970 | 12.90 | 0.7 | 27.9 | 2.48 | 88 | 2.63 | 0.55 | 80 | 10 | 0.05 | 0.4 | 5.7 | 15.8 | 0.68 |
| 8566 - 8 21 | 5000 5 | 70 38. | 0 3660 | 0 26400 | 6.6 | 23.9 | 1170 | 24.20 | 5.1 | 29.1 | 6.1 | 195 | 3.3 | 2.9 | 80 | 14 | 6.0 | 1.3 | 11.5 | 370 | 16.0 |
| 8566-9 21 | 1 0009 | 100 26. | 8 2660 | 14500 | 3.9 | 13.7 | 880 | 13.30 | 5.2 | 21.6 | 0.36 | 152 | 4.6 | 21 | 20 | 2.2 | 0.41 | 0.04 | 4.92 | 22 | 4.1 |
| 8566 - 10 15 | 00000 | 69 23. | 9 1910 | 0 10200 | 2.94 | 11.2 | 740 | 8.60 | 2.5 | 20.3 | 0.28 | 141 | 2.32 | 0.16 | 6 | 0.84 | 0.11 | 0.21 | 2.74 | 11 | 1.4 |
| | | | | | | | | | | | | | | | | | | | | | |

Appendix B – Laser Ablation Data for Sources

| Appendix B - Lase | r ablation IC | MPS data for | all analyses o | f all natural so | urces in order o | of analyses, star | ndard used for | quantification | is listed below | each element | | | | | | | | | | | |
|-------------------|---------------|--------------|----------------|-------------------|------------------|-------------------|------------------|------------------|------------------|------------------|---------|----------|----------------------|------------------------|---------|---------------|------------|-------------------|-------------------|-------------------|-------------------|
| | dır | SHS | "Cr | uM ²⁵⁵ | ⁵⁶ Fe | 59C0 | IN ₀₉ | uZ ⁶⁰ | ⁷¹ Ga | ¹² Ge | SAS SAS | oWe | ¹⁰⁷ Ag 11 | Cd IIS | In II | Sn 121 | 3D 122 U | nV ²⁶¹ | ²⁰² Hg | ²⁰⁸ Pb | ²⁰⁹ Bi |
| | MBH 69 | MBH 69 | MBH 69 | MASSI | MBH 66 | MBH 69 | MBH 69 | MBH 69 | MASSI | VBH 66 M | BH 69 M | A ISSI A | IBH 69 MI | 3H 69 MBF | I 69 MB | H 72 MBF | 69 MBH 0 | (9 MBH 66 | MASSI | MBH 66 | MBH 66 |
| NSCD-03 | 3.9 | 145 | 0.07 | -0.5 | -0.1 | 0.21 | 6.6 | 56.3 | 0.29 | 0.38 | 1.4 | 0.05 | 16.9 | 0.1 0.0 | 0 1 | .0 11. | 9 0.64 | 0.021 | 2.42 | 9.32 | 0.069 |
| NSCD-03_1 | 3.4 | 172 | 60.0 | 0.5 | 2.2 | -0.02 | 6.7 | 61 | 0.27 | -0.65 | 0 | -0.1 | 20.530 | 0.1 0.0 | 1. 1. | 21 0. | 3 0.13 | 0.045 | 1.72 | 8.4 | 0.067 |
| NSCD-03_2 | 4.2 | 152 | 0.13 | -0.25 | 1.88 | -0.01 | 7.9 | 78.1 | -0.03 | -1.18 | 1.48 | -0.03 | 17.2 -0 | 0.0 0.0 | 1 1 | 41 0.2 | 2 0.33 | 0.018 | 2.2 | 10.7 | 0.08 |
| NSCD-03_3 | 1.5 | 126 | 0.05 | 0.27 | 1.8 | 0.03 | 20.2 | 85.8 | -0.03 | 0.38 | 13 | 0.17 | 15.560 | 0.02 0.0 | 1. | .64 0.2 | 7 0.32 | 0.03 | 2.61 | 12.7 | 0.132 |
| NSCD-03_4 | 3.8 | 140 | -0.09 | 0.8 | 1.8 | -0.087 | 8.1 | 107 | 0.19 | -0.3 | 0.87 | 0.13 | 11.260 | 0.02 0.0 | 1 1 | 97 0.2 | 58 0.22 | 0.027 | 2.27 | 13.7 | 0.12 |
| NSCD-03_5 | 2.6 | 137 | 0.146 | 0.4 | 2.09 | -0.06 | 7.2 | 101 | 0.13 | 0.2 | 0.7 | 0.14 | 17.2 | 0.1 0.0 | 00 1. | .61 0.1 | 55 -0.01 | 0.025 | 1.74 | 11.8 | 0.077 |
| NSCD-03_6 | 3.8 | 157 | 0.01 | -0.5 | 1 | -0.08 | 7.6 | 119 | -0.06 | 1.04 | -0.67 | -0.19 | 18.4 | 0.07 0.0 | 00 1 | .87 0. | 5 0.17 | 0.012 | 2.14 | 14.1 | 0.141 |
| NSCD-03_7 | 4.3 | 144 | 0.01 | -0.5 | 0.8 | -0.02 | 7 | 230 | 0.05 | 0.59 | 1.49 | -0.18 | 10.9 (| 0.0 | 00 3. | 26 0.4 | 4 0.24 | 0.047 | 2.34 | 27.7 | 0.232 |
| NSCD-01 | 9.4 | 142 | 0.06 | -0.3 | 2.6 | 0.01 | 8.4 | 233 | 0.36 | 0.36 | 1.57 | 0.15 | 8.1 | 0.01 0.0 | 3. | .78 0.5 | 8 0.24 | 0.02 | 2.1 | 24.4 | 0.217 |
| NSCD-01_1 | 9.3 | 148 | 0.03 | -0.1 | 1.45 | 0.03 | 6.9 | 218 | 0.15 | 0.24 | 1.5 | 0.13 | 4.74 (| 0.04 0.0 | 00 3. | .02 0.3 | 6 0.7 | 0.019 | 2.39 | 21.1 | 0.218 |
| NSCD-01_2 | 13.5 | 144 | 0.01 | 6.1 | 0.6 | 0.11 | 10.7 | 661 | -0.04 | -0.1 | 1.4 | 0.01 | 17.4 | 0.09 0.0 | 00 3. | .17 0.5 | 1 0.74 | 0.072 | 2.24 | 18.8 | 0.225 |
| NSCD-01_3 | 7.6 | 154 | 0.15 | -0.3 | 1.72 | -0.14 | 7.9 | 215 | 0.15 | -0.52 | . 0.9 | -0.04 | 18.8 | 0.03 0.0 | 0 3. | 17 0.3 | 7 0.13 | 0.028 | 2.06 | 18 | 0.173 |
| NSCD-01_4 | 9 | 145 | 0.04 | -0.05 | 0.6 | 0.01 | 7.6 | 183 | -0.05 | -0.5 | 1.1 | 0.39 | 24 | 0.11 0.0 | 33 2. | 39 0.4 | 6 0.47 | 0.025 | 2.38 | 14.3 | 0.145 |
| NSCD-01_5 | 8.7 | 141 | 0.12 | 0.8 | 0.1 | 0.48 | 7 | 194 | -0.1 | -0.23 | 0.82 | -0.04 | 7.69 | 0.03 0.0 | 01 2. | 85 0.4 | 5 0.37 | 0.035 | 1.77 | 15 | 0.185 |
| NSCD-01_6 | 9.3 | 166 | -0.27 | 0.8 | 1.26 | 0.05 | 7.9 | 178 | -0.15 | -0.29 | 0.67 | 0.13 | 12.990 | 0.2 -0.1 | 01 2. | 53 0.1 | 6 0.36 | 0.022 | 1.62 | 13.2 | 0.158 |
| NSCD-01_7 | 6 | 138 | -0.23 | 0.3 | 99 | 0.43 | 693 | 590 | -0.28 | 0.19 | 137 | 0.14 | 197 | 0.13 9.1 | 0 21 | 10 17 | 6 171 | 9.23 | 2.64 | 147 | 36.3 |
| NSCD-02 | 19 | 133 | 0.02 | -0.1 | 0.87 | 0.07 | 10 | 273 | 0.39 | -0.1 | 0.4 | 0.27 | 18.7 (| .0- 70.0 | 01 3. | 36 0.4 | 8 0.57 | 0.024 | 2.86 | 19.8 | 0.225 |
| NSCD-02_1 | 20.7 | 224 | -0.03 | 1.1 | 1.46 | 0.12 | 6.2 | 234 | 0.1 | 0.9 | 1.83 | 0.07 | 10.9 | 0.0 0.0 | 00 2. | .75 0. | 4 0.16 | 0.038 | 2.95 | 18.4 | 0.185 |
| NSCD-02_2 | 21 | 144 | -0.05 | 0.4 | 1.11 | 0.08 | 7.9 | 263 | -0.16 | -0.4 | 1.38 | 0.06 | 13.9 (| 0.0 0.0 | 00 3 | .13 0.4 | 2 0.18 | 0.031 | 3.15 | 20.1 | 0.197 |
| NSCD-02_3 | 22 | 147 | -0.51 | 0 | 1.62 | 0.03 | 8.7 | 250 | 0.16 | -0.61 | 0.26 | 0.08 | 8.08 | 0.12 0.0 | 00 3. | 38 0.2 | 3 0.11 | 0.019 | 2.5 | 19 | 0.205 |
| NSCD-02_4 | 24 | 155 | -1.18 | 0.9 | 1.07 | -0.06 | 9.3 | 243 | -0.07 | -0.18 | - 0.97 | -0.12 | 9.34 (| 0.04 0.0 | 00 3. | 12 0.2 | 3 0.62 | 0.015 | 2.31 | 18.3 | 0.166 |
| NSCD-02_5 | L.L- | 116 | -0.11 | -0.1 | 0.6 | 0.2 | 34.6 | 79.2 | -0.01 | 0.22 | 1.1 | 0.36 | 6.19 (| 0.02 -0.0 | 1 10 | .03 0.1 | 8 0.22 | 0.011 | 2.69 | 7 | 0.073 |
| NSCD-02_6 | 2.6 | 121 | -0.4 | 1.7.1 | 196 | 0.4 | 14.6 | 66 | -0.02 | 0.5 | 2.22 | 0.03 | - 19.8 | 0.12 0.0 | 1 1 | 25 0.2 | 1 0.53 | 0.025 | 2.4 | 8.2 | 0.093 |
| NSCD-02_7 | 90 | 118 | 0.5 | 0 | 1.01 | 0.09 | 7.5 | 161 | -0.05 | 0.9 | 0.3 | 0.09 | 17.5 | 0.01 0.0 | 1 1. | 83 0.2 | 4 0.1 | 0.003 | 2.59 | 12.7 | 0.113 |
| NSCD-07 | 18 | 162 | 1.1 | 1.1 | 0.64 | 0.14 | 6.7 | 152 | 0.02 | -0.93 | 1 | 0.08 | 16.3 (| 0.0 0.0 | 00 1 | .47 0.1 | 73 0.2 | 0.018 | 1.8 | 13.4 | 0.108 |
| NSCD-07_1 | 5 | 125 | 0.93 | -0.51 | 0.18 | -0.02 | 7.9 | 150 | -0.01 | -0.54 | 0.5 | -0.02 | 11.9 | 0.0 | 1 1. | 64 0.1 | 54 0.39 | 0.033 | 2.32 | 12.8 | 0.082 |
| NSCD-07_2 | -2.7 | 396 | 1.62 | 1.4 | 0.16 | -0.09 | 6.5 | 104 | 0.13 | 0.9 | 0.0 | 0.66 | 13.9 0 | .124 0.0 | 1 1. | 02 0.1 | 2 0.22 | 0.006 | 1.78 | 7.3 | 0.1 |
| NSCD-07_3 | 22 | 164 | -0.1 | 0.5 | 1.34 | -0.17 | 10 | 148 | -0.16 | -0.1 | 2.9 | -0.02 | 6.7 | 0.13 0.0 | 1. | .88 0.1 | 8 0.19 | -0.002 | 2.36 | 13.6 | 160'0 |
| NSCD-07_4 | 22 | 378 | 6.0- | 2.2 | 0.51 | -0.08 | 5.5 | 151 | -0.14 | -0.03 | 0.59 | 0.46 | 14 (| .05 -0.0 | 02 1. | .65 0.2 | 5 -0.14 | -0.004 | 1.92 | 13.1 | 0.13 |
| NSCD-07_5 | 6.3 | 244 | 1.1 | 1.3 | 0.43 | 0.09 | 5.7 | 127 | -0.12 | -0.89 | 0.65 | 0.25 | 5.74 | 0.15 0.0 | 1 1. | 37 0.1 | 4 -0.16 | 0.027 | 1.99 | 11.8 | 0.081 |
| NSCD-07_6 | 20 | 142 | 1.7 | 0.82 | 0.84 | 0.07 | 6.1 | 130 | 0.15 | -0.57 | 1.17 | 0.12 | 12.9 | 0.15 -0.0 | 1 10 | .85 0.1 | 9 0.03 | -0.006 | 0.96 | 13.3 | 0.079 |
| NSCD-07_7 | 3 | 137 | -0.2 | -0.61 | 3.4 | -0.067 | 587 | 95 | 0.15 | -0.85 | 139 | -0.04 | 165 - | 0.02 0.1 | 6 | 88 64 | 5 7000 | 7.79 | 2.38 | 610 | 55 |
| NSCD-06 | 6.5 | 142.8 | -0.38 | -1.3 | 0.32 | -0.12 | 12.3 | 93.5 | -0.04 | 0.5 | 1.63 | 0.5 | 7.95 | 0.1 0.0 | 1. 1. | .41 0.1 | 54 -0.05 | 0.05 | б | 13.6 | 0.071 |
| NSCD-06_1 | 2 | 147 | -0.04 | 0.4 | 0.49 | 0.02 | 6.1 | 77.3 | -0.04 | -0.4 | -0.36 | -0.15 | 7.11 | 0.23 -0.0 | 01 | .19 0.1 | 8 0.16 | 0.002 | 1.88 | 11.6 | 0.067 |
| NSCD-06_2 | 14.1 | 96 | -0.09 | 9.0 | 0.44 | -0.12 | 9.9 | 77.6 | -0.06 | -1.12 | 1.1 | 0.03 | 5.92 | 0.04 -0.0 | 1 10 | 44 0.2 | 6 0.4 | 0 | 2.58 | 11.3 | 0.071 |
| NSCD-06_3 | 10 | 124 | 0.27 | 2.07 | 0.65 | 0.03 | 2.7 | 62.3 | 0.26 | -0.47 | 1.18 | 0.11 | 0.940 0 | .125 0.0 | 1 1 | 19 0.1 | 10.0- 1 | 0 | 2.71 | 93 | 0.04 |
| NSCD-06-4 | 5.5 | 871 | CS.0 | -0.12 | 0.30 | 60.0 | 4.0 | 41.9 | -0.19 | -0.1 | 15.1 | 0.3 | 13.8 | 0.0 00.0 | 0 | .0 6/ | c770 0 | 0.006 | 2.00 | 0.84 | 0.00 |
| NSCD-06-5 | 2.2 | 160 | 0.17 | 11.0 | 0.34 | 0.02 | 1.6 | 82 | c1.0 | -0.2 | 0.29 | 0.12 | 9.84 | 0.0- 52.0 | 10 II | 27 0.1 | 11.0- 0.11 | 0 | 2.56 | CII CO | 0.066 |
| 0 00-CD-OL | 6.0 | C01 | -0.16 | 0.8/ | -0.0 | 0 00 | 10.0 | 1.20 | 0.45 | 0.2 | C0.1 | 0.50 | 10./10 | 0.0 1.0 2.0 2.0 0.0 | | 0.0 0.0 | 50.0 CC | 0.024 | \$777 | 5.6 | 0.004 |
| 1 OD-CTOSN | 7.8 | 114 | -0.04 | 100 | 17.1 | -0.05 | × č | 98.9 | 17.0 | 0.0 | 1.8 | 0.87 | - 064.11 | 0.0 /0.0 | 2. | 5.0 0.5 20 | 1.0 1.1 | 0.018 | 1./4 | 10 | 201.0 |
| NSCD-05 1 | 5.4 2 | 136 | 65.0 | 47"N- | 12.4 | 71.0- | 0.0 | 111 | 20.0- | 1.1 | | 0.07 | 2.6 | 00.0 | 1 0 | 20 20 | 10.0 0.04 | 0.054 | 10.7 | 16.1 | 0.13 |
| NSCD 05 2 | 30 | 961 | 7:0 | T O | 07 1 | 101 | 1.0 | 111 | 50.0 | 100 | 90 | 10.0 | 10.420 | 00 00 | | 0 | 0.20 | 0000 | 7 57 | 1.7.1 | 0.154 |
| NSCD-05 3 | 0.7 | 131 | 0.03 | 5.0 | 1.00 | 1.0- | 1.0 | 115 | 0.10 | 0.54 | 0.0 | 0.07 | 1 08 | 107 000 | - C | 18 | 2C.0 C | 0.005 | 10.7 | 1.7 | 116 |
| NSCD-05 4 | 45 | 139 | -0.035 | -0.7 | 80 | 680 0- | 0.1 | 511 | 0.19 | 10- | 0.0 | 0.08 | 6 53 | 500 | 10 | 00 07 | 500 6 | 0.028 | C1 C | 11 | 0.146 |
| NSCD-05_5 | 50 | 149 | 0.00 | 0.86 | 0.4 | 0 144 | 8.2 | 103 | -0.12 | -0.03 | 11 | -0.1 | 7.86 | 00 100 | 0 10 | 13 0.2 | 3 0.79 | 20.02 | 2.29 | 16.8 | 0.14 |
| NSCD-05_6 | 2.1 | 155 | 0.001 | 1.4 | 1.9 | 0.1 | 7.4 | 104 | 0.22 | 0.5 | 0.47 | 0.08 | 7.87 | 0.19 0.0 | 1 | 98 0.4 | 2 0.29 | 0,008 | 0.83 | 16.1 | 0.157 |
| NSCD-05 7 | 15 | 128 | -0.044 | 0.65 | 37 | 0.41 | 920 | 207 | 0.16 | 0.01 | 182 | -0.03 | 169 | 0.13 0.4 | 1 | 09 54 | 0 237 | 8.87 | 2.19 | 356 | 43.1 |
| | | | | | | | | | | | | | | | | | | | | | |

| MBH 69 NSCD-04 3.9 NSCD-04_1 1.9 NSCD-04_2 3.9 | 345 | ^{sa} Cr | 55 Min | 56Fe | 59C0 | IN ₀₉ | 66Zn | 71 Ga | 72 Ge | 56 SV 51 | Mo | 07 Ag 11 | ¹ Cd ¹ | ¹⁵ In 11 | ⁸ Sn ¹² | ¹ Sb ¹² | Te 197 A | 1 ²⁰² Hg | ²⁰⁸ Pb | ²⁰⁹ Bi |
|---------------------------------------------------------|--------|------------------|-------------|------------|---------------|------------------|--------|---------|----------|----------|---------|----------|------------------------------|---------------------|-------------------------------|-------------------------------|----------------------|---------------------|-------------------|-------------------|
| NSCD-04 3.9 NSCD-04_1 1.9 NSCD-04_2 3.9 | MBH 69 | MBH 69 | MASSI | MBH 66 | MBH 69 | MBH 69 | MBH 69 | MASSI A | MBH 66 M | BH 69 M. | 4SSI M. | BH 69 M | BH 69 M | 3H 69 MI | 3H 72 Mb | 3H 69 Mb | H 69 MBH | 56 MASSI | MBH 66 | MBH 66 |
| NSCD-04_1 1.9 NSCD-04_2 3.9 | 148 | 0.03 | 0.1 | 1.2 | 0.03 | 1.7 | 84.1 | 0.02 | 0 | 0.92 | 0.17 | - 16.2 | 0.05 | 10.0 | 1.36 0 | 1.15 -4 | .04 0.02 | 1.67 | 12.53 | 0.094 |
| C.C. 7 40-01-02-0 | C01 | 10.0 | 1.1 | 7.0 | 11.0 | 0.0 | 2.66 | 0.03 | 0.35 | 1.0/ | 11.0 | 11 8 | 0.2 0.1 | 10.0 | 75 0 | 30 36 | 20.0 CT | 1 78 | 14./ | CCL.0 |
| NSCD-04 3 6.4 | 144 | 0.13 | 0.05 | 2.5 | -0.02 | 14 | 80 | -0.06 | -03 | 0.1 | 1.12 | 18.1 | 01.10 | 0.02 | 47 0 | 22 0 | 28 0.02 | 1.27 | 12.2 | 0.115 |
| NSCD-04 4 4.8 | 151 | 0.09 | 0.75 | 3.7 | 0.25 | 7.3 | 119 | 0.35 | 1.34 | 2 | 0.2 | 26.5 | 1.13 | 1 10.0 | .72 0 | 31 0 | 16 0.03 | 1.86 | 1.7.1 | 0.177 |
| NSCD-04_5 1.3 | 147 | -0.06 | 1 | 3.4 | 0.18 | 10.1 | 66.5 | 0.15 | 0.05 | 0.99 | 0 2 | 1.240 - | 0.02 | 0.01 | 1 0 | 1.32 0 | 46 0.01 | 3 2.16 | 9.35 | 0.064 |
| NSCD-04_6 4 | 144.8 | -0.14 | 0.5 | 3.2 | 0.16 | 50.8 | 78 | -0.1 | 0.87 | 1.5 (| 1.23 | 27.6 | 0.11 (| 0.02 | 1.13 6 | 0.38 6 | 08 0.00 | 3 2.68 | 11.5 | 0.078 |
| NSCD-04_7 4.6 | 121 | -0.11 | 0.1 | 2.2 | 0.19 | 4 | 58 | -0.04 | -0.93 | 1.5 | 0.1 | 5.35 | 0 | 10.0 | 0.8 (| 0.13 6 | 39 -0.00 | 2 2.61 | 8.2 | 0.088 |
| NSCD-09 5.5 | 132 | -0.09 0.00 | -0.6 | 1.6 | 0.11 | 4.37 | 11 | 0.36 | -0.07 | 0.81 | 0.03 2 | 1.550 | 0.28 | 00.00 | 0 15 | .05 | 35 -0.00 | 1 2 | 101 | 0.069 |
| NSCD-09_1 5.4 | 135 | 60.0- | 1.7 | 6.7 8 C | 0.16 | 15.6 | 5.85 | -0.15 | -0.52 | - 67 | /0.0 | 11.8 | 0.18 | 10.0 | 08 0 | 13 | 0.0- 0.00 | 10.1 5 | 18./ | 00.0 |
| NSCD-09 3 5.4 | 168 | 0.13 | 0.63 | 1.4 | 10.0 | 9 | 92 | 0.08 | 0.4 | 0.7 | 1.02 | 9.8 | 0.01 | 0.02 | 11 0 | 117 | 00.0- 0 | 5 1.47 | 11.7 | 0.087 |
| NSCD-09 4 5 | 148 | 0.13 | 1.2 | 4.4 | -0.11 | 6.2 | 90 | -0.1 | 0.8 | 1.8 0 | 1.07 | 9.29 | 7.02 | 10.0 | 1.2 0. | 238 -(| 06 -0.00 | 3 2.3 | 12 | 0.077 |
| NSCD-09_5 4 | 131 | -0.26 | 0.8 | 5.2 | -0.03 | 8.2 | 117 | -0.01 | 0.5 | 0.13 0 | 0.08 | - 0.11 | 0.04 (| 1 00.0 | 1.49 6 | 0.11 0 | 48 0.01 | 1 2.1 | 14.7 | 0.102 |
| NSCD-09_6 5.4 | 131.8 | -0.35 | 0.8 | 1.5 | 0.05 | 5.8 | 118 | 0.17 | 0.36 | -0.03 (| 0.19 | - 14.8 | 0.03 (| 1 10.0 | .41 0. | 289 0 | 22 0.03 | 7 1.21 | 13.8 | 0.116 |
| NSCD-09_7 12.8 | 151 | 0.27 | -0.34 | 2.3 | -0.15 | 5.7 | 105 | 0.1 | -0.34 | 0.7 | -0.1 | 6 | 0.01 | 00.0 | .59 6 | 0.13 6 | 36 -0.00 | 1.98 | 13.7 | 0.07 |
| NSCD-10 10 | 149.4 | 0.16 | -0.79 | 4.9 | -0.09 | 5.3 | 108 | 0.07 | -0.6 | 0.09 | 90.0 | 11.7 | 0.04 | 10.0 | 39 0. | - 189 | .05 0.01 | 0.71 | 15.3 | 0.103 |
| NSCD-10_1 9 | 201 | -0.48 | 0.4 | 50 | 0.33 | 630 4.4 | 280 | 0.05 | 0 20 | 1 46 | 0.03 | 188 | 0.14 | 1.62 | 40 0 | 06 | 000 0000 | 2.27 | 230 | 26.2 |
| NSCD-10_2 15.5 | 120 7 | 0.67 | 00'0 | 7.C | -0.07 | 4.4 4 | 001 | -0.01 | 0.6 | 1.40 | 101 | - 65 3 | 1- 506 | 100 | 43 0. | CL | 00.0- 0.0 | 1 1 98 | 17.6 | 0.00 |
| NSCD-10 4 12.9 | 156.1 | -0.4 | 1.24 | 1.7 | -0.19 | 5.9 | 142 | -0.05 | 0.28 | 0.6 | 0.26 1 | 1.57 (| 0.03 0.03 | 0.02 | 1.4 0 | 122 | 1.2 0.02 | 3 2.12 | 17.4 | 0.084 |
| NSCD-10_5 3 | 147 | -0.7 | 0.96 | 0.7 | -0.21 | 7.5 | 151 | 0.2 | 1.31 | 0.7 | 9.11 | - 16.6 | 0.01 | 1 10.0 | .68 0 | 0.21 0 | 42 -0.00 | 1 2.66 | 17.1 | 0.1 |
| NSCD-10_6 22 | 138 | 0.2 | 0.38 | 7.5 | -0.02 | 7.2 | 167 | 0.17 | -1.3 | 1.34 - | 0.09 | - 12.3 | 0.08 (| 1 10.0 | 1.71 6 | 1.33 -(| .29 0.01 | 2.26 | 18.8 | 0.107 |
| NSCD-10_7 22 | 146 | 0.9 | 0.05 | 9 | 0.14 | 5.3 | 148 | 0.05 | -1.21 | 0.8 | 0.06 | 17.3 | 0.16 | 00.0 | .47 0. | - 185 | 0.00 | 2.39 | 17.3 | 0.11 |
| NSCD-11 1 10 | 117 | 0.57 | 2.0 | 4 [| 10.0 | 4 1 | 130 | -0.06 | 01.10 | | 77.0 | 0.61 | - 57.0 | 10.0 | .48 U. 60 0. | 15 0 | 0.03 0.03 55 0.01 | 007 7 | 5.CI 15.A | 0.00 |
| NSCD-11 2 19 | 125 | 1.3 | 0 | 4 | 0.07 | 3.2 | 121 | -0.13 | 0.6 | 0.7 | 0.13 | 38.8 | - 81.6 | 10.0 | .45 0 | | 0.02 0.02 | 2.44 | 13.4 | 160.0 |
| NSCD-11 3 13 | 105 | 0 | 0.37 | 2.2 | 0.07 | 5.3 | 131 | 0.07 | -0.36 | 0.6 | 7.02 | 54.2 | 0.05 (| 1 10.0 | 37 | 0 0 | 0.01 0.01 | 2.62 | 13.8 | 0.095 |
| NSCD-11_4 21 | 138 | -0.64 | 0.7 | 2.9 | 0 | 4.8 | 147 | 0.21 | 1.05 | 1.68 -4 | 0.01 | 58.2 | + 71.0 | 0.01 | 1.65 6 | 0 0 | 59 -0.00 | 1 2.43 | 15.6 | 0.14 |
| NSCD-11_5 22 | 127 | 1.21 | 1.7 | 4.3 | 0.07 | 18.7 | 126 | 0.14 | -0.97 | 1.17 | 0.14 | 55.8 | 9.15 (| 0.03 | 1.56 C | 111 | .2 0.02 | . 1.46 | 13.5 | 0.081 |
| NSCD-11_6 16 | 114 | 1.2 | 0.25 | 3.1 | -0.17 | 6,4 | 170 | 0.07 | 0.69 | 0.22 | -0.3 | 61.6 | 0.27 | 0.02 | 2.17 0 | 0.17 | 58 0.02 | 2.58 | 16.8 | 0.103 |
| NSCD-II / I/ | 154 | -0.4 | -0.12 | 7.7 | 10.0- | 4.4 A | 811 | 0.1 | -0.40 | | 97.0 | 8.02 | 1.0 | 00.0 | 1.18 | 0 500 | 70.0 27 | 1.04 | 0.41 | 760.0 |
| NSCD-12 1 24 | 142.6 | 0.1 | 2.3 | 3.1 | -0.07 | 6.2 | 136 | 0.05 | -1.21 | 0.1 0 | 125 | 16.6 | 9.04 | 1.03 | .76 0. | 209 0 | 21 -0.00 | 13 | 15.2 | 0.128 |
| NSCD-12_2 21 | 142 | 0.2 | -0.7 | 6.6 | 0.18 | 6.4 | 136 | -0.02 | -0.1 | 0 (| .19 | - 23.1 | 0.04 (| 1 00.0 | .59 | 0.1.0 | 62 -0.00 | 1 2.41 | 15.6 | 0.124 |
| NSCD-12_3 14.2 | 106 | 0.32 | 2.4 | 6.4 | -0.16 | 4.5 | 129 | 0.11 | 0.8 | 1.16 (| 60'0 | 16.5 |) 60.0 | 00.0 | 1.28 C | 0.19 | 1 0.01. | 5 1.83 | 14.8 | 0.104 |
| NSCD-12_4 II | 131 | 0.3 | -0.63 | 6.1 | -0.11 | 9.6 | 120 | -0.04 | -0.2 | | 0.24 | 19.2 | .039 | 10.0 | .63 |) (0) | .61 0.02 | 2.07 | 14.4 | 0.08 |
| NSCD-12_5 10./ | 115.7 | 0.0 | -0.0 0.0 | 7.4 | -0.08 0.00 | 4, 6 | 111 | 60.0- | 1.0 | 1.0- | 1 97.0 | 0.42 | 1.0 | 1000 | 75 0. | F 0/1 | 10.0- 62. | 657 1 | 13.8 | 790.0 |
| NSCD-12 7 21 | 140 | -1.6 | -0.6 | 6.2 | 0.1 | 587 | 158 | 0.32 | -0.17 | 145 6 | 102 | 196 | 0.12 | 0.06 | 0.2 | 84 | 6 60 | 1.89 | 16 | 16 |
| NSCD-13 38 | 122.5 | -0.2 | 1 | 3.4 | -0.09 | 2.9 | 148 | -0.04 | -0.11 | -0.2 | 9.22 | 10.2 |).24 (| 10.0 | 1.4 0 | 0 0 | 64 0.01 | 7 2.82 | 16.4 | 0.1 |
| NSCD-13_1 24 | 117 | 1.7 | -0.1 | 4.3 | -0.03 | 4.5 | 149 | 0.07 | -1.05 | -0.19 | 9.26 | 11.4 |).07 (| 1 10.0 | .64 0 | 129 0 | 42 0.02 | 5 2.63 | 17 | 0.101 |
| NSCD-13_2 29 | 142 | 1.6 | -0.57 | 4.2 | -0.01 | 3.75 | 141 | 0.06 | 1 | -0.24 | 0.04 | 15.8 |) 60.(| 0.02 | 1.74 0. | 212 0 | 18 -0.00 | 5 2.55 | 16.3 | 0.118 |
| NSCD-13_3 26 | 116 | 4.6 | 2.05 | њ. 1 | -0.03 | 4.2 | 145 | 80.0 | 16.0 | 0.8 | 80.0 | 9.46 | 0.1 | 000 | . 67 | 0.13 6 | -0.00 | 5 2.44 | 15.9 | 0.081 |
| NSCD-13_4 22.9 | 147 | 0.3 | 0.4 | 1.7 | -0.11 | 4.7 | 147 | 0.07 | -0.45 | 0.72 | 0.25 | - 68.6 | 0.02 | 50.0 | 1.0 | 1 20 | 27 0.00 | 2.31 | 10.8 | 0.115 |
| NSCD-13 6 37 | 001 | C.0 | | 4.8 | -0.13 | t, v | 136 | -0.02 | 10.0- | 10.0 | 0 | 5 01 | 0 010 | 0000 | 0 89 | 312 17 | 000-0-000 | 6177 S | 14.3 | 0.067 |
| NSCD-13_7 29 | 126 | 8.8 | 1.2 | 3.1 | -0.14 | 2.1 | 182 | -0.03 | 0.14 | 1.4 | 0.11 | 12 | 0.1 0. | 0.03 2 | .32 0 | 26 0 | 38 0.02 | 2.86 | 23.4 | 0.161 |

| Appendix B continue | 31P | S ^H | ⁵³ Cr | ⁵⁵ Mn | ⁵⁶ Fe | ⁵⁹ C0 | IN ₀₀ | uZ99 | 71Ga | ⁷² Ge | 75AS | 95M0 | 107 Ag | ^{III} Cd | 115 In | 118 Sn | ¹²¹ Sb | ²⁵ Te 19 | Au 202 | Hg 208 | b 20 |
|------------------------------|--------------|----------------|------------------|------------------|------------------|------------------|------------------|---------------|------------|------------------|-------------|-------------|--------|-------------------|---------------|----------|-------------------|---------------------|----------------|------------------|---------|
| NSCD-14 | MBH 69 40 | 87 87 | 7 MBH 69 | MASSI | 0 270 | 0 001 | 3 4 69 | 013 MBH 69 | ISSM -0.77 | 0.43 0.43 | ABH 69 A | MASSI 10.47 | MBH 69 | -0.13 | 0.04 MBH 69 A | 18H 72 A | M 69 HB | 8H 69 MB | H 66 MA | 18M 18S | 66 MB |
| NSCD-14 1 | 32 | 134 | 13 | 0.2 | 2.8 | 0.21 | 4.6 | 192 | -0.06 | 0.05 | 6.0 | -0.33 | 13.9 | -0.19 | 0.03 | 2.54 | 0.37 | 0.5 0. | 06 2. | 03 2 | |
| NSCD-14 2 | 16 | 157 | 210 | 0.2 | 8.2 | 0.33 | 4.2 | 181 | 0.12 | 0.7 | -0.37 | 0.07 | 17.8 | 0.07 | 0.01 | 2.31 | 0.106 | 1.1 0. | 012 1. | 92 24 | 1 0. |
| NSCD-14_3 | 24.3 | 129 | Π | -0.1 | 2.9 | 0.05 | 4.1 | 188 | 0.19 | 0.42 | 2.2 | 0.38 | 9.93 | 0.29 | -0.01 | 2.14 | 0.28 | 0.46 0. | 014 2. | 32 24 | 5 0. |
| NSCD-14_4 | 10 | 156 | - | 1.4 | 3.8 | 0.11 | 7.9 | 223 | 0.12 | -0.16 | 2.1 | -0.01 | 17.4 | 0 | 0.01 | 2.77 | 0.22 | 1.07 0. |)34 2. | 08 28 | 2 0. |
| NSCD-14_5 | 26 | 116 | -5.2 | 5.6 | 9.0 | 0.07 | 6.6 | 116 | -0.1 | -0.3 | 1.4 | -0.02 | 20 | 0.11 | 0.02 | 1.54 | 0.13 | 0.67 0. | 009 1. | 18 | 0.0 |
| NSCD-14_0 | 010 | 136 | 6.5 | 1.0 | 0.1 | 10.0 | 406 | 4C1 | -0.08 | 0.70 | C.U | 0.10 | 101 | 0.04 | 20.0 | 3.4 | 671.0 | 0./ 0. | 000 0. 3 0. | 11 12 | 0 F |
| NSCD-15 | 23 | 124 | L- | 0 | 0.29 | -0.03 | 4.6 | 157 | 0.57 | -0.27 | 0.34 | 0.25 | 21.1 | 11.0 | 10.0 | 1.73 | 0.16 | 0.7 0. | 003 1. | 39 18 | 6 |
| NSCD-15_1 | 20 | 172 | - | -0.8 | 1.09 | -0.08 | 1.4 | 127 | 0.08 | -1.07 | 1 | -0.25 | 24 | -0.09 | -0.01 | 1.29 | 0.186 | 0-19 -0 | 001 2. | 14 15 | 2 0. |
| NSCD-15_2 | 13 | 150 | 41 | 1.18 | 0.19 | 0.07 | 2.6 | 110 | 0.05 | -0.54 | -0.1 | 0.19 | 20.5 | 0.01 | 10.0- | 1.25 | 0.041 | 0.08 0 | 01 2. | 72 13 | 2 0. |
| NSCD-15_3 | 21 | 130 | 46 | 0.7 | -0.2 | 0.05 | 4.7 | 115 | 0.2 | -0.63 | 0.8 | 10.0 | 26.2 | -0.03 | 0.01 | 1.21 | 0.12 | 0.24 0. | 012 2 | | 0 |
| NSCD-15 4 | 10 | 1/2 | 1- 12 6 | 1.0 | 0.36 | -0.00 | 5.5 9 I | 271 | 27.0 | 0.7 | 1.0- | -0.11 | 0.62 | 0.04 | 0.00 | 80.1 | 0.75 | 0.57 0 | 001 27 | 12 14 | 2 0 |
| NSCD-15 6 | 22 | 162 | 5.8 | 07.0 | 0.13 | 0.05 | 2.1 | 124 | -0.27 | 0.01 | -0.15 | -0.14 | 13.6 | 0.17 | 0.01 | 1.45 | 0.198 | 0.8 0.0 | 008 2 | 31 | 00 |
| NSCD-15 7 | 8 | 166 | -2.3 | 0.3 | 0.29 | 0.04 | 3.4 | 131 | 0.27 | 0.4 | 0.6 | 0.07 | 13.3 | 0.26 | 0.01 | 1.38 | 0.19 | 0.07 0. | 06 3. | 03 16 | 8 0.0 |
| NSCD-16 | 14 | 138 | 1.5 | -0.2 | 0.24 | -0.02 | 9.3 | 156 | 0.16 | -0.42 | 0.7 | 0.01 | 11.5 | 0.17 | 0.02 | 1.87 | 0.21 | 0.8 0. | 025 2. | 36 19 | 1 0. |
| NSCD-16_1 | 21 | 136 | -3.6 | 0.2 | 0.41 | -0.06 | 6.8 | 172 | 0.06 | -0.44 | 0.55 | 0.07 | 13.6 | 0.1 | 0.00 | 1.94 | 0.2 | 0.39 0. | 006 2. | 53 21 | 1 0. |
| NSCD-16_2 NSCD-16_3 | 10.1 | 180 | -0.4 2 | 1.5 | 0.16 | 0.08 | 0.0 | 18/ | -0.55 | 0.00 | 14 | 0.05 | 18.8 | 0.02 | 10.0 | 1.74 | CF2 0 | 0.09 0.0 | 11 1. | 2 2 2 | o o |
| NSCD-16 4 | 20 | 150 | 1.1 | 1.31 | 0.25 | -0.03 | 6.6 | 196 | 0.19 | 0.08 | 0.65 | -0.07 | 5.82 | 0 | 0.01 | 1.9 | 0.17 | 0.82 0. | 36 1. | 35 26 | 000 |
| NSCD-16_5 | 15.5 | 119.8 | -1.3 | 0.1 | -0.01 | 0.06 | 4.2 | 126 | -0.06 | -0.35 | -0.7 | 0 | 5.52 | -0.05 | 0.00 | 1.49 | 0.038 | 1.3 0. | 009 1. | 95 17 | 4 0 |
| NSCD-16_6 | 9.8 | 150 | -0.4 | 0.7 | 0.15 | -0.12 | 5.8 | 166 | 0.03 | 0 | -0.3 | -0.27 | 14.4 | -0.03 | 0.04 | 1.59 | 0.24 | 0.72 0. | 06 2. | 56 21 | 8 8 |
| NSCD-08 | 64 | 157 | 0.0 | C-7 C | 0.47 | 0.05 | 5 56 | 151 | -0.13 | 0.6 | 161 | -0.06 | 36.9 | 20.0 | 0.03 | 1.00 | 50 0 | 0.04 0.0 | 7 C70 | 6 18 | |
| NSCD-08_1 | 21.2 | 164 | 1.7 | 0.9 | 0.18 | -0.04 | 5.6 | 151 | 0.03 | -0.26 | 0.27 | 0.33 | 11.4 | 0.06 | 0.01 | 1.45 | 0.1 | 0.54 0. | 1. 1. | 76 19 | 8 0. |
| NSCD-08_2 | 22.7 | 140 | 1.7 | 0.56 | 0.383 | 0.02 | 3.3 | 166 | -0.22 | -0.61 | -0.01 | -0.1 | 12.2 | -0.02 | 0.00 | 1.84 | 0.18 | 0 60.1 | 004 1. | 82 21 | 3 0. |
| NSCD-08_4 | 51 | 144 | 1.9 | 5.4 -0.3 | c0.0 | 17.0 | 6.8 | 166 | 17.0- | -0.13 | C8.0 8.0 | 0.01 | 20.3 | c0.0 | -0.01 | 1.15 | 0.25 | 0.28 0. | | 10 80 | 00 |
| NSCD-08 5 | 16 | 107 | 0 | 0.5 | 0.121 | -0.04 | 0 m | 166 | 0.13 | 0.8 | 0.0 | 0.36 | 36.7 | -0.02 | 0.01 | 1.71 | 0.28 | 0.78 | | 21 21 21 | 0.0 |
| NSCD-08_6 | 16 | 151 | 2.3 | 0.2 | 0.25 | 0.08 | 5.4 | 175 | 0.3 | 0.27 | -0.2 | 0.04 | 10.9 | 0.01 | 0.00 | 1.76 | 0.32 | 0.18 0. | 0. 0. | 77 23 | 9 0. |
| NSCD-08_7 | -2.6 | 171 | 0.5 | -0.1 | 20.7 | 1.04 | 672 | 840 | -0.01 | 0.16 | 146 | -0.18 | 177 | 0.37 | 8.30 | 1750 | 620 | 8040 7 | 91 2. | 26 24 | - 0 |
| Bolivia 1 | 6.6 | 182 | -0.2 | -0.1 | 14.1 | 0.016 | 0.16 | 20.05 | 0.024 | -0.35 | 0.8 | 0.029 | 2.89 | 0.034 | -0.01 | 0.15 | 0.12 | 20.0 | | 54 0.0 | 10 0 |
| Bolivia_2 | -3.1 | 148 | -0.8 | 1.5 | 11.8 | 0.018 | 0.52 | 0.33 | -0.005 | -0.93 | 0.58 - | -0.004 | 2.21 | 0.0335 | 0.00 | 0.06 | 0.07 -0 | .0915 -0 | 001 1. | 48 0. | 5 -0. |
| Bolivia_3 | 5.5 | 139 | 16.0- | 0.5 | 0.7 | 0.011 | -0.24 | -0.53 | 0.025 | 0.46 | 0.21 | 0.004 | 1.87 | 0.09 | -0.01 | 0.06 | -0.01 | 0- 90'0 | 001 1. | 75 -0.0 | 0 * |
| Bolivia_4 Rolivia_5 | 6.6 | 147 | -1- | 0.4 | c0.0 8.0 | 200.0 | 0.24 | -0.45 | -0.002 | 1.0 | | -0.009 | 0.17 | 0.063 | 10.0- | 0.037 | -0.07 | .105/ | | 4/ 0.0 81 0.0 | 0.0 |
| Bolivia 6 | 4.8 | 142 | 0.1 | 1.4 | 3.9 | -0.008 | -0.44 | 1.49 | 0.036 | -1- | 0.5 | 0.008 | 3.43 | 0.001 | 0.01 | 0.07 | 0.23 | 0.05 | 0 1. | 46 0.1 | 98 -0.0 |
| Bolivia_7 | 6.6 | 162 | 0.1 | 1.9 | 33.8 | 0.014 | 0.46 | 0.02 | -0.009 | 0.42 | -0.04 | 0.019 | 1.7 | -0.009 | 0.00 | -0.02 | -0.02 | 0.163 -0 | 001 2. | 15 0.1 | 0.0 |
| Kazakhstan | 3.3 | 124 | 1.2 | - 0 | 0.1 | 0.028 | 0.18 | -0.33 | 0.1 | -0.66 | 0.94 | -0.045 | 7.66 | 0.02 | 0.02 | -0.044 | - 0.07 | 0.056 -0 | 001 2. | 54 0.0 | H6 0. |
| Kazaknstan_1 Kazakhstan 7 | 6.D | C71 | -0.7 50.7 | 0.5 | -0.5 | C00.0- | 25.0- 0.04 | -0.47 0.47 | 220.0- | -0.45 | - FC 0 | 0.000 | 878 | 0/0.0 | 10.01 | 11.0 | - 20.0- | 0- 00.00 | 100 100 | 13 0.0 | 0 |
| Kazakhstan 3 | 3.2 | 182 | 0 | 0.42 | 0.3 | 0.024 | 0.2 | -0.8 | 0.029 | 0.5 | 0.65 | 0.044 | 96.6 | 0.008 | 0.01 | 0.04 | 0.017 | .024 0. | 000 3. | 0.0 0.0 | 88 |
| Kazakhstan 4 | 5.2 | 115 | 1.9 | 1.2 | -0.7 | 0.016 | 0.25 | 0.87 | -0.023 | -0.32 | 0 | 0.1 | 100.2 | -0.026 | 0.00 | 0.1 | 0 | 0.018 -0 | 006 2. | 51 0.0 | 22 0.1 |
| Kazakhstan_5 | 0.6 | 131.5 | 1.4 | 1.03 | -0.5 | 0.074 | -0.19 | -0.16 | 0.043 | 0.7 | 0.55 | -0.016 | 40.7 | -0.023 | 0.02 | 0.008 | -0.08 | 0- 200 | 005 2. | 0.0 0.0 | 10 10 |
| Kazakhstan 7 | 0 | 113 | 2.5 | -1.12 | -0.9 | 0.01 | -0.28 | -0.3 | 0.037 | 0.3 | - 0.47 | -0.003 | 43.4 | -0.034 | 10.0 | 0.07 | 0.12 | 0.05 | 0 | 41 -0.0 | |

| | 0W ³⁶ 8 | 107 Ag | ¹¹ Cd | us na | ⁸ Sn 121 | ¹ Sb 125 | Te 197 | Au 202F | g ²⁰⁸ Ph | 209 |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------|-----------|------------------|-----------|---------------------|---------------------|----------|------------|---------------------|-------|
| Montrality 1 151 151 151 151 151 151 151 151 151 | 69 MASSI | MBH 69 A. | 4BH 69 Mi | BH 69 MB | H 72 MB | H 69 MB | H 69 MBI | H 66 MAS | SI MBH 60 | 6 MBH |
| Montrialier in the standard of the standard in the stand | 5 0.005 | 30.5 | -0.016 | 0.00 -0.0 | .054 -0 | 0.0- 10.0 | 0162 | 0 2.2 | 0.001 | 0.0- |
| Montraji i i i i i i i i i i i i i i i i i i | 0.006 | 35.5 | -0.022 | 0- 10.0- | 0.04/ 0.0 | -0. | 1220 | 0 2.4 | 0.04 | 0.0 |
| | 0.02 | 52.6 | 0,061 | 0.01 0.0 | 105 -0.4 | 008 -0.0 | 043 | 0 2.2 | 0.004 | 0.0 |
| MNLS3111112010101010101010101MNLS3131313141313010101010101010101MNLS31313131413141301010101010101010101MNLS31314131401010101010101010101010101MNLS3141516010101010101010101010101MNLS31212120101010101010101010101MNLS31212120101010101010101010101MNLS31212120101010101010101010101MNLS31212120101010101010101010101MNLS3121201010101010101010101010101MNLS3121201010101010101010101010101 <tr< th=""><th>4 0</th><th>43.1</th><th>0.029</th><th>0.01 -0.</th><th>.0- 160.</th><th>.111 0.6</th><th>005</th><th>0 1.6</th><th>1 0.005</th><th>0.0</th></tr<> | 4 0 | 43.1 | 0.029 | 0.01 -0. | .0- 160. | .111 0.6 | 005 | 0 1.6 | 1 0.005 | 0.0 |
| | 4 0.061 | 10.7 | -0.005 | 0.00 -0. | .025 -0. | .104 0. | .13 | 0 2.2 | 3 -0.017 | 0.0 |
| Montaciality is indicated by the matrix and | 2 0.038 | 14.2 | 0.004 | 0.03 0. | 0.002 | .04 0. | 0.0 0.0 | 006 2.1 | -0.006 | 0.0 |
| | 4 0.083 7 -0.004 | 70 | 0.0152 | 0-00 000 | .104 | 0 -0.1 | 115 | 0 2.5 | -0.008 | 0.0 |
| | 8 0.012 | 53.9 | 0 | 0.00 0.0 | 0- 100 | 083 -0.0 | 062 | 0 2.6 | 0.06 | 0.0- |
| | 7 -0.012 | 64.6 | 0 | 0.03 0. | .14 0. | .04 0. | .12 | 0 2.2 | 5 0.015 | 0.0 |
| | 5 -0.027 | 46.8 | -0.013 | 0.00 0 | .05 -0. | .101 -0.6 | 1599 (| 0 2.1 | 5 0.042 | 0.0 |
| | -0.029 | 17.1 | -0.014 | 0.00 0.00 | 0 60.0 | 0.07 0.0 | 019 | 0 2.0 | 0.052 | 0.0 |
| | 2000- 8 8 | | 600.0- | 0- 000 | 0 110 | .00.0 | 740 | 0 | 0.003 | 0.0 |
| | 0.051 | 97.2 | -0.010 | 0.01 0.0 | 042 -0 | 0.1 0.0 | 023 | 0 2.3 | 5 0.021 | 0.0 |
| | 5 0.072 | 236 | 0.009 | 0.00 -0.0 | .027 -0. | .0- 010. | 005 | 0 4.9 | -0.002 | 0.0 |
| | 3 -0.008 | 239 | -0.005 - | 0.01 | 0 0. | 0.0- 0.0 | 303 (| 0 4.4 | 4 -0.04 | 0.0 |
| | 3 0.039 | 246 | 0.002 | 0.00 0.0 | 042 -0 | 0.0- 10.0 |)256 | 0 4.6 | 0.023 | 0.0 |
| | 9 0.035 | 228 | -0.010 | 0.00 0.0 | 061 -0. | 0.032 0.0 | 014 | 0 5.2 | 0.036 | 0.0 |
| | -0.004 5 -0.014 | 656 | 0 08 | 0.00 | .0- 000 | 081 0.0 | 000 | 0 52 | 100.0- | 0.0 |
| | 600.0- 7 | 217 - | -0.015 | 0.00 -0.0 | 025 0. | .04 -0. | 200 | 0 4.4 | -0.015 | 0.00 |
| | 9 0.015 | 246 - | -0.015 | 0.00 0.0 | 017 0. | 1.0- 00.0 | 006 | 0 5.3 | 2 0.015 | 0.01 |
| | -0.004 | 435 | 0.089 | 0.00 0.0 | 054 0. | 0.0 0.0 | 034 | 0 4.6 | -0.006 | 0.00 |
| | 4 0.015 5 0 | 367 | 0.014 | 0.00 | .0 / .0. | .0 .0 .0.0 | 001 | 0 0 0 4 | 0.005 | 0.0- |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | 5 -0.008 | 371 | 0 | 0.00 00.0 | 035 0. | .0- 90. | 600 | 0 4.8 | 5 0.018 | -0.0 |
| | 6 -0.012 | 385 | -0.005 | 0.00 0.0 | 067 -0. | .004 -0.1 | 008 | 0 3.4 | 4 -0.017 | 0.01 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 7 -0.004 | 366 | 600.0- | 0.02 0 | .05 0.4 | .067 0.0 | 002 | 0 4.3 | 5 0.038 | 0.00 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 8 0.036 | 369 | -0.004 | 0.00 0.0 | 005 0.0 | .018 -0. | 008 | 3.8 | 0.023 | -0.0 |
| | 7 0.045 | 287 | .0.00 | 0.00 0.0 | 071 -0. | 0.0 0.0 | 016 | 0 5.7 | 100.0- 4 | -0.0 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1 0 | 405 | 0 | 0.00 0.0 | 018 -0. | 0.0 0.0 | 110 | 0 8.9 | 0.034 | -0.0 |
| $ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | 0 6 | 286 | 0.016 | 0.01 0. | 017 -0 | 0.13 -0. | 007 | 0 4.6 | -0.005 | -0.0 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 0 0 | 167 | | 0.00 | 0- 050 | 0.0 0.0 | 200 | 0 0.1 | 5 -0.043 | 10 G |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1 0.037 | 277 | 0.014 | 0- 00.0 | 0.0 0.0 | 024 -0.0 | 002 | 0 5.2 | 0.004 | -0.0 |
| MuN-Kew 7 74 108 -0.21 0.47 0.5 0.068 0.04 -0.18 -0.06 0.08 0.04 0.18 0.000 0.01 0.00 0.01 0.06 0.01 MuN-Kew 1 2.1 109 0.22 0.05 0.16 0.017 0.118 0.33 0.003 0.01 0.22 0 273 0.009 0.00 0.061 0.066 0.014 MuN-Kew 1 2.3 103 -0.33 0 -1.5 -0.017 0.13 0.33 0.013 0.21 3.59 0.0 0.00 0.01 0.046 0.016 MuN-Kew 3 0 80 0.56 0.34 -1.61 0.007 0.13 0.28 0.01 0.43 3.59 0.012 2.67 0 0.00 0.03 0.010 0.006 MuN-Kew 3 0 80 0.56 0.3 -1.61 0.007 0.13 0.28 0.01 0.43 3.47 0.012 2.67 0 0.00 0.03 0.010 0.001 | 2 0.014 | 263 | -0.005 | 0.00 0.0 | 027 -0. | .036 -0.4 | 007 | 0 5.5 | 5 -0.009 | 0.0 |
| Mun-Kew 2 0.2 79 0.2 -0.05 -0.06 0.007 -0.18 0.33 -0.003 0.01 0.22 0 273 -0.099 0.00 0.061 -0.096 0.01 Mun-Kew 2 1 2.3 103 -0.03 0 -1.5 -0.012 0.22 0.41 -0.003 -0.24 0.89 0 2.29 0 0.01 0.043 0.001 -0.006 Mun-Kew 2 1 5.4 114 -0.06 1.04 -1.8 -0.005 -0.51 -0.62 0.012 0.21 3.59 -0.012 2.76 0 0.00 0.012 -0.12 -0.007 Mun-Kew 3 0 89 0.55 0.3 -1.61 -0.007 -0.13 0.28 -0.011 0.43 5.47 -0.012 0.003 0.013 -0.11 0.009 | 2 0 | 259 | -0.009 | 0.00 0.0 | 017 -0 | 0.06 -0.0 | 014 0 | 0 4.8 | -0.01 | -0.0 |
| MUNTARVZ 1 2.5 103 -0.05 0 1 -1.5 -0.012 0.5 0.5 0.41 -0.005 -0.54 0.39 0 2.29 0 0.01 0.045 0.001 -0.006 MUNTARVZ 1 5.4 114 -0.06 1.04 -1.8 -0.005 -0.51 0.62 0.011 0.21 3.59 -0.012 2.76 0 0.00 0.012 0.12 0.007 MUNTARVZ 1 0 89 0.012 0.161 -0.007 0.13 0.28 -0.011 0.43 4.7 0.012 2.76 0 0.00 0.035 -0.11 0.009 | 2 0 | 273 | -0.009 | 0.00 0.0 | 061 -0. | .0- 960. | 014 | 0 5.6 | 0.037 | 0.00 |
| MILIAMENTEZZI 20 10 0.05 0.3 1.61 0.007 4.11 0.28 0.011 0.43 2.57 0.012 0.03 0.012 0.11 0.009 0.012 0.012 0.010 0.012 0.011 0.009 | 0 6 | 926 | | 0.01 | 0.0 0.0 | -0- 100- | 000 | 6.C 0 | 2000 0 | 0.00 |
| | 7 -0.012 | 267 | 0 0 | 0.00 0.0 | 035 -0. | 0.0 11.0 | 600 | 0 4.8 | 0.002 | 0.00 |
| Mult-Kew2.4 0.8 123.1 0.17 -1.5 0.6 0.02 0.17 -0.07 0.002 0.44 3.98 0 273.5 0.001 0.00 0.03 -0.162 0 | 8 0 | 273.5 | 0.001 | 0.00 0.0 | .03 -0. | .162 (| 0 | 0 5.6 | 0.034 | 0.00 |
| MuMKew2.5 4.2 94.2 0.28 0.1 -2.7 0.015 0.48 0.7 0.057 0.02 8 0 2.65 0.019 0.00 0.036 0.041 0.003 | 0 | 265 | -0.019 | 0.00 0.0 | 036 -0. | .041 -0. | 003 | 0 5.3 | 0.018 | 0.0- |
| MINANARY, 25 3.4 110 0.11 0.77 -2.2 4.0003 -0.03 0 -0.005 0.46 5.7 -0.020 2.99 0.016 0.00 0.004 0.0194 0.0105 MINARARY, 7 3.8 110 0.13 0.29 5.5 0.004 -0.43 0.06 0.46 0.47 0.06 0.47 0.014 0.002 0.004 0.000 0.004 0.0144 0.005 | 0.020 | 299 | 0.016 | 0.00 | 0.0 610 | 102 -0.0 | 1025 | 0.0 | 0.055 | 0.0 |

| Appendix B contit | -11 | 11 | 13 | - 32 | - 12 | 60 | 60 | - 11 | | | 3 | | 1 10 | | | 101 | 361 | 101 | 100 | 306 | 100 |
|----------------------------|--------|--------|--------|------------------|----------------------------|---------|--------|--------|----------|---------|----------|---------|-----------|---------|----------|-----------------------------------------|-----------|---------------------|-------|-------|--------|
| | MRH 69 | MRH 60 | WRH 60 | uM ^{oc} | ³⁰ Fe MBH 66 | MBH 69 | MRH 60 | MRH 60 | MASSI M | BH 66 M | AS AS | OM ISSE | BH 60 M | Cd MB | TI OT AR | H 72 MRI | Sb MBH | fe ¹⁹⁷ A | H-m n | g MRH | MRH 6 |
| MuM-Co1 | 1.1 | 103.3 | -0.16 | -0.08 | -0.7 | -0.026 | -0.27 | 0.1 | -0.006 | 0.18 | -0.5 0 | 0.018 (| 860.0 | 0 0 | .01 0. | 103 -0. | 15 0.0 | 7 0 | 2.82 | 0.078 | -0.016 |
| MuM-Co1_1 | 9.3 | 107 | -0.17 | 1.1 | 0.36 | 0.052 | 0.23 | 0.53 | 0.025 | 0.4 | -0.3 | 0 | 0.044 | 0 0 | .00 00. | 023 (| 0.0 | 0 0 | 2.2 | 0.018 | 0.006 |
| MuM-Col_2 | 1.2 | 101.7 | -0.26 | -0.54 | 0.4 | 0.025 | 0.32 | -0.16 | 0.003 | .0.09 | 0.31 | 0 | 0.298 | 0 0 | .02 0. | 0- 680 | 0.0 0.0 | 0 90 | 32 | 0.032 | 2.86 |
| MuM-Col_3 | 4.9 | 011 | 0.83 | -0.22 | 17.4 | 0.083 | 0.4 | 1.1 | -0.008 | -1.3 | 1.01 6 | 0.054 | 1.48 -(| 015 0 | 00.00 | 0.0 0.0 | 02 -0.0 | H3 0 | 2.32 | -0.00 | 0.172 |
| MuM-Col 4 | 6.11 | 15/ | 1.0 | -0.35 | 78.0 | /00/0- | 0.04 | 87.1 | 0.016 | 10.0- | 0.46 | 0 0 | - /2010 | 0 670.0 | 0 70. | 1.0 800 | 145 0.0 | 10 0 | 181 | 67.0 | 11 |
| MuM-Col 6 | 2.2 | 122 4 | 1.15 | CZ-0 | 70.0 | 1000 | 0.43 | -0.43 | 010.0 | 050 | 1 55 L | 004 | - /01.0 | 0 010 | 00 | 754 0.0 | 0.0 59 | 0 0 | 1000 | 0.000 | 0.11.0 |
| MuM-Col 7 | 4 | 132 | -0.93 | -0.47 | -0.22 | -0.004 | -0.04 | 0.54 | -0.006 | 1.17 | 0.47 -6 | 0.004 6 | 1.021 -6 | 0 9000 | 0 10 | 757 0.0 | 33 0.1 | 0 | 2.7 | 0.022 | 0.022 |
| MuM-Co2 | 3.2 | 128 | 0.36 | -0.5 | 0.18 | 0.059 | 0.32 | -0.39 | -0.005 | -0.04 | 1 | 0.01 | 1.22 0 | .051 0 | .01 0. | 916 -0.0 | M8 0.0. | 35 0 | 3.18 | 0.03 | 0.036 |
| MuM-Co2_1 | 1.5 | 114 | 0.86 | -1.1 | 43.4 | 0.075 | 0.72 | 1.25 | 0.011 | -0.67 | 0.9 | 0 |)- 76.0 | 0.006 0 | .14 0. | 0.0000000000000000000000000000000000000 | 05 0 | 0 | 2.23 | 0.206 | 7.9 |
| MuM-Co2_2 | 3.4 | 143 | 0 | -1.5 | 1.99 | 0.005 | 0.37 | 0.25 | -0.006 | -0.42 | 0.14 -(| 600.0 | 20.4 | 0 0 | .05 0. | 026 -0. | 04 0.1 | 0 10 | 8.3 | 0.054 | 19.4 |
| MuM-Co2_3 | -0.1 | 135 | -0.45 | 0.4 | 0.1 | -0.002 | 1.01 | 0.17 | -0.005 | 0.17 | 0.8 | 0.008 | 12 0 | 017 0 | .02 0. | 146 0.1 | 122 0.0. | 28 0 | 6 | 0.09 | 16.2 |
| MuM-Co2 4 | | 155 | 0.0 | -1.06 | 18.0 | 0 00 | 80.0 | 1 0.05 | 10.0 | 0.45 | 70.0 | 0 0 | 8.12 | | 0 0 0 | 0 00 | 11 -0.0. | 0 the c | 2.2 | C0.0 | 1.13 |
| MuM-Co2 6 | 5.6 | 150 | 4.0 | 0.0- | 0.13 | 20.0 | 17.1 | CU.U- | 0.003 | 0.10 | 21.0 | | | 0 00 | .0 0. | 151 00 | 1'n CI | 115 0 | 195 | SU.U | 18.4 |
| MuM-Co2 7 | 0.0 | 146 | 0.2 | -0.19 | -0.59 | 0.009 | 0.16 | 0.15 | -0.003 | 0.51 | 0.29 | 0 | 0.68 0 | 015 0 | 00 | 0.0 0.0 | 93 -0.0 | 0 10 | 2.88 | 0.03 | 0.444 |
| MuM-Cu1 | -0.6 | 150 | -1.4 | 0.7 | -0.02 | 0.026 | 0 | 0.23 | -0.009 | 0.48 | 0.34 -(| 0.005 1 | 01.3 | 0 0 | .01 0. |).0- 860 | 0.0 0.0 | 9 | 2.81 | 0.034 | 0.125 |
| MuM-Cu1_1 | -2.5 | 148 | 1.7 | 0.14 | 1.27 | -0.007 | -0.11 | -0.2 | -0.003 | -1.14 | 1.39 -(| 0.004 | 63.6 -(| 0.005 0 | 00 00 | 1.1 -0.1 | 0.0 -0.0 | 14 0 | 2.62 | 0.028 | 0.02 |
| MuM-Cu1_2 | 7.5 | 190 | 1.7 | -1.4 | 0.88 | 0.04 | -0.03 | 0.34 | 0.011 | -0.8 | 2.2 | 0 | 68.2 -(| 0.006 0 | .00 00. | 016 0. | 14 0.1 | 7 0 | 2.55 | 0.020 | 0.479 |
| MuM-Cu1_3 | -8.9 | 163 | -0.8 | 0 | -0.2 | -0.002 | 0.77 | -0.35 | 0 | -0.36 | 2.27 | 0 | 77.4 | 0.02 | 0 10 | 048 0.0 | 0.0. | 332 0 | 2.20 | 0.01 | 0.712 |
| MuM-Cul 4 | 11 | 133 | -0.4 | -0.4 | C4.0 | C00.0 | 21.0 | 0.06 | 0 0050 | -1.64 | 0.35 0.0 | 040 | 20.2 | 0 0 | .0 10. | -0- 2/0 | 0.0 8/0 | 0 0 | 2.1.2 | CO.0 | 0.018 |
| MirM-Cirl 6 | 9 | 151 | -1.6 | 5.0 | 037 | 700.0- | 0.33 | 0.78 | CLC00.0- | 10.1 | 0.08 | U U | 195 | | 0 10 | -0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 | 143 -0.04 | 174 0 | 2.2 | 0000 | 100 |
| MuM-Cu1 7 | -5.3 | 105 | 0.5 | 0.86 | 0.43 | 0.032 | 0.19 | 0.52 | -0.005 | 0.2 | 0.41 -6 | 0.004 | 58.4 -6 | 005 0 | .01 0. | 127 -0.0 | 125 0.0 | 5 0 | 2.3 | 0.07 | 0.023 |
| MuM-Cu2 | -1.1 | 121 | -0.1 | -0.71 | 0.15 | 0 | 0.59 | 0.03 | -0.005 | 0.09 | 0.4 -(| 0.004 | 76.3 -(| 1.005 0 | .01 0. | 004 0.4 | 0.1 0.1 | 3 0 | 2.19 | 0.01 | 0.012 |
| MuM-Cu2_1 | -0.9 | 131 | -0.4 | -0.4 | -0.32 | 0 | 2.23 | 0.24 | 0 | -0.04 | 0.51 6 | 014 | 47.6 | 0.1 0 | .00 00. | 056 0.0 | 47 0. | 1 0 | 2.2 | -0.01 | -0.001 |
| MuM-Cu2_2 | 10.9 | 135 | 1.7 | -1.8 | -0.84 | 0.021 | 0.47 | 0.62 | 0 | 0.59 | 0.18 | 0 0 | 82.7 -(| 0 900 | 00 00 | 047 0. | 0.0- 80 | 39 0 | 1.62 | 0.039 | 0.031 |
| MuM-Cu2 4 | 3 6 | 133 | -1 5 | 0.14 | -0.47 | 0.043 | 0.37 | 0.18 | 0000 | 10.0 | 0.02 | | 35.7 0 | 0 520 | 0 10 | .0 207 | 10- 80 | 10 | 1.2 | 0.04 | 0.035 |
| MuM-Cu2 5 | 5 | 153.7 | -1.9 | 0 | -0.39 | -0.005 | 0.26 | 0.33 | 0 | 0.07 | 0.03 -0 | 0.005 | 85.4 | 0 0 | .0- 10. | 009 0.1 | 17 -0.0 | 5 0 | 2.50 | 0.04 | 0.000 |
| MuM-Cu2_6 | 2.4 | 167 | -0.4 | 0 | 0.07 | 0.011 | -0.23 | -0.2 | 0.012 | - 0.19 |)- 61.0 | 0.014 | 58 0 | .022 0 | .00 00. | 151 0.4 | 0 60 | 0 | 2.10 | 0.084 | 0.017 |
| MuM-Cu2_7 | -5.8 | 144.6 | -1.9 | 0.0 | -2.61 | -0.004 | 3.3 | 0.8 | 0 | -0.47 | 0.42 0 | 1001 | 58.6 0 | .022 0 | .01 0. | 095 0.0 | 0.1 | 4 0 | 1.62 | .000 | 0.007 |
| Penn-S | 12.5 | 194 | | -0.26 | 9 | 120.0 | 0.36 | 6.3 | 0 0 | 0.34 | 322 -4 | 810.0 | 203 0 | 0 410.0 | 0.00 | 0.0 710 | -0.0- 110 | 0 00 | 4.2 | 0.42 | -0.004 |
| Penn-S_1 | C.11- | 142 | 4.1 | 17:0- | 91 | c 10 0- | -0.04 | 1.06 | 100 | CI.0- | 333 -1 | 004 | 0 177 177 | 0 100 | 0 9 | 0.0 0.00 | 0.0- 20 | 0 791 | 3.60 | 20.00 | 0.004 |
| Penn-S 3 | 0.9 | 133.4 | -0.4 | -0.14 | 1.1 | -0.003 | 0.45 | -0.13 | 0 | 0.03 | 389 0 | 210, | 194 | 0 0 | 00 | -0.0 | 0.0 0.1 | 4 0 | 4.8 | 10.0- | -00.00 |
| Penn-S_4 | 19.5 | 147 | 2 | -0.24 | -0.4 | -0.002 | 0.01 | -0.69 | 0 | 0.64 | 351 | 0 | 193 | 0 0 | .00 00. | 0.0- 110 | 0.7 0.2 | 1 0 | 4.32 | 00.00 | -0.002 |
| Penn-S_5 | -2.4 | 147 | -0.2 | -0.64 | -0.7 | -0.009 | -0.03 | -0.15 | 0 | -0.19 | 346 0 | 1.017 | 188 | 0 0 | .0- 00. | 006 0.1 | 08 0 | 1 0.00 | 5 4.5 | -0.00 | 0.000 |
| Penn-S_6 | -1.2 | 112 | -1.9 | 0.1 | 2.1 | -0.010 | -0.29 | 0.7 | -0.008 | 0.14 | 371 | 0 | 161 | 0 0 | .0- 00. | 026 -0.0 | 126 -0.11 | 52 0 | 5.00 | -00.0 | 0.0004 |
| Penn-S_7 | 4 | 109 | 1.4 | 1.3 | 6.0 | -0.002 | -0.02 | -0.88 | 0.021 | -0.22 | 323 0 | 0.022 | 192 -(| 0.005 0 | .00 | 016 -0.0 | 0.0 | 151 0 | 4.50 | 0.03 | 0.0054 |
| MuM-Margi | C.U- | 1.061 | 7 - | -0.1 | 4.1 | 0.044 | 15.0 | 7.0- | 600.0- | C0.0 | 8/.0 | 0 0 | 8.10 | 00 | .0 CO. | 100 001 | 10 -01 | 9 0 | .4.I | 0000 | 0.041 |
| MuM-Marg1_1 MuM-Marg1_7 | 7 4 | 148 | -1 14 | 0.3 | 5.0- C O | 100.0 | 70.0 | 7.0- | -0.003 | 0.54 | 1 | | 1.20 | | .0 | 1.0 8.0 | 1.0 0C | 000 /000 | 777 Y | 60.0 | CH0.0 |
| MuM-Marg1 3 | 8.8 | 144 | -0.8 | 0.2 | 2 | -0.016 | 0.71 | 0.12 | 0.028 | 0.48 | 9.13 | 0 | 66.8 | 0 | 101 | 725 -0. | 03 0.1 | 7 0 | 1.78 | 0.074 | 0.007 |
| MuM-Margl 4 | 3.9 | 121 | -2.5 | 0.09 | 1.4 | 0.006 | 0.2 | -0.33 | 0 | 0.32 | 0.65 | 0 | 55.9 | 0 0 | .02 0. | 335 -0.0 | 0 900 | 0 | 1.6 | 0.02 | 0.011 |
| MuM-Marg1_5 | 4 | 157.4 | 0.7 | -0.1 | 0.8 | 0 | 0.19 | 0.95 | 0.006 | 0.56 - | 0.35 -(| 0.004 | 62.9 0 | .028 0 | .00 00. | 0 110 | 03 -0.04 | 0 9/1 | 2.12 | 0.115 | -0.003 |
| MuM-Margl_6 | 2 | 125 | 0 | 0.6 | 0 | 0.007 | 0.03 | 1.4 | -0.00587 | 1 | 0.56 -(| 0.004 |)- L.L.L. | 0.011 0 | .01 0. | 005 -0.1 |)65 0.6 | 5 0 | 1.78 | -0.00 | 0.017 |
| MuM-Marg1 7 | 0 | 140 | -0.4 | 0.5 | 1.7 | -0.006 | 0.79 | 0.62 | 0.036 | -0.23 | 0.42 | 0 |)- 86 | 011 0 | .0- 00. | 0- 110 | 011 0.0 | 3 0 | 1.71 | 0.04 | 0.007 |

| Appendix is commerce | 340 | 30 | 5641 | 56 | 59 | 60 | 66.7 | 71.0 | 72.0 | 75 . | 35 | 107 . | II co | 1154. | 118 | 121 cu | 125 _m . 1 | . 16 | 202 | 208 | 209 |
|-----------------------------------|-------------|--------|-------------|--------------|----------------|--------|--------|--------|--------------|--------------|-------|-----------------|---------|---------|---------|----------------|----------------------|---------|-----------------------------------------|-------|--------|
| MBH 69 | S MBH 69 | MBH 69 | MASSI | MBH 66 | C0 MBH 69 | MBH 69 | MBH 69 | MASSI | VBH 66 A | AS (BH 69 A) | Mo A | Ag 4BH 69 A. | BH 69 M | BH 69 M | BH 72 M | (BH 69 M | Ie IBH 69 M | BH 66 A | ASSI N | BH 66 | MBH 66 |
| MuM-Marg2 7 | 120 | 0.4 | 0.3 | 0.4 | -0.022 | 0.66 | 1.4 | -0.008 | 1.07 | -0.14 | 0 | 102 | 0.010 | 0.02 | 0.029 | 0.06 | 0.27 (| 0.005 | 1.34 | 0.072 | 0.084 |
| MuM-Marg2_1 4 MuM-Maro2_2 2_5 | 148 | -1.1 | -0.0 | -0.4 -2.4 | 0.009 | -0.29 | 0.59 | 0.025 | 0 7 | 0.25 | 0 0 | 98.4 | 0.005 | 0.00 | 0.047 | 0.03 | 0.12 | 0 0 | 2.06 | 0.009 | 3.26 |
| MuM-Marg2_3 8.8 | 142 | -0.3 | 1.3 | -1.9 | 0.016 | -0.11 | 0.09 | 0 | -0.04 | 0.21 | 0 | 108.7 | 0 | 0.00 | 0.006 | 0.106 | 0.16 | 0 | 1.81 | 0.006 | 3.5 |
| MuM-Marg2_4 6.8 | 135 | -0.42 | -0.06 | -1.5 | 0.007 | -0.01 | 0.1 | 0 | 0.93 | 0.37 | 0 | 165 | 0 | 0.02 | 0.069 | -0.04 | 0.23 | 0 | 1.47 | 0.04 | 2.22 |
| MuM-Marg2_5 7.3 | 130 | -0.1 | -0.6 | -3.5 | 0.013 | 0.38 | -0.21 | 0.028 | -0.03 | 0.13 | 0.008 | 126 | 0 0 | 0.01 | 0.045 | -0.033 | 0 | 0 | 1.85 | 0.037 | 1.26 |
| MuM-Marg2_6 4.4 MuM-Marg2 7 -5 | 129 | 0.1 | 0.0 4.1- | 0.3 | -0.004 | -0.04 | 0.74 | 0.033 | -0.06 | 0.09 | 0.008 | 123 | 0.023 | 0.00 | 0.014 | 0.034 | 0.015 | 0 0 | 2.34 | 0.024 | 1.59 |
| Penn-L -5.4 | 144 | -0.1 | -1.02 | 2.1 | 0.009 | 0.07 | -0.06 | 0.042 | 0.8 | 463 | 0 | 219 | 0 | 0.00 | 0.027 | 0.002 | 0.11 | 0 | 5 | 0.034 | 0.004 |
| Penn-L_1 -6 | 151 | -0.39 | -0.5 | -1.8 | -0.011 | 0.1 | 0.3 | 0.013 | -0.35 | 436 | 0.014 | 227 | 0 | 0.00 | -0.01 | -0.014 | 0.091 | 0 | 5.62 | 0.047 | -0.008 |
| Penn-L_Z 0 Penn-L_3 7 1 | 154 | -0.2 | -1.01 | 2.8 | 0.006 | 0.28 | -0.6 | -0.003 | 100 | 442 | 0.013 | 222 | 0 000 | 0.00 | -0.02 | 0 038 | 0.05 | 0 0 | 6.14 | 0.014 | 0.008 |
| Penn-L 4 9.1 | 129 | -0.41 | 0.9 | 1.8 | -0.004 | 0.31 | -0.23 | -0.003 | 75.0 | 379 | 0.038 | 199 | 0.005 | 0.00 | 0.004 | 0.042 | 0.038 | 0 | 4.7 | 0.043 | -0.010 |
| Penn-L_5 8.3 | 135 | 0.55 | 0.76 | 1.4 | 0.002 | -0.16 | 0.35 | -0.010 | -0.97 | 410 | 0 | 201 | 0 | - 00.0 | 0.002 | 0.01 | 0.058 | 0 | 4.69 | 0.043 | -0.003 |
| Penn-L_6 -8.4 | 129 | 0.37 | 0.07 | 3.3 | 0 | -0.14 | 1 | -0.014 | -0.4 | 431 | 0 | 242 | 0.016 | 0.00 | 0.018 | 80.0 | 0.11 | 0 0 | 4.59 | 0.041 | 0.004 |
| Penn-L_7 -/.1 MM_IRH 6 | 161 | -0.19 | 1.2 | 2.42 | 7007 | 0.09 | 0.50 | -0.00 | -0.5 | 13.7 | 0 14 | 184 | C00.0- | 00.0 | 0.06 | 0.00 | 610.0 | 0 0 | 7.07 | 0.004 | 200.0- |
| MM-IRH 1 -6 | 128.5 | -0.35 | -0.2 | -0.83 | -0.17 | -0.1 | 0.2 | -0.042 | 0.6 | 11 | 0.32 | 193 | 0.02 | -0.01 | 0.002 | 0.086 | -0.1 | 0.003 | 1.64 | 0.005 | -0.016 |
| MM-IRH_2 12 | 131 | -0.77 | -0.5 | 0.4 | 0 | -0.7 | 0.01 | 0 | 7 | 12.5 | 0.02 | 215.3 | 0.05 | -0.01 | 0.05 | -0.13 | 0.02 | 0.003 | 2.33 | 0.004 | 0.002 |
| MM-IRH_3 -7 | 179 | 0.3 | -2 | -0.3 | -0.01 | -0.8 | 0 | 0.08 | 1.4 | 16.3 | 60.0 | 317 | 0.02 | - 10.0 | 0.044 | 0.04 | -0.1 | 0 | 3.42 | 0.007 | -0.005 |
| MM-IRH_4 -2 | 156 | -0.41 | 0.93 | -0.08 | -0.09 20.02 | -0.28 | 0.08 | -0.09 | 0.88 | 13.6 | 0.17 | 204.7 | 0.14 | - 10.0 | -0.089 | 0.013 | -0.15 | 0.002 | 2.18 | 0.004 | 0.004 |
| MM-IRH 6 7.6 | 141 | -0.04 | -0.47 | 21- | -0.115 | -0.17 | 0.07 | CT-0- | -0.81 | C C L | 50.0 | 267 | 0+0.0+0 | 0.00 | 200.0 | 0.05 | -0.14 | C70.0 | 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 0.012 | -0.019 |
| MM-IRH_7 3.6 | 138 | -0.24 | -0.1 | -1.66 | -0.053 | -0.45 | 0.32 | 0.09 | -0.78 | 11.7 | -0.1 | 202 | 0.003 | 0.01 | 0.029 | 0.1 | -0.12 (| 0.029 | 1.36 | 0.016 | 0.008 |
| MM-CMK 0.9 | 151 | -0.17 | -0.1 | 0.1 | -0.01 | -0.33 | -0.22 | -0.083 | 0.88 | 10.4 | -0.24 | 109.9 | 10.0 | 0.00 | 0.02 | -0.05 | 0.15 | 0.002 | 4.33 | 0.001 | -0.001 |
| MM-CMK_I -/./ | 144 | 0.27 | 0.6 | 0.53 | -0.21 | -0.2 | 0.23 | 0.013 | 5.0- 10.0 | 11.4 | -0.06 | 116.3 | -0.029 | 10.0- | 0.013 | 10.0 | | 100.0 | 3.98 | 100.0 | 100.0- |
| MM-CMK 3 -1.7 | 135 | -0.02 | 0 | 60.0- | -0.01 | -0.8 | 0.19 | 0.21 | 0.3 | 10.5 | 0.13 | 130.3 | 10.0 | -0.01 | 0.065 | -0.02 | 0.2 | 0 | 3.8 | 0.022 | 100.0- |
| MM-CMK_4 -2.6 | 113 | -0.01 | -0.63 | 0.8 | 0.06 | -0.88 | 0.1 | 0.07 | 0.6 | 10.4 | 0.17 | 63 | 0.04 | 0.01 | 0.041 | 60.0 | - 10.0 | 0.001 | 1.42 | .0013 | -0.012 |
| MM-CMK_5 4.4 | 119 | -0.2 | 0,4 | 0.1 | 0.01 | 1.14 | -0.21 | -0.3 | -0.16 | 10 | 0.09 | 56.7 | 0.02 | 0.01 | 0.007 | 0.05 | 0.1 | 0.012 | 1.48 | 0.005 | 0.007 |
| MM-CMK_0 2 MM-CMK_7 _05 | 1.011 | 75.0 | 1.0 | 0 | 0.13 | 1.0 | 0.18 | -0.03 | 1.0 | 11 | 0 07 | 6.16 | 0 00 0 | 0.00 | 0.01 | c0.0- | 0.01 | 500.0 | 5.0.C | C10.0 | C100.0 |
| MM-PMK 7.2 | 94 | -0.44 | -0.56 | -2- | 0.01 | -0.06 | -0.25 | 0.17 | 0.44 | 12 | 0.2 | 26.2 | 0.06 | 0.01 | 0.018 | 0.11 | 0.012 | 0.003 | 1.54 | 900.0 | -0.008 |
| MM-PMK_1 -7 | 105 | 0.34 | 1.2 | -0.6 | 0.078 | -0.29 | 0.46 | -0.07 | 0.58 | 13.4 | -0.09 | 20.8 | 0.08 | 0.02 | 0.032 | -0.004 | 0.002 | 0.009 | 1.42 | 0.002 | 0 |
| MM-PMK_2 9 | 16 | 0.01 | 0.95 | 1.2 | 0.01 | 0.44 | 0.4 | 0.02 | 0.38 | 8.9 | 0.07 | 18.9 | 0.048 | 0.01 | 0.05 | 0.076 | 0.053 | 0.001 | 1.29 | 010 | 0.011 |
| MM-PMK 4 -2 | 122.4 | -0.61 | 0.43 | -0.6 | -0.28 | -0.85 | 20.0- | 0.06 | -0.78 | 8.1 | 0.1 | 27.2 | 0.047 | 00.00 | 0.108 | 0.12 | 0 0 | 200.0 | 1.59 | 20000 | 0.001 |
| MM-PMK_5 -4 | 93 | 0.13 | 0.9 | -1.9 | 0.14 | 0.7 | -0.01 | 0.19 | 0.45 | 5.9 | -0.06 | 24.5 | 0.08 | 0.00 | 0.071 | 0.047 | 0.16 (| 0.005 | 2.01 | 0.008 | -0.002 |
| MM-PMK_6 -9 | 103 | 0.27 | 1.2 | 0.5 | 0.04 | -0.2 | 0.04 | 0.15 | -0.5 | 11.5 | -0.02 | 24.9 | 0.05 | 0.00 | 0.007 | -0.07 | 0.014 (| 2005 | 2.1 | 0.004 | -0.001 |
| MM-PMK_7 -3 MM-CFW -4 | 121.3 | -1.06 | 0.7 | -2.9 | 0.19 | -0.21 | 0.28 | -0.08 | -0.01 | 10.9 | 0.14 | 23.4 | 0.142 | 0.00 | 0.1 | -0.103 | 0.07 | 0.002 | 1.11 | 0 | -0.00 |
| MM-CFW 1 -4 | 106 | -0.47 | 36 | 870 | 0.04 | 0.2 | 0.54 | -0.13 | -0.9 | 8.6 | 0 | 26.6 | 0.04 | 0.00 | -0.01 | 0.035 | 0.01 | 0.001 | 2.75 | 760.0 | 0.009 |
| MM-CFW_2 3 | 156 | -0.65 | 1.5 | 8.5 | -0.09 | 1.3 | 0.26 | -0.04 | 0.3 | 9 | -0.24 | 157 | -0.09 | -0.01 | -0.04 | 0.034 | 0.22 | 0.004 | 6.67 | 0.004 | -0.008 |
| MM-CFW_3 3 | 154 | -1.55 | 0.9 | 12.7 | -0.093 | 0.32 | 0.81 | 0.19 | -0.96 | 10.1 | 0.13 | 181 | -0.013 | - 10.0 | -0.025 | 610.0- | -0.1 | 0.008 | 11.93 | 0.003 | -0.005 |
| MM-CFW 5 9 | 661 | 1.0 | 171 | 94 | C7.C | 0.51 | 0.46 | 0.19 | -0.3 | 1.01 | 0.25 | 110 | t0.0 | 0.00 | | ccu.u 0.075 | 0.02 | 100.0 | 65.5 | 1.033 | 0.0026 |
| MM-CFW_6 10 | 196 | 0.1 | 1.2 | 233 | 0.012 | 0.02 | 0.78 | 0.02 | 0.65 | 33.7 | 0.24 | 73.1 | 0.105 | 0.00 | 0.009 | -0.08 | 0.08 | 0 | 3.87 | 0.005 | 0.006 |
| MM-CFW 7 -3.3 | 210 | 0.9 | 0.7 | 36.8 | 0.17 | -1.3 | 0.21 | 0.15 | 0 | 23.6 | -0.07 | 142.7 | 0.1 | 0.00 | 0.029 | -0.01 | 0.15 (| 0.017 | 7.36 | 0.014 | -0.006 |

| | 31P | 34S | ⁵³ Cr | 55 Min | ⁵⁶ Fe | 59C0 | IN 09 | 66 Zn | 71Ga | "Ge | 25 AS | 95Mo | 107 Ag | " Cd | 115 In | 118Sn | 121 Sb | ¹²⁵ Te | 07 Au | ⁰² Hg | ⁰⁸ Pb | ²⁰⁹ Bi |
|----------|--------|--------|------------------|--------|------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|----------|----------|-------------------|----------|------------------|------------------|-------------------|
| | MBH 69 | MBH 69 | MBH 69 | MASSI | MBH 66 | MBH 69 | MBH 69 | MBH 69 | MASSI | MBH 66 | MBH 69 | ISSIM | MBH 69 | MBH 69 | VIBH 69 | MBH 72 1 | WBH 69 N | IBH 69 A | IBH 66 1 | W ISSN | 3H 66 A | fBH 66 |
| Odw-WW | -2.8 | 186 | -0.49 | 0.3 | -2.8 | 0.08 | 0.5 | 0.82 | -0.04 | -0.18 | 7.7 | -0.03 | 77.3 | 0.01 | -0.01 | -0.022 | 0.53 | 0.04 | 0.003 | 1.1 | 800. | 0.074 |
| MM-WP0_1 | -0.1 | 164 | -0.04 | -0.2 | 0.1 | -0.26 | -0.1 | 0.17 | 0 | -0.28 | 8.2 | -0.34 | 149 | -0.166 | -0.01 | -0.046 | 0.306 | -0.12 | 0.004 | 1.4 | .02 | 0.005 |
| MM-WP0_2 | 1.3 | 147 | 0.19 | -0.7 | -0.9 | 0.06 | -1.18 | 0.26 | 0.04 | -0.27 | 12.6 | 0.18 | 113.2 | 0.13 | -0.01 | 0.013 | 0.319 | -0.399 | 0.003 | 1.74 | .021 | 0.068 |
| MM-WP0_3 | -2 | 142 | 0.06 | -0.6 | -1.8 | 0 | -0.94 | 0.17 | -0.2 | 0.23 | 8.6 | -0.01 | 66 | 0.04 | 0.00 | -0.02 | 0.226 | -0.24 | 0.007 | 1.41 | 10.0 | 0.016 |
| MM-WPO 4 | 0.8 | 150 | -0.09 | -1.48 | -2.3 | -0.066 | -0.04 | -0.19 | -0.21 | 0 | 6.5 | 0.14 | 102 | -0.04 | 0.00 | 0.021 | 0.219 | -0.11 | 0.002 | 1.07 | .008 | 0.02 |
| MM-WPO 5 | 1.4 | 105 | -0.35 | 0 | 7 | 0.01 | 0 | -0.21 | 0.02 | -0.42 | 6.8 | -0.08 | 100 | -0.162 | -0.01 | 0.011 | 0.22 | -0.08 | 0.002 | 1.49 | .028 | 0.004 |
| MM-WPO_6 | -3.3 | 166 | -0.16 | -0.6 | 3.5 | -0.14 | -0.34 | 0.02 | -0.01 | 0.44 | 8.9 | 0.43 | 100.4 | -0.03 | 0.00 | 0.006 | 0.21 | -0.05 | 0.007 | 1.48 | 003 | 0.006 |
| MM-WPO_7 | -5.1 | 148.4 | 0.11 | 1 | -3.3 | -0.14 | 0.39 | -0.15 | 0.09 | 0.89 | 8.8 | 0.13 | 93.8 | 0.022 | 0.00 | 0.04 | 0.35 | 0.04 | 0.003 | 1.07 | .014 | 0.028 |
| HMO-MM | -1.5 | 124 | -0.13 | 0.4 | 4.2 | 0.03 | 0.5 | 0.63 | 0.14 | 0.29 | 41.9 | 0.01 | 200.4 | 0.02 | 0.00 | 0 | 0.06 | -0.133 | 0.001 | 2.27 | .005 | -0.003 |
| I_HMO-MM | -5.2 | 124 | 0.06 | 0.6 | -0.2 | -0.032 | 0.1 | -0.31 | -0.06 | 0.2 | 39.5 | 0.3 | 202 | 0.06 | -0.01 | -0.034 | 0.08 | -0.12 | 0.007 | 1.84 | .012 | 0.007 |
| MM-OMH_2 | 1.8 | 113 | -0.02 | -0.76 | 2.6 | 0.04 | -1.1 | 0.35 | -0.06 | 0.9 | 31.4 | -0.098 | 211.4 | -0.121 | 0.00 | 0.035 | 0.092 | 0.06 | 0.008 | 1.67 | .016 | -0.001 |
| MM-OMH 3 | 1.9 | 139 | 0.28 | 0.3 | 4.7 | 0.26 | -0.29 | 0.15 | -0.06 | 0.26 | 39.3 | 0.22 | 203 | 60.0 | 0.00 | -0.015 | -0.045 | 0.06 | 0.005 | 1.61 | 100. | -0.002 |
| MM-0MH 4 | -2.7 | 142 | 0.01 | -0.3 | 1.3 | 0.07 | -0.73 | 0.41 | 0.04 | 0.08 | 38 | 0.03 | 201 | -0.09 | 0.00 | 0.016 | 0.014 | -0.12 | 0.001 | 1.97 | 101 | 0.001 |
| MM-OMH_5 | -0.8 | 161 | -0.35 | -0.27 | 0.5 | 0.1 | 0.11 | 0.23 | 0.05 | -0.49 | 28.4 | -0.03 | 142 | -0.02 | 0.00 | -0.042 | -0.01 | 0.09 | 0.004 | 2.15 | .002 | -0.005 |
| 9 HWO-WW | 7.2 | 212 | 0.14 | -0.1 | 3.3 | 0.03 | -0.5 | 0.24 | -0.035 | 0.2 | 49.7 | -0.05 | 177 | 0 | 0.00 | 0.009 | -0.048 | 1.16 | 0.013 | 28.6 | 004 | 0.005 |
| 7 HMO-MM | 1 | 170 | 0.39 | 0 | -1.9 | 0.07 | 1.43 | -0.14 | 0.22 | -0.51 | 49.1 | 0.04 | 197 | 0.2 | 0.01 | 0.064 | 0.03 | 0.15 | 0.002 | 1.11 | .002 | 0.003 |
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